# The Crossing Traffic Impact Study 

## Horizon Management Ltd.

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## Executive Summary

| Background | - In November of 2016, Exp Services was hired by Horizon Management Ltd to undertake a traffic impact study for a proposed mixed use development in northeast Saint John, referred to as "The Crossing". <br> - It is estimated that The Crossing will ultimately consist of approximately 850,000 ft2 of building floor area, including commercial, retail, residential, and recreational space. <br> - Full build out is expected to occur in three phases, over a 15-year horizon as follows: <br> - Phase 1 completed by 2023 (approximately $250,000 \mathrm{ft}^{2}$ ) <br> - Phase 2 completed by 2028 (approximately 260,000 ft²) <br> - Phase 3 completed by 2033 (approximately 340,000 $\mathrm{ft}^{2}$ ) |
| :---: | :---: |
| TIS Study Area | - The City of Saint John requested that the TIS consider the impact that newly generated traffic from The Crossing would have on the following intersections: <br> 1. Foster Thurston Drive / Ashburn Road <br> 2. Foster Thurston Drive / NB Route 1 Access Ramps (Exit 128) <br> 3. Ashburn Lake Road / NB Route 1 Access Ramps (Exit 128) <br> 4. Rothesay Avenue / Retail Drive <br> 5. Rothesay Avenue / Ashburn Lake Road <br> 6. Rothesay Road / Fulton Lane <br> 7. Ashburn Road / Jones Drive <br> 8. Ashburn Road / Drury Cove Road <br> 9. Ashburn Road / Rothesay Road <br> 10. Rothesay Avenue / Rothesay Road / NB Route 1 interchange <br> 11. All site access driveway intersections with Ashburn Road |
| Existing Traffic Counts | - Full turning movement counts were undertaken at each intersection within the study area using Miovision's automated video detection equipment. |
| Peak Hour | - From the counts, it was determined that the peak traffic hours were 7:30 am - 8:30 am for the weekday morning, 4:15 pm - 5:15 pm for the weekday evening, and from 1:00 pm - 2:00 pm on Saturday. <br> - An annual growth rate of $1 \%$ was applied to all existing peak hour counts to project background traffic for future horizon years. |
| Projected Traffic Operations without development | - Existing and horizon year traffic operations were projected for the Study Area without the development in place. The following summarizes locations where operational issues (high delays and/or queueing) already exist or are projected: <br> - Rothesay Ave./Retail Dr. - westbound (Retail Dr.) left-turn movement \& SB (Rothesay Ave) left-turn movement (existing); <br> - Rothesay Ave./Ashburn Lake Rd. - northbound (Rothesay Ave.) movement (by 2028); |

- Rothesay Ave./Rothesay Rd. - westbound movement (existing);
- Foster Thurston Dr./Ashburn Rd. - northbound and southbound (Ashburn Rd.) through movements (existing);
- Rothesay Ave./Rte 1 off-ramp - eastbound and westbound (Rothesay Ave.) movements (existing); and
- Rothesay Rd./Rte 1 on-ramp (by 2033).
Recommended
Upgrades to
Address
Current/Future
Operational Issues
without
development
- The following improvements are recommended to address existing and/or future operational issues within the study area regardless of whether the development proceeds:
- Rothesay Rd./Rothesay Ave. - upgrade intersection from current stop-controlled configuration to either traffic signals or a roundabout.
- Rothesay Ave./Rte 1 off-ramp - upgrade intersection from current stop-controlled configuration to either traffic signals or a roundabout.
- Rothesay Rd./Rte 1 on-ramp - construct weaving lane between Route 100 on-ramp and Foster Thurston off-ramp.
- Rothesay Ave./Retail Dr./Ashburn Lake Rd. - realign existing intersections into a 4-leg, fully actuated signalized intersection, with dedicated left turn lanes.

Trip Generation

- The number of newly generated vehicle trips for each phase of the proposed development were estimated as follows using standard trip generation rates published by the Institute of Transportation Engineers:


## Phase 1

- AM Peak Hour - entering: 758, exiting: 641
- PM Peak Hour- entering: 841, exiting: 834
- Saturday Peak Hour - entering: 1071, exiting: 1052


## Phase 2

- AM Peak Hour- entering: 268, exiting: 180
- PM Peak Hour- entering: 428, exiting: 389
- Saturday Peak Hour - entering: 1063, exiting: 915


## Phase 3

- AM Peak Hour - entering: 239, exiting: 121
- PM Peak Hour- entering: 220, exiting: 287
- Saturday Peak Hour - entering: 291, exiting: 251
- Generated trips were adjusted using a $20 \%$ synergy rate and a $25 \%$ pass-by rate and were assigned to the Study Area road network based on existing traffic patterns.

Projected Traffic Operations with development

- Horizon year traffic operations were subsequently projected for the Study Area with the development in place. The following summarizes additional operational issues projected to occur by 2023 with Phase 1 of the development:
- Rothesay Rd. / Rothesay Ave. - westbound (Rothesay Ave), northbound (Route 1 off-ramp), and eastbound (development access) approaches.
- Rothesay Rd./Fulton Ln./Access - eastbound (access) and westbound (Fulton Ln.) movements.
- Rothesay Rd./Ashburn Rd. - eastbound (Ashburn Rd.) approach.
- Rothesay Ave./Rte 1 on-ramp intersections - eastbound approaches.
- It was determined that additional traffic generated by Phase 2 and 3 of the development could not be adequately accommodated without major modifications to the existing road network such as:

1. Major upgrades to the Route 100 interchange area to increase capacity; or
2. Construction of a new underpass near Ashburn Lake Road and Foster Thurston Road.
Impact of Ashburn
Lake / Foster
Thurston
Underpass

Impact of Ashburn
Lake / Foster
Underpass

- The NB Department of Transportation \& Infrastructure has been assessing the long-term need for a new underpass connection in the vicinity of the Ashburn Lake Road and Foster Thurston Drive ramps.
- If/when a new underpass is built, a significant amount of existing traffic is expected to divert away from the Route 100 Interchange, thus alleviating some of the existing operational issues at this location.
- While a significant portion of newly generated traffic from the development would also use the new Ashburn Lake Road underpass, its construction has merit regardless of whether the development proceeds.

Recommended Upgrades to Accommodate Phase 1 Traffic

- The following improvements are recommended to provide acceptable levels of service and delays for Phase 1 of the development:
- Rothesay Rd./Rothesay Ave. - implement actuated-coordinated traffic signals and additional turn lanes at approaches.
- Rothesay Rd./Ashburn Rd. - implement actuated-coordinated traffic signals and separate left turn lane on northbound (Rothesay Rd.) approach.
- Rothesay Ave./Rte 1 off-ramp - implement actuated-coordinated signal and a separate through lane pocket at the eastbound (Rothesay Ave.) approach.
- Ashburn Rd. Accesses - implement separate left turn lanes at all accesses on all approaches to accommodate future traffic demand. Implement traffic signals at the main Ashburn Road access (access in line with Rothesay Ave.).
- Foster Thurston Dr./Ashburn Rd. - addition of separate right turn lane on southbound (Ashburn Rd.) approach to accommodate increase in right turning traffic exiting the development.
- Rothesay Rd./Fulton Ln. - align truck stop access with Fulton Ln. and make access right-in/right-out (left turners use access on

|  | Ashburn Rd.) to prevent left turners from blocking through <br> movement and causing queuing back to Rothesay Rd./Rothesay <br> Ave. intersection. |
| :--- | :--- |
| -Detailed analysis related to these improvements are found in the |  |
| Phase 1 Report |  |

## 1 Introduction

### 1.1 Background

Horizon Management Ltd. is proposing a mixed use development in northeast Saint John (called "The Crossing"), consisting of residential, commercial, and park land. The proposed development site, currently zoned Rural (RU) and Future Development (FD), covers approximately 163 acres. Approximately 120 acres located between Ashburn Road and Highway Route 1 is to be rezoned to Commercial Corridor (CC) and Mid-Rise Residential (RM), while the remaining land located along Marsh Creek is to be rezoned to Park ( P ). A more detailed breakdown of land development is as follows:

- 87.2 acres rezoned to Commercial Corridor
- 31.6 acres rezoned to Mid-Rise Residential
- 42.7 acres rezoned to Park

The proposed development is designed to promote commuters using Rothesay Road and Route 1 to visit the City of Saint John rather than pass through. The area is strategically located adjacent to Rothesay Road and Route 1, as well as several other arterial roadways within the City, making it an ideal location ideal for creating a "gateway" to the City.
It is estimated that a total of approximately $80,000 \mathrm{~m}^{2}$ of building floor area will be constructed at the development site over multiple phases during the next 15-20 years.
Although he development is expected to result in substantial economic benefits for the City of Saint John, concerns have been raised regarding its impacts on traffic circulation. Of particular concern, are the areas between Route 1 and the Kennebecasis Valley and the UNB/Regional Hospital. The development is expected to add significant traffic to this section of the roadway network which already has significant traffic flows.

The City of Saint John has requested a Traffic Impact Study (TIS) be completed and submitted by Horizon Management Ltd. before approval for the proposed development can be granted from the City. The TIS will identify any deficiencies associated with the proposed development and make recommendations to mitigate any expected long-term traffic flow deficiencies within the surrounding area.
The TIS is only one of the technical studies required for the proposed development approval. The required studies are expected to take 3 to 5 years in total to complete.

### 1.2 Study Objectives

The objective of this study is to evaluate existing and future transportation issues and identify any traffic impacts associated with the proposed development within the Study Area. Improvement options to address any deficiencies are to be selected, evaluated, and recommended to ensure a desired level of service to all transportation users within the Study Area over the development horizon.

### 1.3 Study Area

The primary Study Area was identified by the City of Saint John and includes the following intersections:
12. Foster Thurston Drive / Ashburn Road
13. Foster Thurston Drive / NB Route 1 Access Ramps (Exit 128)
14. Ashburn Lake Road / NB Route 1 Access Ramps (Exit 128)
15. Rothesay Avenue / Retail Drive
16. Rothesay Avenue / Ashburn Lake Road
17. Rothesay Road / Fulton Lane
18. Ashburn Road / Jones Drive
19. Ashburn Road / Drury Cove Road
20. Ashburn Road / Rothesay Road
21. Rothesay Avenue / Rothesay Road / NB Route 1 interchange (Exit 129)
22. All site access driveway intersections with Ashburn Road and Rothesay Road

Also included in the Study Area are the existing trails surrounding Marsh Creek, existing transit routes within the area, and parking lots associated with the proposed development. The entire Study Area is shown in Figure 1; with the labels corresponding to the intersection numbers listed above. A detailed site plan can be found in Appendix A.

### 1.4 Horizon Period

Construction of the development is expected to begin in 2018 and be a gradual process with a full build-out completion time of 15 years. As such, this TIS utilizes a horizon year of 2033 with and without the proposed development to determine future traffic conditions within the Study Area at full build-out (i.e. Phases 1, 2, and 3 complete). Similarly, an assumed 2023 Phase 1 horizon year ( 5 years after construction is expected to begin) and 2028 Phase 2 horizon year ( 10 years after the construction is expected to begin) were utilized to capture any traffic impacts within the Study Area throughout the construction process. Comparing future traffic both with and without the development allows for a more accurate assessment of any traffic impacts directly attributed by the proposed development.

An annual growth rate of $1 \%$ has been used to project future background traffic for the horizon periods on the Study Area street network.


Figure 1 - Study Area

## 2 Information Gathering

### 2.1 Existing Traffic Volumes

Exp staff conducted AM and PM peak hour traffic counts at Rothesay Road / Ashburn Road, Ashburn Road / Drury Cove Road, Rothesay Avenue / Retail Drive, and Rothesay Ave / Ashburn Lake on Friday, October 14 $4^{\text {th }}, 2016$ and Friday, October $21^{\text {st }}, 2016$. All other AM and PM counts required for this study were already collected by exp staff for previous studies (including the Move Saint John Transportation Plan and the Route 1 Corridor Study). A $1 \%$ per annum growth rate was applied to all counts collected prior to 2016 to project 2016 base year traffic volumes.

Exp staff conducted Saturday peak hour traffic counts at all intersections within the Study Area (excluding those estimated using Trip Generation) on Saturday, October 15 ${ }^{\text {th }}, 2016$, Saturday October 22 ${ }^{\text {nd }}, 2016$, and Saturday, October $28^{\text {th }}, 2016$.
Peak period counts were collected during the following times at all locations:

- AM Peak Period - Between 7:00 am and 9:00 am on the Friday,
- PM Peak Period - Between 4:00 pm and 6:00 pm on the Friday, and
- Saturday Peak Period - Between 1:00 pm and 5:00 pm on the Saturday.

In addition, counts were estimated using ITE's Trip Generation Manual for the intersections of Rothesay Road / Fulton Lane or Ashburn Road / Jones Drive. Figures 2 and $\mathbf{3}$ show the existing 2016 AM, PM, and Saturday peak hour traffic volumes for all Study Area intersections.


Figure 2 - Existing 2016 Traffic Volumes (1 of 2) AM/PM/SAT


Figure 3 - Existing 2016 Traffic Volumes (2 of 2) AM/PM/SAT

### 2.2 Horizon Year Traffic Volumes

Projected background 2023, 2028, and 2033 AM, PM, and Saturday peak hour traffic volumes were required to evaluate future traffic conditions without the proposed project. Projected volumes were estimated using a $1 \%$ per annum growth rate.
Figures 4 and 5 show the projected background 2023 AM, PM, and Saturday peak hour traffic volumes without the proposed development. Figures 6 and 7 show the projected background 2028 AM, PM, and Saturday peak hour traffic volumes without the proposed development. Figures 8 and 9 show the projected background 2033 AM, PM, and Saturday peak hour traffic volumes without the proposed development.


Figure 4 - Projected 2023 Horizon Year Traffic Volumes (1 of 2) AM/PM/SAT


Figure 5 - Projected 2023 Horizon Year Traffic Volumes (2 of 2) AM/PM/SAT


Figure 6 - Projected 2028 Horizon Year Traffic Volumes (1 of 2) AM/PM/SAT


Figure 7 - Projected 2028 Horizon Year Traffic Volumes (2 of 2) AM/PM/SAT


Figure 8 - Projected 2033 Horizon Year Traffic Volumes (1 of 2) AM/PM/SAT


Figure 9 - Projected 2033 Horizon Year Traffic Volumes (2 of 2) AM/PM/SAT

### 2.3 Street and Intersection Characteristics

### 2.3.1 Study Area Roads

## NB Route 1

Route 1 is classified as a freeway and is maintained by the New Brunswick Department of Transportation and Infrastructure (NBDTI). It provides a bypass route for vehicles passing through the City of Saint John. Route 1 is a divided, 4-lane highway with a posted speed limit of $100 \mathrm{~km} / \mathrm{h}$. Four on/off ramps are present within the Study Area, which provide access to/from Rothesay Avenue, Rothesay Road, Foster Thurston Drive, and Ashburn Lake Road. The estimated average daily traffic on Route 1 is 33,900 vehicles according to traffic counts collected by NBDTI in 2013.

## Rothesay Avenue

Rothesay Avenue is classified as a major arterial. This road provides a route through the commercial area on the east side of Saint John. The roadway has a 4-lane cross-section and operates with a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. There are several driveways present along this road within the Study Area leading to commercial buildings. The three main intersecting roads with Rothesay Avenue used in this Study are Retail Drive which leads to a number of retail stores and Ashburn Lake Road which leads to the on/off ramps to/from Route 1, and Rothesay Road. Separated sidewalks are present along the west side of Rothesay Avenue throughout the entire Study Area, as well as on the east side (continuing south) beginning at the intersection with Tim Street.

Rothesay Road
Rothesay Road is classified as an arterial roadway that runs along the Kennebecasis River towards the Rothesay community area. It is a 2-lane cross-section roadway with a posted speed limit of 50 $\mathrm{km} / \mathrm{h}$ for the majority of the roadway, and changes to $60 \mathrm{~km} / \mathrm{h}$ south of the intersection with Ashburn Road leading to the Route 1 on-ramp. Rothesay Road intersects with Ashburn Road, Fulton Lane, and Rothesay Avenue within the Study Area. There are no separate sidewalks on Rothesay Road, although there are paved shoulders on both sides.

## Ashburn Road

Ashburn Road is classified as a collector road within the Study Area. It provides access to a number of smaller residential areas as well as a few businesses. Ashburn Road is posted at a speed limit of $60 \mathrm{~km} / \mathrm{h}$ with a 2-lane cross-section. Gravel shoulders are present along the entire length of the roadway.

## Foster Thurston Drive

Foster Thurston Drive is classified as an arterial road within the Study Area. It provides access directly off/on Route 1 to/from northern Saint John. Foster Thurston Drive is posted at a speed limit of $50 \mathrm{~km} / \mathrm{h}$ with a 2 -lane cross-section. Narrow gravel shoulders are present along the entire length of the roadway.
Ashburn Lake Road
Ashburn Lake Road is classified as a collector road within the Study Area. It provides access directly off/on Route 1 to/from southern Saint John (Rothesay Avenue), which is primarily a commercial area. Ashburn Lake Road is posted a speed limit of $50 \mathrm{~km} / \mathrm{h}$ with a 2-lane cross section. Railway tracks are present on Ashburn Lake Road approximately 50 m north of Rothesay Avenue.

### 2.3.2 Study Area Intersections

## Route 1 Ramps

Four on and four off ramps to/from Route 1 are present within the Study Area. These ramps connect to Rothesay Road (exit 129), Rothesay Avenue (exit 129), Ashburn Lake Road (northbound exit 128), and Foster Thurston Drive (southbound exit 128). All ramps are free flowing.

## Foster Thurston Drive / Ashburn Road

Foster Thurston Drive / Ashburn Road is a four-legged two-way stop controlled intersection located adjacent to the on/off ramps of Foster Thurston Drive and Route 1. All approaches consist of a shared one lane configuration with no separate turn or slip lanes present.

Rothesay Avenue / Retail Drive
Retail Drive / Rothesay Avenue is a three-leg signalized intersection operating under fixed control with an offset of zero seconds. The northbound approach has one separate through lane and one shared through/right turn lane, the southbound approach has one separate through lane and one shared through/left turn lane, and the westbound approach has separate left and right turn lanes.

## Rothesay Avenue / Ashburn Lake Road

Rothesay Avenue / Ashburn Lake Road is a three-leg signalized intersection operating under fixed control. The northbound approach has one separate through and one shared through/left turn lane, the southbound approach has one separate through and one shared through/right turn lane, and the westbound approach has a shared left turn/right turn lane. The eastbound leg (Ashburn Lake Road) provides access to/from Route 1. This intersection is coordinated with the Retail Drive / Rothesay Avenue intersection so that motorists receive a green light in progression on Rothesay Avenue. The Rothesay Avenue / Ashburn Lake Road intersection is set at an offset of 45 seconds to the Retail Drive / Rothesay Avenue intersection.

## Rothesay Road / Fulton Lane

Rothesay Road and Fulton Lane is a three-legged unsignalized intersection with the stop control located on the westbound approach (exiting Fulton Lane). Each approach is made up of a simple one lane configuration. Fulton Lane consists of a second hand clothing store, a single-detached family home, and a land survey and survey engineering company office building. Existing traffic volumes from Fulton Lane were generated in TripGen using this existing development information.

## Ashburn Road / Jones Drive

Ashburn Road / Jones Drive is a three-legged unsignalized intersection with the stop control located on the eastbound approach (exiting Jones Drive). Each of the approaches consists of a shared one lane configuration. Jones Drive is a small residential area with ten single-detached houses present. Existing traffic volumes from Jones Drive were generated in TripGen using this information.

## Ashburn Road / Drury Cove Road

Ashburn Road / Drury Cove Road is a three-legged unsignalized intersection with the stop control located on the eastbound approach (exiting Drury Cove Road). Each approach consists of a shared one lane configuration. Drury Cove Road leads to a residential area and connects with smaller, local roads within the area.

## Ashburn Road / Rothesay Road

Ashburn Road / Rothesay Road is a three-legged unsignalized intersection with the stop control located on the eastbound approach (exiting Ashburn Road). Each approach consists of a shared one lane configuration.

### 2.4 Active Transportation Characteristics

The existing Trans Canada Trail that runs through the Study Area is Line 11, which is part of Zone 10 in New Brunswick. This trail currently runs adjacent to Ashburn Road and into Rockwood Park.
Figure 7 shows the Trans Canada Trail Line 11 through the Study Area.


Figure 7 - Existing Trans Canada Trail Through Study Area (Line 11)

### 2.5 Transit Characteristics

Saint John Transit is Saint John's public transit system that provides bus routes through the Study Area. There are currently two existing routes where a section runs through the Study Area that includes: the main line (blue), and the comex routes (green). These routes are shown in Figure 8.


Figure 8 - Existing Transit Routes in Study Area
The section of the main line that runs through the Study Area is the Fairville Boulevard Plaza via Rothesay Avenue, which provides service along Rothesay Avenue and Retail Drive. The bus runs in this area every half hour from 6:10 am to 10:40 pm on weekdays, every half hour from 7:10 am to 10:40 pm on Saturday's, and every hour from 10:40 am to $5: 40 \mathrm{pm}$ on Sunday's. A bus stop for this route is located within the Study Area adjacent to the intersection of Rothesay Avenue and Retail Drive.

The section of the comex route that runs through the Study Area is the Kennebecasis Valley Comex, which provides service through the Rothesay Area. The route runs along Route 1 and continues onto Rothesay Road using Exit 129. The bus runs Monday to Friday at 7:05 am, 8:15 am, 4:05 pm, 4:40 $\mathrm{pm}, 5: 15 \mathrm{pm}$, and 6:25 pm. There are currently no bus stops located within the Study Area for this route.

### 2.6 Development Characteristics

The proposed development consists of commercial corridor, mid-rise residential, and parkland rezoning. A detailed layout of the developments can be found in Appendix A.

The commercial corridor will consist of the following developments:

- Highway Service Stop - 26,000 SF
- Various Fast Food Restaurants - 11,400 SF
- Outdoor Anchor - 36,000 SF
- Entertainment Anchor - 40,000 SF
- Health Club - 40,000 SF
- Two hotels - 125 rooms each
- Six Sit-Down Restaurants - 31,400 SF total
- Garage-6,300 SF
- Car Wash - 2,400 SF
- Convenience Retail - 24,075 SF
- Tourist Information Centre - 9,000 SF
- Museum - 15,000 SF
- Two banks - 9,300 SF total
- Various Retail Centres - 123,000 SF total
- Entertainment Centre - 40,000 SF
- Entertainment/Recreation Area - 15 acres
- Dealership - 6 acres
- Storage Facility - 4 acres
- Dealership - 3 acres
- Four offices - 18,000 SF/level, 15,000 SF/level, 15,000 SF/level, and 8,300 SF/level
- Gas Station

The residential area will consist of the following developments:

- 12 mid-rise residential buildings - 20 dwelling units each


## 3 Existing and Future Background Traffic Operations

### 3.1 Introduction

Existing and horizon year operational conditions were established to determine how the street network within the Study Area is currently functioning and how it will function by the horizon years for Phase 1, 2, and 3 without the proposed development. Traffic operations within the Study Area were evaluated using current traffic volumes, road configuration, and traffic control. The intersection performance was measured using the traffic analysis software, Synchro 9, a deterministic model that employs Highway Capacity Manual and procedures are accepted by provincial and municipal agencies throughout North America.

The intersection operations were primarily evaluated in terms of the Level of Service (LOS). Level of Service is a common measure of the quality of performance at an intersection and is defined in terms of vehicular delay. This delay includes deceleration delay, queue move-up time, stopped delay, and acceleration delay. LOS is expressed on a scale of A through F, where LOS A represents very little delay (i.e., less than 10 seconds per vehicle) and LOS F represents very high delay (i.e., greater than 50 seconds per vehicle for a stop sign controlled intersection and greater than 80 seconds per vehicle for a signalized intersection). The ramps were analyzed in terms of LOS, which is measured in terms of density, or passenger cars / km / lane ( $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ). Similar to intersections, LOS is expressed on a scale of A to F. The Highway Capacity Manual (HCM) software was used to evaluate the ramp operations.
Usually LOS D or better is considered acceptable in urban areas before improvements are considered, although some communities accept LOS E. The LOS criteria for signalized and stop sign controlled intersections are shown in Table 1. A description of traffic performance characteristics is included for each LOS.

Table 1 - Level of Service Criteria for Intersections

| LOS | LOS Description | Control Delay (seconds per vehicle) |  |
| :---: | :--- | :---: | :---: |
|  | Signalized <br> Intersections | Stop Controlled <br> Intersections |  |
| A | Very low delay; most vehicles do not stop <br> (Excellent) | less than 10.0 | less than 10.0 |
| B | Higher delay; more vehicles stop (Very <br> Good) | between 10.0 and 20.0 | between 10.0 and 15.0 |
| C | Higher level of congestion; number of <br> vehicles stopping is significant, although <br> many still pass through intersection without <br> stopping (Good) | between 20.0 and 35.0 | between 15.0 and 25.0 |
| D | Congestion becomes noticeable; vehicles <br> must sometimes wait through more than one <br> red light; many vehicles stop (Satisfactory) | between 35.0 and 55.0 | between 25.0 and 35.0 |
| E | Vehicles must often wait through more than <br> one red light; considered by many agencies <br> to be the limit of acceptable delay | between 55.0 and 80.0 | between 35.0 and 50.0 |
| F | This level is considered to be unacceptable <br> to most drivers; occurs when arrival flow <br> rates exceed the capacity of the intersection <br> (Unacceptable) | greater than 80.0 | greater than 50.0 |

### 3.2 Existing and Horizon Year LOS without Development

### 3.2.1 Foster Thurston Drive / Ashburn Road

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table $\mathbf{2}$ for the Foster Thurston Drive / Ashburn Road intersection. The analysis output can be found in Appendix B.

Table 2 - LOS Summary for Foster Thurston Dr/Ashburn Rd without Development


Overall, the Foster Thurston Drive / Ashburn Road intersection is currently operating at an excellent LOS A with an intersection delay of 8 seconds/vehicle and 5 seconds/vehicle during the AM and Saturday peak period, respectively and at an overall very good LOS B with an intersection delay of 11 seconds/vehicle during the PM peak period. The eastbound and westbound movements are operating at LOS B or better with average delays of 10 seconds/vehicle or less during the AM, PM, and Saturday peak periods. The northbound approach is operating the lowest in terms of LOS, particularly during the PM peak period. It is operating at satisfactory LOS D (average delay of 31 seconds/vehicle) and LOS B (average delay of 11 seconds/vehicle) during the AM and Saturday peak period, respectively. During the PM peak period the northbound approach operates at an unacceptable LOS F with an average delay of 86 seconds/vehicle. The southbound approach operates at LOS D or better with an average delay of 30 seconds/vehicle or less during the AM, PM, and Saturday peak period. The $\mathrm{v} / \mathrm{c}$ ratios are all 0.65 or less, indicating that there is sufficient capacity.

By the 2023, 2028, and 2033 horizon years without development, the Foster Thurston Drive / Ashburn Road intersection is projected to operate at an overall LOS C or better with an intersection delay of 19 seconds/vehicle or less during the AM, PM, and Saturday peak period. All movements during the Saturday peak period are projected to operate at LOS B or better with an average delay of 12 seconds/vehicle or better for the 2023, 2028, and 2033 horizon years. During the AM peak period, all westbound and eastbound movements are projected to operate at LOS B or better with an average delay of 11 seconds/vehicle or lower by the 2023, 2028, and 2033 horizon years. By 2028 and 2033, the northbound and southbound approaches are projected to operate at LOS F with average delays of 109 seconds/vehicle or less. By 2033 during the PM peak period the northbound and southbound movements are projected to operate at LOS F with average delays of 216 seconds/vehicle or less. The v/c ratios at each movement for all three peak periods do not exceed 0.95 .

Operational deficiencies currently exist at the northbound movement of the Foster Thurston Drive / Ashburn Road intersection during the PM peak period, and are projected to occur at the northbound and southbound movements during the AM peak period by 2028 without development as well as in the northbound and southbound movements during the PM peak period by 2033 without development.

### 3.2.2 Foster Thurston Drive /NB Route 1 Access Ramps (Exit 128)

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 3 for the Foster Thurston Drive Access Ramps to Route 1. The analysis output can be found in Appendix B

The Foster Thurston Drive off-ramp from Route 1 is currently operating at LOS C, LOS B, and LOS A during the AM, PM, and Saturday peak period, respectively. By the 2023 horizon year without development, the Foster Thurston Drive off-ramp is projected is operating at LOS D (density of 17.6 $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ) during the AM peak period; minimal changes are projected for the PM and Saturday peak periods. By the 2028 and 2033 horizon years without development, the Foster Thurston Drive offramp is projected to continue operating at LOS D, LOS B, and LOS A during the AM, PM, and Saturday peak periods, respectively.

The Foster Thurston Drive on-ramp from Route 1 is currently operating at LOS C, LOS B, and LOS A during the AM, PM, and Saturday peak period, respectively. By the 2023 horizon year without development the on-ramp is projected to operate at LOS D (density of $17.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ), LOS B (density of $8.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ), and LOS B (density of $6.0 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ) during the AM , PM, and Saturday peak period, respectively. Minimal changes are projected for the Foster Thurston Drive on-ramp from Route 1 by the 2028 and 2033 horizon year without development during all three peak periods.

No operational deficiencies are projected for the Foster Thurston on-ramp or off-ramp for Route 1 during the AM, PM, or Saturday peak period by the 2033 horizon year without the development in place.

Table 3 - LOS Summary for Foster Thurston Dr/Rte 1 Ramps without Development

|  | AM Peak | PM Peak | SAT Peak |
| :--- | :---: | :---: | :---: |
| Ramp | LOS <br> Density (pc/km/ln) | LOS <br> Density (pc/km/ln) | LOS <br> Density (pc/km/ln) |
| Existing (2016) Conditions |  |  |  |
| Rte 1 - Foster <br> Thurston Dr off-ramp | C | B | A |
| Rte 1 EB - Foster <br> Thurston Dr on-ramp | 16.5 | 6.8 | 4.4 |

Projected 2023 Horizon Year Conditions without Development

| Rte 1 - Foster | D | B | A |
| :--- | :---: | :---: | :---: |
| Thurston Dr off-ramp | 17.6 | 7.3 | 4.7 |
| Rte 1 EB - Foster | D | B | B |
| Thurston Dr on-ramp | 17.7 | 8.4 | 6.0 |

Projected 2028 Horizon Year Conditions without Development

| Rte 1 - Foster | D | B | A |
| :--- | :---: | :---: | :---: |
| Thurston Dr off-ramp | 18.5 | 7.7 | 5.0 |
| Rte 1 EB - Foster | D | B | B |
| Thurston Dr on-ramp | 18.6 | 8.7 | 6.2 |


| Projected 2033 Horizon Year Conditions without Development |  |  |  |
| :--- | :---: | :---: | :---: |
| Rte 1 - Foster | D | B | A |
| Thurston Dr off-ramp | 19.5 | 8.0 | 5.2 |
| Rte 1 EB - Foster | D | B | B |
| Thurston Dr on-ramp | 19.4 | 9.1 | 6.4 |

### 3.2.3 Ashburn Lake Road / NB Route 1 Access Ramps (Exit 128)

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 4 for the Ashburn Lake Road Access Ramps to Route 1. The analysis output can be found in Appendix B

The Ashburn Lake Road off-ramp from Route 1 is currently operating at LOS A, LOS C, and LOS A during the AM, PM, and Saturday peak period, respectively. By the 2023 horizon year without development, the Ashburn Lake Road off-ramp is projected is operating at LOS D (density of 18.2 $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ) during the PM peak period; minimal changes are projected for the AM and Saturday peak periods. By the 2028 and 2033 horizon years without development, the Foster Thurston Drive offramp is projected to continue operating at LOS A, LOS D, and LOS A during the AM, PM, and Saturday peak periods, respectively.

The Ashburn Lake Road on-ramp from Route 1 is currently operating at LOS A, LOS D, and LOS B during the AM, PM, and Saturday peak period, respectively. By the 2023 and 2028 horizon years without development the on-ramp is projected to continue operating at LOS A, LOS D, and LOS B during the AM, PM, and Saturday peak period, respectively. By the 2033 horizon year without development, the on-ramp is projected to operate at LOS B (density of $6.1 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ), LOS E (density
of $22.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ), and LOS B (density of $7.8 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ) during the $A M, P M$, and Saturday peak period, respectively.

No operational deficiencies are projected for the Ashburn Lake Road on-ramp or off-ramp for Route 1 during the AM, PM, or Saturday peak period by the 2033 horizon year without the development in place.

Table 4 - LOS Summary for Ashburn Lake Rd/Rte 1 Ramps without Development

|  | AM Peak | PM Peak | SAT Peak |
| :--- | :---: | :---: | :---: |
| Ramp | LOS | LOS | LOS |
|  | Density (pc/km/ln) | Density (pc/km/ln) | Density (pc/km/ln) |

Existing (2016) Conditions

| Rte 1 - Ashburn Lake | A | C | A |
| :--- | :---: | :---: | :---: |
| Rd off-ramp | 3.3 | 17.0 | 4.3 |
| Rte 1 EB - Ashburn | A | D | B |
| Lake Rd on-ramp | 5.4 | 19.1 | 6.8 |

Projected 2023 Horizon Year Conditions without Development

| Rte 1 - Ashburn Lake | A | D | A |
| :--- | :---: | :---: | :---: |
| Rd off-ramp | 3.6 | 18.2 | 4.7 |
| Rte 1 EB - Ashburn | A | D | B |
| Lake Rd on-ramp | 5.6 | 20.4 | 7.2 |

Projected 2028 Horizon Year Conditions without Development

| Rte 1 - Ashburn Lake | A | D | A |
| :--- | :---: | :---: | :---: |
| Rd off-ramp | 3.9 | 19.2 | 4.9 |
| Rte 1 EB - Ashburn | A | D | B |
| Lake Rd on-ramp | 5.8 | 21.3 | 7.5 |

Projected 2033 Horizon Year Conditions without Development

| Rte 1 - Ashburn Lake | A | D | A |
| :--- | :---: | :---: | :---: |
| Rd off-ramp | 4.1 | 20.2 | 5.2 |
| Rte 1 EB - Ashburn | B | E | B |
| Lake Rd on-ramp | 6.1 | 22.4 | 7.8 |

### 3.2.4 Rothesay Avenue / Retail Drive

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 5 for the Rothesay Avenue / Retail Drive intersection. The analysis output can be found in Appendix B.

Table 5 - LOS Summary for Rothesay Ave/Retail Dr without Development


The Rothesay Avenue / Retail Drive intersection is operating at an overall LOS C or better with an intersection delay of 24 seconds/vehicle or less during the AM, PM, and Saturday peak period. The worst movement in terms of LOS is the westbound left-turn movement, which is operating at LOS D (average delay of 41 seconds/vehicle) during the AM peak period and at an unacceptable LOS F with an average delay of 132 seconds/vehicle and 130 seconds/vehicle during the PM and Saturday peak periods, respectively. All other movements are operating at LOS B or better with average delays of 15 seconds/vehicle or less. The $95^{\text {th }}$ percentile queue lengths are the longest at the westbound left turn movement, with lengths of 36 m to 112 m . The v/c ratio at the westbound left turn movement exceeds 1.0 during the PM peak period and is approaching the threshold during the Saturday peak period.

By the 2023, 2028, and 2033 horizon years without development, the Rothesay Avenue / Retail Drive intersection is projected to operate at an overall LOS E or better with an intersection delay of 56 seconds/vehicle or less during all three peak periods. All movements are projected to operate at LOS D or better with an average delay of 54 seconds/vehicle or less during the AM, PM, and

Saturday peak periods. The exception is the westbound left turn movement during the PM and Saturday peak period which is projected to operate at LOS F (average delay of 191 seconds/vehicle or less). The $95^{\text {th }}$ percentile queue length at this movement are projected to 137 m during the PM peak period. The $\mathrm{v} / \mathrm{c}$ ratio at the westbound left turn movement is projected to exceed 1.0 during both the PM and Saturday peak period, indicating that the demand exceeds the capacity. The v/c ratio at the southbound movement is projected to approach 1.0 during the PM and Saturday peak period.

Operational deficiencies currently exist at the westbound left turn movement during the PM and Saturday peak period and are projected to worsen in terms of delay and queuing by the 2033 horizon year without development.

### 3.2.5 Rothesay Avenue / Ashburn Lake Road

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 6 for the Rothesay Avenue / Ashburn Lake Road intersection. The analysis output can be found in Appendix B.

The Rothesay Avenue / Ashburn Lake Road intersection is currently operating at LOS B with an intersection delay of 20 seconds/vehicle or less during the AM, PM, and Saturday peak period. All individual movements are operating at LOS C or better with an average delay of 26 seconds/vehicle or less. The $\mathrm{v} / \mathrm{c}$ ratios are all 0.81 or less, indicating that there is sufficient capacity. The $95^{\text {th }}$ percentile queue lengths are all 76 m or less, with the longest queues projected at the eastbound approach.

By the 2023, 2028, and 2033 horizon year without development, the Rothesay Avenue / Ashburn Lake Road intersection is projected to operate with minimal changes during the AM and Saturday peak period.

By the 2023 horizon year without development during the PM peak period, the Rothesay Avenue / Ashburn Lake Road intersection is projected to operate at an overall LOS C with an intersection delay of 33 seconds/vehicle. All individual movements are projected to operate at LOS D or better with an average delay of 37 seconds/vehicle or less. The $\mathrm{v} / \mathrm{c}$ ratio at the northbound approach is approaching the threshold.

By the 2028 and 2033 horizon years without development during the PM peak period, the Rothesay Avenue / Ashburn Lake Road intersection is projected to operate at an overall LOS E or better with an intersection delay of 68 seconds/vehicle. The northbound approach is projected to operate at acceptable LOS or better, however, the $\mathrm{v} / \mathrm{c}$ ratio exceeds the threshold during both horizon years, indicating that the demand exceeds the capacity. The eastbound approach v/c ratio is approaching the threshold during both horizon years.

Operational deficiencies are projected for the Rothesay Avenue / Ashburn Lake Road intersection by 2028 without development at the northbound movement during the PM peak period.

Table 6 - LOS Summary for Rothesay Ave/Ashburn Lake Rd without Development

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOSAverage Delay (seconds per vehicle)$[95 \%$ Queues (m)] |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  | Westbound |  |  | Northbound |  | Southbound |  |  |
|  |  |  |  | Ashburn Lake Rd |  |  |  |  | Rothesay Ave |  | Rothesay Ave |  |  |
|  |  |  |  |  |  | $\frac{1}{4}$ |  | $\stackrel{R}{\mathrm{R}}$ |  | $\xrightarrow{\mathrm{R}}$ | 4 |  | R |
| Existing (2016) Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave @ Ashburn Lake |  | AM Peak | $\begin{gathered} \text { B } \\ 10 \end{gathered}$ | $\begin{gathered} \hline B \\ 13 \\ {[0.42]} \end{gathered}$ | shared |  |  |  |   <br> shared  <br>  9 <br>  $[0.28]$ |  |  | $A$ 10 $[0.54]$ | shared |
|  |  | PM Peak | $\begin{gathered} \text { B } \\ 20 \end{gathered}$ | $\begin{gathered} \hline \hline \text { C } \\ 26 \\ {[0.77]} \end{gathered}$ | shared |  |  |  |   <br> shared  <br>  $B$ <br>  19 <br>  $[0.81]$ |  |  | $\begin{gathered} \hline \hline \text { B } \\ 17 \\ {[0.56]} \\ \hline \end{gathered}$ | shared |
|  |  | Sat Peak | $\begin{gathered} B \\ 13 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 20 \\ {[0.65]} \\ \hline \end{gathered}$ | shared |  |  |  |   <br> shared $B$ <br>  10 <br>  $[0.41]$ |  |  | $\begin{gathered} \hline B \\ 12 \\ {[0.45]} \\ \hline \end{gathered}$ | shared |
| Projected 2023 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave @ Ashburn Lake |  | AM Peak | $\begin{gathered} B \\ 11 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 16 \\ {[0.56]} \\ \hline \end{gathered}$ | shared |  |  |  |   <br> shared  <br>  9 <br>  $[0.31]$ |  |  | $\begin{gathered} \hline B \\ 10 \\ {[0.58]} \\ \hline \end{gathered}$ | shared |
|  |  | PM Peak | $\begin{gathered} \text { C } \\ 33 \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 31 \\ {[0.83]} \\ \hline \hline \end{gathered}$ | shared |  |  |  |   <br> shared C <br>  30 <br>  $[0.92]$ |  |  | D 37 $[0.60]$ | shared |
|  |  | Sat Peak | $\begin{gathered} B \\ 15 \end{gathered}$ | $C$ 22 $[0.70]$ | shared |  |  |  |   <br> shared $\left[\begin{array}{c}B \\ \\ \\ \\ {[0.44]}\end{array}\right]$ |  |  | $\begin{gathered} \hline \hline B \\ 15 \\ {[0.48]} \\ \hline \end{gathered}$ | shared |
| Projected 2028 Horizon Year Conditions Without Development |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave @ Ashburn Lake |  | AM Peak | $\begin{gathered} B \\ 12 \end{gathered}$ | $\begin{gathered} \text { B } \\ 17 \\ {[0.59]} \\ \hline \end{gathered}$ | shared |  |  |  |   <br> shared A <br>  10 <br>  $[0.33]$ |  |  | $\begin{gathered} \hline \text { B } \\ 11 \\ {[0.61]} \\ \hline \end{gathered}$ | shared |
|  |  | PM Peak | $\begin{gathered} \mathrm{D} \\ 53 \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 43 \\ {[0.87]} \end{gathered}$ | shared |  |  |  |   <br> shared D <br>  50 <br>  $[1.00]$ |  |  | $E$ 61 $[0.63]$ | shared |
|  |  | Sat Peak | $\begin{gathered} B \\ 18 \end{gathered}$ | $C$ 24 $[0.74]$ | shared |  |  |  |   <br> shared $B$ <br>  11 <br>  $[0.46]$ |  |  | $C$ 22 $[0.51]$ | shared |
| Projected 2033 Horizon Year Conditions Without Development |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave @ Ashburn Lake |  | AM Peak | $\begin{gathered} B \\ 12 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 18 \\ {[0.62]} \\ \hline \hline \end{gathered}$ | shared |  |  |  |   <br> shared A <br>  10 <br>  $[0.36]$ |  |  | $\begin{gathered} \hline B \\ 12 \\ {[0.64]} \\ \hline \hline \end{gathered}$ | shared |
|  |  | PM Peak | $\begin{gathered} E \\ 68 \end{gathered}$ | $E$ 59 $[0.91]$ | shared |  |  |  |   <br> shared E <br>  78 <br>  $[1.09]$ |  |  | $\begin{gathered} \hline E \\ 61 \\ {[0.67]} \\ \hline \end{gathered}$ | shared |
|  |  | Sat Peak | $\begin{gathered} \mathrm{C} \\ 25 \end{gathered}$ |  | shared |  |  |  |   <br> shared B <br>  11 <br>  $[0.49]$ |  |  | D 36 $[0.54]$ | shared |

### 3.2.6 Rothesay Road / Fulton Lane

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 7 for the Rothesay Road / Fulton Lane intersection. The analysis output can be found in Appendix B.

The Rothesay Road / Fulton Lane intersection is operating at an overall excellent LOS A and an intersection delay of 0 seconds/vehicle during the AM, PM, and Saturday peak period. The southbound movement is operating at LOS A with an average delay of 10 seconds/vehicle or less during the AM, PM, and Saturday peak period. The westbound movement is operating at a good LOS B with an average delay of 13 seconds/vehicle or less during the AM and Saturday peak periods and at a satisfactory LOS D with an average delay of 26 seconds/vehicle during the PM peak period. The $95^{\text {th }}$ percentile queue lengths are 1 vehicle at all approaches and the $\mathrm{v} / \mathrm{c}$ ratios are 0.06 or less at all approaches.

Minimal changes are projected at the Rothesay Road / Fulton Lane intersection by the 2023 and 2028 horizon year. By the 2033 horizon year, the westbound movement during the PM peak period is projected to operate at an acceptable LOS E with an average delay of 48 seconds/vehicle and a v/c ratio of 0.12 . The $95^{\text {th }}$ percentile queue length at this approach is projected to be 1 vehicle.

## No operational deficiencies are projected at the Rothesay Road / Fulton Lane intersection by 2033 without development.

Table 7 - LOS Summary for Rothesay Rd/Fulton Ln without Development


### 3.2.7 Ashburn Road / Jones Drive

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 8 for the Ashburn Road / Jones Drive intersection. The analysis output can be found in Appendix B.

The Ashburn Road / Jones Drive intersection is operating at an overall excellent LOS A with virtually no overall intersection delay during all three peak periods. All individual movements are operating at LOS B or better with average delays of 14 seconds/vehicle or less during the AM, PM, and Saturday peak periods. All v/c ratios are 0.01 or lower.
By the 2033 horizon year, the eastbound movement of the Ashburn Road / Jones Drive intersection is projected to operate at LOS C with an average delay of 16 seconds/vehicle. Minimal queueing is
projected at this approach. No other major changes are projected during the AM, PM, or Saturday peak period.

No operational deficiencies are projected at the Ashburn Road / Jones Drive intersection by 2033 without development.

Table 8 - LOS Summary for Ashburn Rd/Jones Dr without Development

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Eastbound |  | Westbound |  |  | Northbound |  | Southbound |  |  |
| North South Street | Traffic | Time Period |  | Jones Dr |  |  |  |  | Ashburn |  |  | Ashburn R |  |
| @ East West Street | Control |  |  | $4$ | $\stackrel{R}{\mathrm{R}}$ | 4 | ${ }^{\text {A }}$ | $\xrightarrow{R}$ | L $\mathbf{T}$ | $\stackrel{R}{\mathrm{R}}$ | $4$ |  | $\stackrel{R}{\mathrm{R}}$ |
| Existing (2016) Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Jones Dr | STOP | AM Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \mathrm{A} \\ 10 \\ {[0.01]} \\ \hline \end{gathered}$ | shared |  |  |  | $\begin{array}{lc} \hline & A \\ \text { shared } & 8 \\ & {[0.00]} \\ \hline \hline \end{array}$ |  |  | free flow | shared |
|  |  | PM Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} B \\ 14 \\ {[0.01]} \end{gathered}$ | shared |  |  |  |   <br>  $A$ <br> shared 8 <br>  $[0.00]$ <br>   |  |  | free flow | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \text { A } \\ 10 \\ {[0.01]} \end{gathered}$ | shared |  |  |  |   <br> shared A <br>  7 <br>  $[0.00]$ |  |  | free flow | shared |
| Projected 2023 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Jones Dr | STOP | AM Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \text { A } \\ 10 \\ {[0.01]} \\ \hline \end{gathered}$ | shared |  |  |  | $\begin{array}{cc} \hline & A \\ \text { shared } & 8 \\ & {[0.00]} \\ \hline \hline \end{array}$ |  |  | free flow | shared |
|  |  | PM Peak | $\begin{aligned} & A \\ & 0 \end{aligned}$ | $\begin{gathered} \mathrm{B} \\ 15 \\ {[0.01]} \end{gathered}$ | shared |  |  |  |   <br>  $A$ <br> shared 8 <br>  $[0.00]$ |  |  | free flow | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \mathrm{A} \\ 10 \\ {[0.01]} \end{gathered}$ | shared |  |  |  |   <br> shared A <br>  $[0.00]$ <br>   <br>   |  |  | free flow | shared |
| Projected 2028 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Jones Dr |  | AM Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \text { A } \\ 10 \\ {[0.01]} \\ \hline \end{gathered}$ | shared |  |  |  |   <br> shared $A$ <br>  8 <br>  $[0.00]$ |  |  | free flow | shared |
|  |  | PM Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \mathrm{C} \\ 15 \\ {[0.01]} \\ \hline \end{gathered}$ | shared |  |  |  |   <br> shared $A$ <br>  8 <br>  $[0.00]$ |  |  | free flow | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \mathrm{A} \\ 10 \\ {[0.01]} \end{gathered}$ | shared |  |  |  | $\begin{array}{lc} \hline \hline & A \\ \text { shared } & 7 \\ & {[0.00]} \\ \hline \end{array}$ |  |  | free flow | shared |
| Projected 2033 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Jones Dr | STOP | AM Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} B \\ 10 \\ {[0.01]} \\ \hline \end{gathered}$ | shared |  |  |  |   <br> shared A <br>  8 <br>  $[0.00]$ |  |  | free flow | shared |
|  |  | PM Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \mathrm{C} \\ 16 \\ {[0.01]} \\ \hline \end{gathered}$ | shared |  |  |  |   <br> shared $A$ <br>  8 <br>  $[0.00]$ |  |  | free flow | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} \hline B \\ 10 \\ {[0.01]} \end{gathered}$ | shared |  |  |  |   <br> shared A <br>  $[0.00]$ |  |  | free flow | shared |

### 3.2.8 Ashburn Road / Drury Cove Road

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 9 for the Ashburn Road / Drury Cove Road intersection. The analysis output can be found in Appendix B.

Under existing conditions, the Ashburn Road / Drury Cove Road intersection is operating at an overall LOS A with an average intersection delay of 1 seconds/vehicle during both the AM, PM, and Saturday peak period. The eastbound movement is operating at an excellent LOS A with an average delay of 8 seconds/vehicle during the AM and PM peak period; there are no left-turning vehicles at this approach during the Saturday peak period, therefore, this movement experiences free flow. The southbound approach is operating at a very good LOS B with an average delay of 10 seconds/vehicle during the AM and Saturday peak period and at a good LOS C with an average delay of 15 seconds/vehicle during the PM peak period. All $95^{\text {th }}$ percentile queue lengths are 1 vehicle during all
three peak periods. Minimal changes are projected by the 2023, 2028, and 2033 horizon years without the development in place.

No operational deficiencies are projected for the Ashburn Road / Drury Cover Road by the 2023, 2028, and 2033 horizon years without the development in place.

Table 9 - LOS Summary for Ashburn Rd/Drury Cover Rd without Development

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street <br> @ East West Street | Traffic Control | Time Period |  | Eastbound Ashburn Rd |  |  | Westbound Ashburn Rd |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  |  |  |  |  |  |  |  | Cove |  |
|  |  |  |  | $4$ | ${ }^{\top}$ | $\xrightarrow{\mathrm{R}}$ |  |  |  |  | 4 | $\mathbf{T}^{\mathbf{T}}$ | $\xrightarrow{R}$ |  | ${ }^{\text {T }}$ | $\xrightarrow{R}$ |
| Existing (2016) Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Drury Cove Rd @ Ashburn Rd | STOP | AM Peak | $\begin{aligned} & \text { A } \\ & 1 \end{aligned}$ | $\begin{gathered} \hline \text { A } \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} B \\ 10 \\ {[0.02]} \\ \hline \end{gathered}$ |  | shared |
|  |  | PM Peak | $\begin{aligned} & A \\ & 1 \end{aligned}$ | $\begin{gathered} \hline \mathbf{A} \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} C \\ 15 \\ {[0.08]} \\ \hline \end{gathered}$ |  | shared |
|  |  | Sat Peak | $\begin{aligned} & A \\ & 1 \end{aligned}$ | $\begin{gathered} \mathrm{A} \\ 0 \\ {[0.00]} \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} B \\ 10 \\ {[0.02]} \end{gathered}$ |  | shared |
| Projected 2023 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Drury Cove Rd @ Ashburn Rd | STOP | AM Peak | $\begin{aligned} & \text { A } \\ & 1 \end{aligned}$ | $\begin{gathered} \hline \text { A } \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} \hline B \\ 11 \\ {[0.03]} \\ \hline \end{gathered}$ |  | shared |
|  |  | PM Peak | $\begin{aligned} & A \\ & 1 \end{aligned}$ | $\begin{gathered} \hline \mathbf{A} \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} C \\ 16 \\ {[0.09]} \\ \hline \end{gathered}$ |  | shared |
|  |  | Sat Peak | $\begin{aligned} & A \\ & 1 \end{aligned}$ | $\begin{gathered} \mathrm{A} \\ 0 \\ {[0.00]} \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} \hline B \\ 10 \\ {[0.02]} \end{gathered}$ |  | shared |
| Projected 2028 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Drury Cove Rd @ Ashburn Rd | STOP | AM Peak | $\begin{gathered} A \\ 1 \end{gathered}$ | $\begin{gathered} \hline A \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} \hline B \\ 11 \\ {[0.03]} \end{gathered}$ |  | shared |
|  |  | PM Peak | $\begin{gathered} A \\ 1 \end{gathered}$ | $\begin{gathered} \text { A } \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} \text { C } \\ 17 \\ {[0.09]} \end{gathered}$ |  | shared |
|  |  | Sat Peak | $\begin{aligned} & A \\ & 1 \end{aligned}$ | $\begin{gathered} \mathrm{A} \\ 0 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} \mathrm{B} \\ 10 \\ {[0.02]} \end{gathered}$ |  | shared |
| Projected 2033 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Drury Cove Rd @ Ashburn Rd | STOP | AM Peak | $\begin{aligned} & \text { A } \\ & 1 \end{aligned}$ | $\begin{gathered} \text { A } \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} \mathrm{B} \\ 11 \\ {[0.03]} \\ \hline \end{gathered}$ |  | shared |
|  |  | PM Peak | $\begin{aligned} & A \\ & 1 \end{aligned}$ | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} C \\ 18 \\ {[0.10]} \\ \hline \end{gathered}$ |  | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 1 \end{aligned}$ | $\begin{gathered} \mathrm{A} \\ 0 \\ {[0.00]} \end{gathered}$ | shared |  |  | free flow |  |  |  | $\begin{gathered} B \\ 10 \\ {[0.02]} \end{gathered}$ |  | shared |

### 3.2.9 Rothesay Avenue / Rothesay Road

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 10 for the Rothesay Road / Rothesay Avenue intersection. The analysis output can be found in Appendix B.

Under existing conditions, the Rothesay Road / Rothesay Avenue intersection is operating at unacceptable LOS F with intersection delays of 64 seconds/vehicle, 129 seconds/vehicle, and 51 seconds/vehicle during the AM, PM, and Saturday peak period. The westbound approach is experiencing the highest delays, which is operating at LOS F with average delays from 107 seconds/vehicle to 407 seconds/vehicle during the AM, PM, and Saturday peak period. The westbound approach also has $\mathrm{v} / \mathrm{c}$ ratios that exceed 1.0 during all three peak periods, indicating that the volumes at this approach exceed the capacity. The southbound left-turn movement operates at LOS B or better with average delays of 10 seconds/vehicle or less and $\mathrm{v} / \mathrm{c}$ ratios of 0.40 or less during all three peak periods.

Table 10 - LOS Summary for Rothesay Rd/Rothesay Ave without Development

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street <br> @ East West Street | Traffic Control | Time Period |  | Eastbound |  | Westbound | Northbound |  | Southbound |  |  |
|  |  |  |  |  |  | esay Ave |  | Rothesay Rd |  | Rothesay Rd |  |
|  |  |  |  |  | $\xrightarrow{R} \quad \stackrel{L}{4}$ |  |  |  |  | ${ }^{\mathbf{T}}$ | $\xrightarrow{\mathrm{R}}$ |
| Existing (2016) Conditions |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Rothesay Ave | STOP | AM Peak | $\begin{gathered} F \\ 64 \end{gathered}$ |  | $F$ 241 $[1.39]$ | shared |  | free flow shared | $\begin{gathered} \text { A } \\ 8 \\ {[0.23]} \end{gathered}$ | free flow |  |
|  |  | PM Peak | $\begin{gathered} F \\ 129 \end{gathered}$ |  | $\begin{gathered} \hline \text { F } \\ 407 \\ {[1.80]} \\ \hline \end{gathered}$ | shared |  | free flow shared | $\begin{gathered} \mathrm{B} \\ 10 \\ {[0.40]} \\ \hline \end{gathered}$ | free flow |  |
|  |  | Sat Peak | $\begin{gathered} F \\ 51 \end{gathered}$ |  | $\begin{gathered} \hline F \\ 107 \\ {[1.10} \end{gathered}$ | shared |  | free flow shared | $\begin{gathered} \text { A } \\ 8 \\ {[0.21]} \end{gathered}$ | free flow |  |
| Projected 2023 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Rothesay Ave | STOP | AM Peak | $\begin{gathered} F \\ 100 \end{gathered}$ |  | $\begin{gathered} \text { F } \\ 385 \\ {[1.72]} \\ \hline \end{gathered}$ | shared |  | free flow shared | $\begin{gathered} \text { A } \\ 8 \\ {[0.25]} \\ \hline \end{gathered}$ | free flow |  |
|  |  | PM Peak | $\begin{gathered} F \\ 226 \end{gathered}$ |  | $\begin{gathered} \hline F \\ 718 \\ {[2.49]} \\ \hline \end{gathered}$ | shared |  | free flow shared | $\begin{gathered} \mathrm{B} \\ 11 \\ {[0.47]} \\ \hline \end{gathered}$ | free flow |  |
|  |  | Sat Peak | $\begin{gathered} \text { F } \\ 57 \end{gathered}$ |  | $\begin{gathered} \mathrm{F} \\ 149 \\ {[1.22]} \end{gathered}$ | shared |  | free flow shared | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.21]} \end{gathered}$ | free flow |  |
| Projected 2028 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Rothesay Ave |  | AM Peak | $\begin{gathered} F \\ 135 \end{gathered}$ |  | $\begin{gathered} F \\ 522 \\ {[2.02]} \end{gathered}$ | shared |  | free flow shared | $\begin{gathered} \text { A } \\ 8 \\ {[0.26]} \end{gathered}$ | free flow |  |
|  |  | PM Peak | $\begin{gathered} F \\ 310 \end{gathered}$ |  | $F$ 992 $[3.09]$ | shared |  | free flow shared | $\begin{gathered} \text { B } \\ 12 \\ {[0.51]} \\ \hline \end{gathered}$ | free flow |  |
|  |  | Sat Peak | $\begin{gathered} F \\ 85 \end{gathered}$ |  | $\begin{gathered} \hline F \\ 162 \\ {[1.25]} \end{gathered}$ | shared |  | free flow shared | $\begin{gathered} \hline \mathrm{A} \\ 8 \\ {[0.22]} \end{gathered}$ | free flow |  |
| Projected (YEAR) Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Rothesay Ave | STOP | AM Peak | $\begin{gathered} F \\ 178 \end{gathered}$ |  | $F$ 691 $[2.39]$ | shared |  | free flow shared | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.28]} \\ \hline \end{gathered}$ | free flow |  |
|  |  | PM Peak | $\begin{gathered} F \\ 411 \end{gathered}$ |  | $\begin{gathered} \hline \mathbf{F} \\ 1317 \\ {[3.79]} \end{gathered}$ | shared |  | free flow shared | $\begin{gathered} \mathrm{B} \\ 13 \\ {[0.54]} \\ \hline \end{gathered}$ | free flow |  |
|  |  | Sat Peak | $\begin{gathered} F \\ 151 \end{gathered}$ |  | $\begin{gathered} \mathrm{F} \\ 231 \\ {[1.42]} \end{gathered}$ | shared |  | free flow shared | A 8 $[0.22]$ | free flow |  |

By the 2023, 2028, and 2033 horizon years the Rothesay Road / Rothesay Avenue intersection is projected to continue to get worse overall in terms of LOS with intersection delays of 226 seconds/vehicle or less by 2023, intersection delays of 310 seconds/vehicle or less by 2028, intersection delays of 411 seconds/vehicle or less by 2028. The southbound approach is projected to have minimal changes by 2033. The westbound approach, however, is projected to continue to get worse in terms of average delays. By 2023 the westbound approach is projected to operate at LOS with an average delay of 718 seconds/vehicle or less, by 2028 the average delay on the westbound approach is projected to be 992 seconds/vehicle or less, and by 2033 the average delay on the westbound approach is projected to be 1317 seconds/vehicle or less.

Operational deficiencies are currently experienced at the Rothesay Road / Rothesay Avenue intersection overall and particularly at the westbound approach. Operational deficiencies are projected to get worse by the 2033 horizon year without the development in place.

### 3.2.10 Rothesay Road / Ashburn Road

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 11 for the Rothesay Road / Ashburn Road intersection. The analysis output can be found in Appendix B.

Under existing conditions, the Rothesay Road / Ashburn Road intersection is operating at an overall LOS B or better with an intersection delay of 10 seconds/vehicle or less during the AM, PM, and Saturday peak period. The eastbound left turn and right turn movements are both operating at LOS C or better with average delays of 23 seconds/vehicle or less during all three peak periods. The westbound movement during the PM peak period is operating at LOS C (average delay of 20 seconds/vehicle). The westbound approach (parking lot exit) had no vehicles present during the AM and Saturday peak period. The $95^{\text {th }}$ percentile queue lengths are 6 vehicles or less and at each approach during the AM, PM, and Saturday peak period. The v/c ratios are 0.66 or less indicating there is sufficient capacity.

Table 11 - LOS Summary for Rothesay Rd/Ashburn Rd without Development

| Intersection |  |  | Overall <br>  <br> Delay <br> (sec/veh) | Turning Movements LOS Average Delay (seconds per vehicle) [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street <br> @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Ashburn Rd |  |  | Ashburn Rd |  |  | Rothesay Rd |  |  | Rothesay Rd |  |  |
|  |  |  |  |  |  | R |  |  |  |  |  | R | $\xrightarrow{4}$ |  |  |
| Existing (2016) Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Ashburn Rd | STOP | AM Peak | $\begin{aligned} & \text { A } \\ & 4 \end{aligned}$ | $\begin{gathered} C \\ 16 \\ {[0.07]} \end{gathered}$ |  | $\begin{gathered} B \\ 12 \\ {[0.26]} \\ \hline \end{gathered}$ |  |  |  | shared | $\begin{gathered} \mathrm{A} \\ 9 \\ {[0.10]} \\ \hline \end{gathered}$ |  |  | free flow | shared |
|  |  | PM Peak | $\begin{gathered} \text { B } \\ 10 \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ 23 \\ {[0.36]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} C \\ 17 \\ {[0.66]} \\ \hline \end{gathered}$ | shared | $C$ 20 $[0.01]$ | shared | shared | $\begin{gathered} \hline \mathrm{A} \\ 8 \\ {[0.09]} \\ \hline \end{gathered}$ |  |  | free flow | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 4 \end{aligned}$ | $\begin{gathered} \hline B \\ 13 \\ {[0.10]} \end{gathered}$ |  | $\begin{gathered} \text { B } \\ 10 \\ {[0.20]} \end{gathered}$ |  |  |  | shared | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.05]} \end{gathered}$ |  |  | free flow | shared |
| Projected 2023 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Ashburn Rd | STOP | AM Peak | $\begin{gathered} \text { A } \\ 5 \end{gathered}$ | $\begin{gathered} C \\ 17 \\ {[0.08]} \end{gathered}$ |  | $\begin{gathered} B \\ 13 \\ {[0.29]} \end{gathered}$ |  |  |  | shared | $\begin{gathered} \text { A } \\ 9 \\ {[0.11]} \\ \hline \end{gathered}$ |  |  | free flow | shared |
|  |  | PM Peak | $\begin{gathered} B \\ 12 \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 26 \\ {[0.43]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \mathrm{C} \\ 19 \\ {[0.72]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \hline \mathrm{C} \\ 24 \\ {[0.02]} \\ \hline \end{gathered}$ | shared | shared | $\begin{gathered} \hline A \\ 8 \\ {[0.10]} \\ \hline \end{gathered}$ |  |  | free flow | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 5 \end{aligned}$ | $\begin{gathered} \mathrm{B} \\ 13 \\ {[0.12]} \\ \hline \end{gathered}$ |  | $\begin{gathered} \mathrm{B} \\ 10 \\ {[0.21]} \end{gathered}$ |  |  |  | shared | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.05]} \\ \hline \end{gathered}$ |  |  | free flow | shared |
| Projected 2028 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Ashburn Rd | STOP | AM Peak | $\begin{gathered} \text { A } \\ 5 \end{gathered}$ | $\begin{gathered} C \\ 17 \\ {[0.09]} \\ \hline \end{gathered}$ |  | $\begin{gathered} \text { B } \\ 13 \\ {[0.31]} \\ \hline \end{gathered}$ |  |  |  | shared | $\begin{gathered} \mathrm{A} \\ 9 \\ {[0.12]} \\ \hline \end{gathered}$ |  |  | free flow | shared |
|  |  | PM Peak | $\begin{gathered} B \\ 13 \end{gathered}$ | $\begin{gathered} \hline D \\ 30 \\ {[0.48]} \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{C} \\ 11 \\ {[0.77]} \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{D} \\ 28 \\ {[0.02]} \end{gathered}$ | shared | shared | $\begin{gathered} \mathrm{A} \\ 8 \\ 8 \\ {[0.11]} \end{gathered}$ |  |  | free flow | shared |
|  |  | Sat Peak | $\begin{gathered} \text { A } \\ 5 \end{gathered}$ | $\begin{gathered} B \\ 14 \\ {[0.13]} \end{gathered}$ |  | $\begin{gathered} \mathrm{B} \\ 11 \\ {[0.23]} \end{gathered}$ |  |  |  | shared | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.05]} \end{gathered}$ |  |  | free flow | shared |
| Projected 2033 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Ashburn Rd | STOP | AM Peak | $\begin{gathered} \text { A } \\ 5 \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ 18 \\ {[0.10]} \end{gathered}$ |  | $\begin{gathered} \hline B \\ 14 \\ {[0.33]} \\ \hline \end{gathered}$ |  |  |  | shared | $\begin{gathered} \mathrm{A} \\ 9 \\ {[0.13]} \\ \hline \end{gathered}$ |  |  | free flow | shared |
|  |  | PM Peak | $\begin{gathered} C \\ 15 \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 35 \\ {[0.54]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{D} \\ 25 \\ {[0.82]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{E} \\ 35 \\ {[0.03]} \\ \hline \end{gathered}$ | shared | shared | $\begin{gathered} \mathrm{A} \\ 8 \\ 8 \\ {[0.11]} \end{gathered}$ |  |  | free flow | shared |
|  |  | Sat Peak | $\begin{gathered} \text { A } \\ 5 \end{gathered}$ | $\begin{gathered} B \\ 14 \\ {[0.14]} \end{gathered}$ |  | $\begin{gathered} B \\ 11 \\ {[0.24]} \end{gathered}$ |  |  |  | shared | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.06]} \\ \hline \end{gathered}$ |  |  | free flow | shared |

Minimal changes are projected at the Rothesay Road / Ashburn Road intersection during the AM and Saturday peak period by the 2023, 2028, and 2033 horizon years without the development in place.

By the 2023, 2028, and 2033 horizon years without development during the PM peak period, the Rothesay Road / Ashburn Road intersection is projected to operate at LOS C or better with an intersection delay of 15 seconds/vehicle or less. The eastbound left turn movement is projected to operate at LOS D with an average delay of 35 seconds/vehicle or less. The eastbound right turn movement is projected to operate at LOS D or better with an average delay of 25 seconds/vehicle or less. The westbound movement is projected to operate at LOS E or better with an average delay of 35 seconds/vehicle or less. All v/c ratios are projected to be 0.82 or less, indicating that demand is
approaching capacity. The $95^{\text {th }}$ percentile queue lengths are projected to be 10 vehicles or less, with the longest queues projected on the eastbound right turn lane.

No operational deficiencies are projected at the Rothesay Road / Ashburn Road intersection by the 2033 horizon year without development.

### 3.2.11 Rothesay Avenue / NB Route 1 interchange

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 12 for the Rothesay Avenue / Route 1 off-ramp, Table 13 for the Rothesay Avenue / Route 1 on-ramp (furthest west), and Table 14 for the Rothesay Avenue / Route 1 on-ramp (furthest east). The analysis output can be found in Appendix B.

### 3.2.11.1 Rothesay Avenue / Route 1 off-ramp Intersection

Under existing conditions. the Rothesay Avenue / Route 1 off-ramp intersection is operating at an unacceptable LOS F with an intersection delay of 52 seconds/vehicle and 92 seconds/vehicle during the AM and Saturday peak periods, respectively. The eastbound and westbound movements are both operating at unacceptable LOS F with an average delay of 248 seconds/vehicle or less during the Am and Saturday peak periods. During the AM and Saturday peak periods, the v/c ratios at these approaches are all approaching or exceeding 1.0, indicating the demand is approaching or exceeding capacity.

During the PM peak period the intersection is operating at good LOS C with an intersection delay of 21 seconds/vehicle. The individual movements are operating at LOS D or better with average delays of 28 seconds/vehicle or less. The $\mathrm{v} / \mathrm{c}$ ratios are all 0.78 or less, indicating that there is sufficient capacity.

By the 2023, 2028, and 2033 horizon years during the AM and Saturday peak period, the Rothesay Avenue / Route 1 off-ramp is projected to operate at LOS F with an intersection delay of 214 seconds/vehicle or less. The individual movements are all projected to operate at LOS F with average delays of 529 seconds/vehicle or less during the AM and Saturday peak period. The v/c ratios are all projected to exceed 1.0 , indicating that the demand exceeds the capacity.

During the PM peak period, the Rothesay Avenue / Route 1 off-ramp intersection is projected to operate at an overall LOS D with an intersection delay of 34 seconds/vehicle or less by the 2023 and 2028 horizon year. The eastbound and westbound approaches are projected to operate at LOS E or better with an average delay of 39 seconds/vehicle or less and LOS E with an average delay of 46 seconds/vehicle or less, respectively. By the 2033 horizon year, the intersection is projected to operate at an acceptable LOS E with an average delay of 44 seconds/vehicle during the PM peak period. The eastbound and westbound approaches are projected to operate at LOS F with average delays of 109 seconds/vehicle or less. The v/c ratios at the eastbound and westbound approaches are approaching 1.0, indicating that the demand is approaching the capacity of these approaches.

Table 12 - LOS Summary for Rothesay Ave/Rte 1 off-ramp without Development

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  | Westbound |  | Northbound |  |  | Southbound |  |
|  |  |  |  | Rothesay Ave (towards on-ramp) |  | Rothesay Ave |  |  |  |  |  | off-ramp |
|  |  |  |  |  | R |  | R | $4$ | ${ }^{\mathbf{T}}$ | R | $4$ | $\stackrel{T}{\mathbf{T}}$ |
| Existing (2016) Conditions |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave/Rte 1 Offramp @ Rothesay Ave | STOP | AM Peak | $\begin{gathered} F \\ 52 \end{gathered}$ | $\begin{gathered} \hline F \\ 134 \\ {[1.17]} \\ \hline \end{gathered}$ | shared | $F$ 80 $[0.96]$ |  |  |  |  |  | free flow |
|  |  | PM Peak | $\begin{gathered} C \\ 21 \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 25 \\ {[0.77]} \\ \hline \end{gathered}$ | shared | D 28 $[0.78]$ |  |  |  |  |  | free flow |
|  |  | Sat Peak | $\begin{gathered} F \\ 92 \end{gathered}$ | F 92 $[1.04]$ | shared | $\begin{gathered} \hline F \\ 248 \\ {[1.45]} \end{gathered}$ |  |  |  |  |  | free flow |
| Projected 2023 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave/Rte 1 Offramp @ Rothesay Ave | STOP | AM Peak | $\begin{gathered} F \\ 81 \end{gathered}$ | $\begin{gathered} \text { F } \\ 206 \\ {[1.35]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline F \\ 128 \\ {[1.12]} \\ \hline \end{gathered}$ |  |  |  |  |  | free flow |
|  |  | PM Peak | $\begin{gathered} \text { D } \\ 27 \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 31 \\ {[0.84]} \end{gathered}$ | shared | $\begin{gathered} \hline E \\ 36 \\ {[0.86]} \end{gathered}$ |  |  |  |  |  | free flow |
|  |  | Sat Peak | $\begin{gathered} F \\ 132 \end{gathered}$ | $\begin{gathered} \hline F \\ 150 \\ {[1.21]} \end{gathered}$ | shared | $\begin{gathered} \hline F \\ 345 \\ {[1.67]} \end{gathered}$ |  |  |  |  |  | free flow |
| Projected 2028 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave/Rte 1 Offramp @ Rothesay Ave | STOP | AM Peak | $\begin{gathered} F \\ 109 \end{gathered}$ | $\begin{gathered} \hline F \\ 275 \\ {[1.51]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline F \\ 177 \\ {[1.25]} \\ \hline \end{gathered}$ |  |  |  |  |  | free flow |
|  |  | PM Peak | $\begin{gathered} \text { D } \\ 34 \end{gathered}$ | $\begin{gathered} \hline E \\ 39 \\ {[0.90]} \\ \hline \end{gathered}$ | shared | $E$ 46 $[0.92]$ |  |  |  |  |  | free flow |
|  |  | Sat Peak | $\begin{gathered} F \\ 151 \end{gathered}$ | F 204 $[1.34]$ | shared | $F$ 430 $[1.86]$ |  |  |  |  |  | free flow |
| Projected 2033 Horizon Year without Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave/Rte 1 Offramp @ Rothesay Ave | STOP | AM Peak | $\begin{gathered} F \\ 143 \end{gathered}$ | $\begin{gathered} \hline F \\ 353 \\ {[1.69]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} F \\ 240 \\ {[1.40]} \\ \hline \end{gathered}$ |  |  |  |  |  | free flow |
|  |  | PM Peak | $\begin{gathered} E \\ 44 \end{gathered}$ | $\begin{gathered} \hline F \\ 107 \\ {[0.96]} \\ \hline \hline \end{gathered}$ | shared | $\begin{gathered} \hline F \\ 109 \\ {[0.99]} \\ \hline \hline \end{gathered}$ |  |  |  |  |  | free flow |
|  |  | Sat Peak | $\begin{gathered} F \\ 214 \end{gathered}$ | F 269 $[1.49]$ | shared | F 529 $[2.08]$ |  |  |  |  |  | free flow |

Operational deficiencies are currently experienced at the Rothesay Avenue / Route 1 off-ramp during the AM and Saturday peak period at both the eastbound and westbound approaches and are projected to be experienced during the PM peak period at the eastbound and westbound approaches by the 2033 horizon year without the development in place.

### 3.2.11.2 Rothesay Avenue / Route 1 on-ramp Intersections

Both of the Rothesay Avenue / Route 1 on-ramp (eastbound street) intersections are operating at LOS A with an intersection delay of 5 seconds/vehicle or better during the AM, PM, and Saturday peak period. Each individual movement (northbound and eastbound) is operating at LOS C or better at both intersections with average delays of 19 seconds/vehicle or less during both the AM, PM, and Saturday peak periods. All the $\mathrm{v} / \mathrm{c}$ ratios are 0.46 or less, indicating there is sufficient capacity.

By the 2023, 2028, and 2033 horizon years without development, both the Rothesay Avenue / Route 1 on-ramp intersections are projected to operate at an overall LOS A with intersection delays of 8 seconds/vehicle or less during all peak periods. Individual movements at both intersections are projected to operate at LOS D or better with an average delay of 26 seconds/vehicle or less during all peak periods. The $\mathrm{v} / \mathrm{c}$ ratios are all projected to be 0.62 or less, indicating that there is sufficient capacity.

No operational deficiencies are projected at the Rothesay Avenue / Route 1 on-ramp intersections by the 2033 horizon year without the development in place.

Table 13 - LOS Summary for Rothesay Ave/Rte 1 on-ramp (furthest west) without Development





Table 14 - LOS Summary for Rothesay Ave/Rte 1 on-ramp (furthest east) without Development


### 3.2.12 NB Route 1 Access with Rothesay Road / Rothesay Avenue

The LOS for existing and projected horizon years 2023, 2028, and 2033 traffic volumes for AM, PM, and Saturday peak hours without development are presented in Table 15 for the Rothesay Road Access Ramps to Route 1 and Table 16 for the Rothesay Avenue Access Ramps to Route 1. The analysis output can be found in Appendix B.

During the AM peak period, the Rothesay Road / Route $\mathbf{1}$ off-ramp is operating at LOS A ( 0.5 $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ density) and is projected to continue to operate at LOS A by the 2033 horizon year without development. The Rothesay Road on-ramp is operating at LOS D with a density of $18.3 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the AM peak period. The on-ramp is projected to continue to operate at LOS D (density of 20.7 $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ or less) during the 2023 and 2028 horizon years without development. By the 2033 horizon year, the on-ramp is projected to operate at an unacceptable LOS F ( $21.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ density) during the AM peak period.

During the PM peak period, the Rothesay Road / Route 1 off-ramp is currently operating at LOS C and is projected to continue operating at LOS C with an average density of $16.1 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ or lower by the 2033 horizon year without the development in place. The Rothesay Road / Route 1 on-ramp is currently operating at LOS B and is projected to continue operating at LOS B with an average density of $7.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ or lower by the 2033 horizon year without the development in place during the PM peak period.

The Rothesay Road / Route 1 on and off-ramps are currently operating at LOS A and are projected to continue operating at LOS A with an average density of $5.0 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ by the 2033 horizon year during the Saturday peak period without the development in place.

Operational deficiencies are projected at the Rothesay Road / Route 1 on-ramp during the AM peak period by 2033 horizon year without the development in place. No operational deficiencies are projected during the PM or Saturday peak periods.

Table 15 - LOS Summary for Rothesay Rd/Rt 1 Ramps without Development

|  | AM Peak | PM Peak | SAT Peak |
| :---: | :---: | :---: | :---: |
| Ramp | LOS Density ( $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ) | LOS Density ( $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ) | LOS Density ( $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ) |
| Existing (2016) Conditions |  |  |  |
| Rte 1 - Rothesay Rd off-ramp | $\mathrm{A}$ | $\mathrm{C}$ | $\begin{gathered} \mathrm{A} \\ 2.9 \end{gathered}$ |
|  | 0.5 |  |  |
| Rte 1 - Rothesay Rd | D | B | A |
| on-ramp | 18.3 | 6.2 | 4.2 |
| Projected 2023 Horizon Year Conditions without Development |  |  |  |
| Rte 1 - Rothesay Rd off-ramp | A | C | A |
|  | 0.7 | 14.3 | 3.2 |
| Rte 1 - Rothesay Rd on-ramp | D | B | A |
|  | 19.6 | 6.7 | 4.5 |
| Projected 2028 Horizon Year Conditions without Development |  |  |  |
| Rte 1 - Rothesay Rd off-ramp | A | C | A |
|  | 0.9 | 15.1 | 3.5 |
| Rte 1 - Rothesay Rd on-ramp | D | B | A |
|  | 20.7 | 7.0 | 4.8 |
| Projected 2033 Horizon Year Conditions without Development |  |  |  |
| Rte 1 - Rothesay Rd off-ramp | A | C | A |
|  | 1.1 | 16.1 | 3.7 |
| Rte 1 - Rothesay Rd on-ramp | F | B | A |
|  | 21.7 | 7.4 | 5.1 |

The Rothesay Avenue / Route $\mathbf{1}$ off-ramp is currently operating at LOS C during the AM peak period and LOS A during both the PM and Saturday peak period. By the 2023, 2028, and 2033 horizon years without the development in place, the off-ramp is projected to operate at LOS D or better with an average density of $18.1 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ or lower during the AM peak period and is continue to operate at LOS A (density of $1.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ or lower) during both the PM and Saturday peak periods.

The Rothesay Avenue / Route 1 on-ramp operating at LOS A (density of $5.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ), LOS D (density of $19.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ), and LOS B (density of $9.3 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ ) during the AM, PM, and Saturday peak periods, respectively. By the 2023, 2028, and 2033 horizon years without the development in place, the on-ramp is projected to operate at LOS B or better (density of $6.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ or lower) during the AM peak, LOS E or better (density of $22.9 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ or lower) during the PM peak period, and continue to operate at LOS B (density of $10.8 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ or lower) during the Saturday peak period.

No operational deficiencies are projected at the Rothesay Avenue / Route 1 access ramps by the $\mathbf{2 0 3 3}$ horizon year without the development in place.

Table 16 - LOS Summary for Rothesay Ave/Rte 1 Ramps without Development

|  | AM Peak | PM Peak | SAT Peak |
| :--- | :---: | :---: | :---: |
| Ramp | LOS <br> Density (pc/km/ln) | LOS <br> Density (pc/km/ln) | LOS <br> Density (pc/km/ln) |
| Existing (2016) Conditions |  |  |  |
| Rte 1 - Rothesay Ave <br> off-ramp | C | A | A |
| Rte 1 - Rothesay Ave <br> on-ramp | 15.0 | 3.7 | 1.2 |


| Projected 2023 Horizon Year Conditions without Development |  |  |  |
| :--- | :---: | :---: | :---: |
| Rte 1 - Rothesay Ave <br> off-ramp | C | A | A |
| Rte 1 - Rothesay Ave | 16.2 | 4.1 | 1.4 |
| on-ramp | A | D | B |

Projected 2028 Horizon Year Conditions without Development

| Rte 1 - Rothesay Ave | D | A | A |
| :--- | :---: | :---: | :---: |
| off-ramp | 17.1 | 4.4 | 1.5 |
| Rte 1 - Rothesay Ave | B | D | B |
| on-ramp | 6.1 | 21.9 | 10.4 |

Projected 2033 Horizon Year Conditions without Development

| Rte 1 - Rothesay Ave | D | A | A |
| :--- | :---: | :---: | :---: |
| off-ramp | 18.1 | 4.7 | 1.7 |
| Rte 1 - Rothesay Ave | B | E | B |
| on-ramp | 6.4 | 22.9 | 10.9 |

## 4 Trip Generation and Assignment

### 4.1 Trip Generation

In order to estimate the amount of traffic that will be generated at the new development site, trip generation rates were utilized for the proposed retail development. These rates are documented in the TripGen 2014 software and are based on the 9th edition of the Trip General Manual, published by the Institute of Transportation Engineers (ITE).

Table 17 shows the estimated traffic generation during of the development. The Table is sectioned based on which developments will be completed by the Phase 1, Phase 2, and Phase 3 horizon years. The AM, PM, and Saturday peak hours for the following components of the development are shown. Figure 10 shows a visual on the site plan of the anticipated phasing used in this study.

The proposed development is projected to generate significantly more traffic during the PM and Saturday peak periods. For this reason, only the PM and Saturday peak hours will be evaluated with respect to the traffic impacts associated with the proposed development, with the exception of the Route 1 ramps, which will be evaluated using the critical peak period based on the directional split for Route 1.

Table 17 - Trip Generation for Development

| Development | $\begin{aligned} & \text { Size } \\ & \left(m^{2}\right) \end{aligned}$ | AM Peak Hour |  |  | PM Peak Hour |  |  | Saturday Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | IN | OUT | TOTAL | IN | OUT | TOTAL | IN | OUT | TOTAL |
| Phase 1 (completed by 2023) |  |  |  |  |  |  |  |  |  |  |
| Highway Service Stop ITE Land Use \#950 | 2,415 | 110 | 102 | 212 | 184 | 170 | 354 | 184 | 170 | 354 |
| $\begin{gathered} \hline \text { FF-1 (fast food \& } \\ \text { drive thru) x3 } \\ \text { ITE Land Use } \\ \# 934 \\ \hline \end{gathered}$ | 1,059 | 264 | 254 | 518 | 193 | 179 | 372 | 343 | 330 | 673 |
| Outdoor Anchor ITE Land Use \#861 | 3,345 | 7 | 2 | 9 | 32 | 34 | 66 | 70 | 68 | 138 |
| Restaurant ITE Land Use \#932 | 520 | 34 | 27 | 61 | 21 | 10 | 31 | 42 | 37 | 79 |
| Garage ITE Land Use \#943 | 585 | 5 | 1 | 6 | 12 | 16 | 28 | 19 | 23 | 42 |
| Car Wash ITE Land Use \#947 | 223 | 4 | 1 | 5 | 17 | 17 | 34 | 17 | 17 | 34 |
| Convenience Retail <br> ITE Land Use \#852 | 1059 | 177 | 177 | 354 | 193 | 201 | 394 | 193 | 201 | 394 |
| $\begin{gathered} \hline \text { Museum/Tourist } \\ \text { Centre } \\ \text { ITE Land Use } \\ \text { \#580 } \end{gathered}$ | 2230 | 6 | 1 | 7 | 1 | 3 | 4 | 11 | 5 | 16 |


| Bank ITE Land Use \#911 | 427 | 7 | 3 | 10 | 25 | 31 | 56 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Small Retail ITE Land Use \#826 | 2,267 | 16 | 5 | 21 | 29 | 37 | 66 | 29 | 37 | 66 |
| Restaurant E ITE Land Use \#932 | 465 | 30 | 24 | 54 | 29 | 20 | 49 | 37 | 33 | 70 |
| Retail E ITE Land Use \#826 | 2,155 | 15 | 5 | 20 | 28 | 35 | 63 | 28 | 35 | 63 |
| Restaurant F ITE Land Use \#932 | 465 | 30 | 24 | 54 | 29 | 20 | 49 | 37 | 33 | 70 |
| Retail F ITE Land Use \#826 | 418 | 4 | 1 | 5 | 5 | 7 | 12 | 5 | 7 | 12 |
| Dealership ITE Land Use \#841 | 2,264 | 35 | 12 | 47 | 26 | 38 | 64 | 49 | 49 | 98 |
| Storage Facility ITE Land Use \#151 | 3,250 | 3 | 2 | 5 | 5 | 4 | 9 | 7 | 7 | 14 |
| Phase 1 T |  | 748 | 641 | 1,389 | 841 | 834 | 1,675 | 1,071 | 1,052 | 2,123 |
| Phase 2 (completed by 2028) |  |  |  |  |  |  |  |  |  |  |
| Restaurant H ITE Land Use \#932 | 465 | 30 | 24 | 54 | 29 | 20 | 49 | 37 | 33 | 70 |
| Retail H ITE Land Use \#826 | 2,861 | 18 | 6 | 24 | 37 | 46 | 83 | 37 | 46 | 83 |
| Restaurant I ITE Land Use \#932 | 465 | 30 | 24 | 54 | 29 | 20 | 49 | 37 | 33 | 70 |
| Retail I ITE Land Use \#826 | 418 | 4 | 1 | 5 | 5 | 7 | 12 | 5 | 7 | 12 |
| Entertainment Anchor ITE Land Use \#435 | 3,716 | 20 | 5 | 25 | 79 | 64 | 143 | 79 | 64 | 143 |
| Health Club ITE Land Use \#492 | 3,716 | 28 | 28 | 56 | 80 | 61 | 141 | 50 | 61 | 111 |
| $\begin{gathered} \text { Hotel } 1+2 \\ \text { ITE Land Use } \\ \text { \#310 } \\ \hline \end{gathered}$ | $\begin{gathered} 250 \\ \text { rooms } \end{gathered}$ | 78 | 55 | 133 | 77 | 73 | 150 | 101 | 79 | 180 |
| Small Retail | 2,564 | 18 | 6 | 24 | 33 | 42 | 75 | 33 | 42 | 75 |
| Entertainment Centre ITE Land Use \#444 | 3716 | 0 | 0 | 0 | 0 | 0 | 0 | 614 | 482 | 1096 |


| $\begin{gathered} \text { Bank } \\ \text { ITE Land Use } \\ \text { \#911 } \\ \hline \end{gathered}$ | 437 | 7 | 3 | 10 | 25 | 32 | 57 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Restaurant } \\ & \text { ITE Land Use } \\ & \# 932 \end{aligned}$ | 539 | 35 | 28 | 63 | 22 | 11 | 33 | 43 | 39 | 82 |
| $\begin{aligned} & \text { Dealership } \\ & \text { ITE Land Use } \\ & \text { \#810 } \end{aligned}$ | 1,650 | 0 | 0 | 0 | 12 | 13 | 25 | 27 | 29 | 56 |
| Phase 2 To |  | 268 | 180 | 448 | 428 | 389 | 817 | 1,063 | 915 | 1,978 |
| Phase 3 (completed by 2033) |  |  |  |  |  |  |  |  |  |  |
| Entertainment / Recreation Area ITE Land Use \#481 | $\begin{gathered} 15 \\ \text { acres } \end{gathered}$ | 6 | 0 | 6 | 60 | 37 | 97 | 164 | 119 | 283 |
| General Office (x4) <br> ITE Land Use \#710 | 10,461 | 154 | 22 | 176 | 29 | 140 | 169 | 26 | 22 | 48 |
| Residential Area (12 mid-rise apartments) ITE Land Use \#223 | 20 units each | 24 | 48 | 72 | 60 | 36 | 96 | 30 | 36 | 66 |
| $\begin{gathered} \text { Gas Station } \\ \text { ITE Land Use } \\ \# 944 \\ \hline \end{gathered}$ | 8 fueling stations | 49 | 48 | 97 | 56 | 55 | 111 | 56 | 55 | 111 |
| Convenience Retail ITE Land Use \#826 | 1,177 | 6 | 3 | 9 | 15 | 19 | 34 | 15 | 19 | 34 |
| Phase 3 Total |  | 239 | 121 | 360 | 220 | 287 | 507 | 291 | 251 | 542 |
| TOTAL |  | 1,255 | 942 | 2,197 | 1,489 | 1,510 | 2,999 | 2,425 | 2,218 | 4,643 |



Figure 10 - Proposed Development Phasing

### 4.2 Trip Assignment

New developments generate new traffic, the total traffic generated is comprised of new trips, diverted trips, and pass-by trips. New traffic is generated by a new development being constructed and in operation. This is traffic that would not have been on the street network without the new development, and needs to be added to the adjacent street and intersection approaches. Diverted traffic is traffic that has been diverted from other nearby areas as a result of the development and also increases the traffic on adjacent streets and intersection approaches. Pass-by traffic is traffic that is already on the adjacent street and intersection approaches and makes an intermediate trip to the development. This traffic is not new to the adjacent street network. The percentage of pass-by trips varies between different types of developments.

For the purpose of this study, a $25 \%$ pass-by trip percentage is assumed. It should be noted that the generated traffic volumes (Table 17) were reduced by $20 \%$ when they were assigned to the network to reflect an internal synergy component.

The generated trips have been assigned to the Study Area streets and intersections based on existing traffic distribution within the Study Area during the peak periods.

The following summarizes the assumptions utilized for assigning new traffic to the development for the PM and Saturday peak hours:

Traffic generated from the north (Foster Thurston Drive): 10\% (PM) and 5\% (Saturday);
Traffic generated from the south (Rothesay Avenue): 30\% (PM) and 40\% (Saturday);
Traffic generated from the east (Route 1): 15\% (PM) and 25\% (Saturday);
Traffic generated from the east (Rothesay Road): 5\% (PM) and 5\% (Saturday), and;
Traffic generated from the west (Route 1): 40\% (PM) and 25\% (Saturday).
It is assumed that traffic generated from the east on Rothesay Road will access the development using the Rothesay Road / Ashburn Road intersection. It was assumed that $80 \%$ of traffic generated from the east and west on Route 1 will access the development using the Rothesay Road / Rothesay Avenue intersection, while $20 \%$ will access the development using the Rothesay Road / Ashburn Road intersection. Traffic generated from the south was assumed to access the development using the Rothesay Road / Rothesay Avenue intersection. Traffic generated from the north was assumed to access the development using the Foster Thurston / Ashburn Road intersection.

Figures 11, 12 and 13 show the traffic assignment for Phase 1 (2023 Horizon Year).


Figure 11 - Trip Assignment - Development Phase 1 (2023 Horizon Year) (1 of 3)


Figure 12 - Trip Assignment - Development Phase 1 (2023 Horizon Year) (2 of 3)


Figure 13 - Trip Assignment - Development Phase 1 (2023 Horizon Year) (3 of 3)

## 5 Future Traffic Operations - Phase 1

### 5.12023 Horizon Year Levels of Service (Phase 1)

Given a) the existing operational issues within the study area, and b) that full buildout of the Crossing is expected to generate significant traffic volumes; a decision was made to initially focus the traffic study on Phase 1 of the development. Consequently, this section focuses on the 2023 horizon year future traffic operations with Phase 1 of the development in place. The Synchro model was updated to reflect changes in traffic volumes and lane configurations associated with the developments for Phase 1 and then re-run to obtain LOS with Phase 1 development.

### 5.1.1 Foster Thurston Drive / Ashburn Road

The Foster Thurston Drive / Ashburn Road intersection is one of the access points to the proposed development. For Phase 1 of the development it was assumed that this access would be utilized by traffic generated from the north. The LOS for the projected 2023 horizon year traffic volumes for PM and Saturday peak hours with Phase 1 of the development under existing conditions as well as with recommended options are presented in Table 18 for the Foster Thurston Drive / Ashburn Road intersection. The analysis output can be found in Appendix C.

By the 2023 horizon year with Phase 1 of the development in place, the Ashburn Road / Foster Thurston intersection is projected to operate at an overall LOS C or better with an intersection delay of 15 seconds/vehicle or less during the PM and Saturday peak period. All individual movements are projected to operate at acceptable LOS E or better with average delays of 35 seconds/vehicle or less for the PM and Saturday peak period. The lone exception is the northbound movement during the PM peak period, which is projected to operate at an unacceptable LOS F (average delay of 168 seconds/vehicle). The lowest movements in terms of LOS are the northbound and southbound approaches, which currently operate under stop control conditions. All v/c ratios are below 0.57 or lower, indicating that there is sufficient capacity.

It is important to note that operational deficiencies are projected at the northbound movement during the PM peak period by the 2023 horizon year without development as well as at the southbound movement during the PM peak period by the 2033 horizon year without development.

The movements experiencing operational deficiencies (northbound and southbound through movements) have very low volumes and operate under stop control conditions. There are limited options to improve these approaches other than a change in traffic control or restricting turn movements. It is notable that trips generated as a result of Phase 1 of the development are not projected to worsen operating conditions significantly.

It is recommended to add a separate channelized right turn slip lane on the southbound approach. This is recommended because of the increase in southbound (Ashburn Road) right turning traffic volume as a result of vehicles exiting the development towards the north. These right turn movements would not be delayed by the through and left turn movements.

Synchro was updated to reflect the recommended change in lane geometry and rerun using 2023 traffic volumes with development. Results are summarized in Table 18. The northbound approach is still projected to operate at LOS F, however, this approach has very low volumes with a v/c ratio well below capacity. It is important to note that delays experienced by the through and left turn movements at the southbound approach and the delays at the northbound approach are not a result of traffic associated with Phase 1 of the development.

Table 18 - LOS Summary for Foster Thurston Dr/Ashburn Rd with Development (Ph 1)


### 5.1.2 Foster Thurston Drive / NB Route 1 Access Ramps

The AM peak period was analyzed for the Foster Thurston Drive / Route 1 on-ramp and off-ramp because the directional split on Route 1 westbound is significantly higher during this period, therefore, the critical operational deficiencies occurring at these access ramps as a result of the development would occur during the AM peak period.
The results of the LOS analysis under projected 2023 traffic volumes with Phase 1 of the development are presented in Table 19 for the Foster Thurston Drive / NB Route 1 Access Ramps. The detailed analysis output can be found in Appendix C.

By 2023 with Phase 1 of the development in place, the Foster Thurston Drive / Route 1 off-ramp is projected to operate at LOS D with an average density of $17.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the AM peak period. The Foster Thurston Drive / Route 1 on-ramp is projected to operate at LOS D with an average density of $17.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the AM peak period.

No operational deficiencies are projected at the Foster Thurston Drive / Route 1 Access Ramps by 2023 with Phase 1 of the development in place.

Table 19 - LOS Summary for Foster Thurston Dr/Rte 1 Ramps with Development (Ph 1)

| Ramp | LOS <br> Density (pc/km/ln) |
| :--- | :---: |
| Projected 2023 Horizon Year Conditions with Development |  |
| Rte 1 - Foster Thurston Dr off-ramp | D |
| (AM Peak) | 17.6 |
| Rte 1 - Foster Thurston Dr on-ramp | D |
| (AM Peak) | 17.7 |

### 5.1.3 Ashburn Lake Road / NB Route 1 Access Ramps

The PM peak period was analyzed for the Ashburn Lake Road / Route 1 on-ramp and off-ramp because the directional split on Route 1 eastbound is significantly higher during this period, therefore, the critical operational deficiencies occurring at these access ramps as a result of the development would occur during the PM peak period.
The results of the LOS analysis under projected 2023 traffic volumes with Phase 1 of the development are presented in Table 20 for the Ashburn Lake Road / NB Route 1 Access Ramps. The detailed analysis output can be found in Appendix C.

By 2023 with Phase 1 of the development in place, the Ashburn Lake Road / Route 1 off-ramp is projected to operate at LOS D with an average density of $19.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the PM peak period.
The Ashburn Lake Road / Route 1 on-ramp is projected to operate at LOS E with an average density of $22.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the PM peak period.

The Ashburn Lake Road / Route 1 on-ramp will begin to experience some congestion by the 2023 horizon year with Phase 1 of the development in place. This is a result of no direct connection to Foster Thurston Drive.

Table 20 - LOS Summary for Ashburn Lake Rd/Rte 1 Ramps with Development (Ph 1)

| Ramp | LOS <br> Density (pc/km/ln) |
| :--- | :---: |
| Projected 2023 Horizon Year Conditions with Development |  |
| Rte 1 - Ashburn Lake Rd off-ramp | D |
| (PM Peak) | 19.6 |
| Rte 1 - Ashburn Lake Rd on-ramp | E |
| (PM Peak) | 22.2 |

### 5.1.4 Rothesay Avenue / Retail Drive / Ashburn Lake Road

The LOS for the projected 2023 horizon year traffic volumes for PM and Saturday peak hours with development under existing conditions as well as with recommended options are presented in Table 21 for the Rothesay Avenue / Retail Drive and Rothesay Avenue / Ashburn Lake Road intersections. The analysis output can be found in Appendix C.

By the 2023 horizon year with Phase 1 of the development in place, the Rothesay Avenue / Retail Drive intersection is projected to operate at an overall acceptable LOS E or better with an intersection delay of 57 seconds/vehicle or less during the PM and Saturday peak period. The westbound left turn movement is operating at an unacceptable LOS F with an average delay of 203 seconds/vehicle or less during both the PM and Saturday peak period. The v/c ratio at the westbound left turn movement exceeds 1.0 during both the PM and Saturday peak period, indicating that the demand exceeds the capacity. All other movements are projected to operate at LOS D or better with average delays of 54 seconds/vehicle or less and $\mathrm{v} / \mathrm{c}$ ratios of 0.92 or less. The $95^{\text {th }}$ percentile queues are projected to reach 139 m to 141 m on the westbound left turn movement during the PM and Saturday peak period.

By the 2023 horizon year with Phase 1 of the development in place, the Rothesay Avenue /
Ashburn Lake Road intersection is projected to operate at an overall LOS D with an intersection delay of 38 seconds/vehicle during the Saturday peak period and at an unacceptable LOS F with an intersection delay of 82 seconds/vehicle during the PM peak period. All individual movements are projected to operate at acceptable LOS E or better with an average delay of 61 seconds/vehicle or less during both the PM and Saturday peak period. The exception is the northbound movement
during the PM peak period which is projected to operate at LOS F with an average delay of 124 seconds/vehicle. The v/c ratio at the northbound approach during the PM peak period is projected to exceed the 1.0 threshold indicating that the demand exceeds the capacity. The $95^{\text {th }}$ percentile queue lengths are projected to be 84 m on the eastbound approach and 98 m on the northbound approach during the PM peak period. High projected delays at the northbound approach of Rothesay Avenue / Ashburn Lake Road is a result of the assumption that traffic generated from the south (south of Retail Drive) would access the development using the Ashburn Lake Road ramps.

It is important to note that operational deficiencies are already projected by the 2023 horizon year at the westbound left turn movement of Rothesay Avenue / Retail Drive without the development in place. Additional operational deficiencies as a result of the traffic generated by the development is projected at the northbound movement of the Rothesay Avenue / Ashburn Lake Road intersection during the PM peak period by the 2023 horizon year.

The Rothesay Avenue / Retail Drive and Rothesay Avenue / Ashburn Lake Road off-set intersections cannot function properly because of the short distance between them and the high traffic volumes.

It is recommended to realign the existing Rothesay Avenue / Retail Drive and Rothesay Avenue / Ashburn Lake Road into a 4-leg signalized intersection. Although it was not within the scope of this study to do a detailed design of the potential future realignment at this location, a possible re-alignment lane configuration was completed in Synchro to determine the potential impact. The distribution of traffic by the 2023 horizon year with Phase 1 of the development at the realigned intersection is shown in Figure 14 for the PM and Saturday peak periods.

The northbound and southbound approaches each have one separate left turn lane, one separate through lane, and one shared through/right turn lane. The right turn lane at the northbound approach is channelized with free flow conditions. The eastbound and westbound approaches each have a separate left turn lane and a shared through/right turn lane. The intersection was assumed to operate under full detection. There are 8 phases, which include a protected left turn phase at each of the approaches. The realigned intersection was modelled in Synchro; results are shown in Table 21.

With the realignment by the 2023 horizon year with Phase 1 of the development in place, the Rothesay Avenue / Retail Drive / Ashburn Lake Road intersection is projected to operate at an overall LOS C with an intersection delay of 27 seconds/vehicle and 22 seconds/vehicle during the PM and Saturday peak period, respectively. All individual movements are projected to operate at satisfactory LOS D or better with an average delay of 44 seconds/vehicle or less and v/c ratios of 0.89 or less during both peak periods. The $95^{\text {th }}$ percentile queue lengths are projected to be the longest at the northbound approach during the PM peak period, at a length of 97 m .


Figure 14 - Projected Volumes for Realigned Rothesay Ave / Retail Dr (2023 w/ Development) - PM/SAT
Table 21 - LOS Summary for Rothesay Ave/Retail Dr with Development (Ph 1)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [95\% Queues (m)] |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound <br> Rothesay Ave |  |  | Southbound <br> Rothesay Ave |  |  |
|  |  |  |  | Ashburn Lake Rd |  |  | Retail Dr |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | $\stackrel{R}{>}$ | $4$ |  | $\stackrel{R}{R}$ | $4$ |  | $\stackrel{R}{R}$ |  |  | $\stackrel{R}{\mathrm{R}}$ |
| Projected 2023 Horizon Year with Development Conditions (Rothesay Ave / Retail Dr) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave <br> @ Retail Dr / | $0$ | PM Peak | $\begin{gathered} \mathrm{E} \\ 57 \end{gathered}$ |  |  |  | $\begin{gathered} \hline F \\ 203 \\ {[1.30]} \end{gathered}$ |  | $\begin{gathered} \hline \text { B } \\ 19 \\ {[0.55]} \end{gathered}$ |  | $\begin{gathered} \hline \text { D } \\ 54 \\ {[0.56]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \text { B } \\ 17 \\ {[0.89]} \end{gathered}$ |  |
| Ashburn Lake Rd |  | Sat Peak | $\begin{gathered} C \\ 35 \end{gathered}$ |  |  |  | $\begin{gathered} \hline F \\ 199 \\ {[1.29]} \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline \hline \mathrm{A} \\ 8 \\ {[0.51]} \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline \text { A } \\ 6 \\ {[0.40]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \text { B } \\ 12 \\ {[0.92]} \end{gathered}$ |  |
| Projected 2023 Horizon Year with Development Conditions (Rothesay Ave / Ashburn Lake Rd) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave @ Retail Dr / |  | PM Peak | $\begin{gathered} F \\ 82 \end{gathered}$ | C 33 $[0.83]$ |  | shared |  |  |  | shared | $\begin{gathered} F \\ 124 \\ {[1.29]} \\ \hline \end{gathered}$ |  |  | $\begin{gathered} \text { E } \\ 61 \\ {[0.67]} \\ \hline \end{gathered}$ | shared |
| Ashburn Lake Rd |  | Sat Peak | $\begin{gathered} \text { D } \\ 38 \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 22 \\ {[0.70]} \\ \hline \end{gathered}$ |  | shared |  |  |  | shared | $\begin{gathered} \hline \text { B } \\ 16 \\ {[0.72]} \\ \hline \end{gathered}$ |  |  | $E$ 61 $[0.58]$ | shared |
| Projected 2023 Horizon Year with Development Conditions and Recommendations (Rothesay Ave / Retail Dr / Ashburn Lake Rd realignment) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave @ Retail Dr / |  | PM Peak | $\begin{gathered} C \\ 27 \end{gathered}$ | $\begin{gathered} \text { D } \\ 44 \\ {[0.89]} \end{gathered}$ | $\begin{gathered} \text { C } \\ 24 \\ {[0.38]} \end{gathered}$ | shared | $\begin{gathered} \text { C } \\ 22 \\ {[0.58]} \end{gathered}$ | $\begin{gathered} \text { C } \\ 24 \\ {[0.73]} \end{gathered}$ | shared | $\begin{gathered} \text { C } \\ 20 \\ {[0.59]} \end{gathered}$ | $\begin{gathered} \text { C } \\ 30 \\ {[0.82]} \end{gathered}$ | shared | $\begin{gathered} \text { C } \\ 21 \\ {[0.60]} \end{gathered}$ | $\begin{gathered} \text { C } \\ 24 \\ {[0.67]} \end{gathered}$ | shared |
| Ashburn Lake Rd |  | Sat Peak | $\begin{gathered} \text { C } \\ 22 \end{gathered}$ | $C$ 28 $[0.73]$ | $C$ 25 $[0.42]$ | shared | $\begin{gathered} \hline \hline \text { B } \\ 19 \\ {[0.55]} \end{gathered}$ | $\begin{gathered} \hline \hline B \\ 18 \\ {[0.70]} \end{gathered}$ | shared | $\begin{gathered} \hline B \\ 13 \\ {[0.34]} \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 22 \\ {[0.67]} \end{gathered}$ | shared | $C$ 28 $[0.78]$ | $\begin{gathered} \hline \text { C } \\ 20 \\ {[0.56]} \end{gathered}$ | shared |

### 5.1.5 Rothesay Road / Fulton Lane

The Rothesay Road / Fulton Lane intersection is proposed to be slightly offset from an access point to the development on Rothesay Road (just east of Fulton Lane). The intersection was analyzed assuming it is a four-leg intersection. The majority of the traffic using this access to the development would be volumes generated from the proposed truck stop.

The LOS for the projected 2023 horizon year traffic volumes for PM and Saturday peak hours with development under existing conditions as well as with recommended options are presented in Table

22 for the Rothesay Road / Fulton Lane / Access intersection. The analysis output can be found in Appendix C.

By the 2023 horizon year with Phase 1 of the development in place, the Rothesay Road / Fulton Lane / Access intersection is projected to operate at an overall LOS A during the PM and Saturday peak period. During the PM peak period, the eastbound and westbound movements are projected to operate at unacceptable LOS F with average delays of 52 seconds/vehicle and 190 seconds/vehicle, respectively. There are very small volumes associated with the westbound right and left turn movement and the eastbound left turn movement, therefore, the $\mathrm{v} / \mathrm{c}$ ratios at these approaches are still well below the threshold despite the higher delays. All other movements are projected to operate at LOS B with average delays of 11 seconds/vehicle or less. During the Saturday peak period all movements are projected to operate at LOS C or better with an average delay of 22 seconds/vehicle or less. The $\mathrm{v} / \mathrm{c}$ ratios are projected to be 0.66 or less during both the PM and Saturday peak period.

Operational deficiencies are projected at the Rothesay Road / Fulton Lane / Access intersection during the PM peak period at the eastbound and westbound approaches by the 2023 horizon year with Phase 1 of the development in place.

It is recommended this proposed development access be aligned with the existing Fulton Lane at Rothesay Avenue. It is also recommended to make this access a right-in/right-out only with the primary access off Ashburn Road. As this access is projected to primarily be utilized by trucks, it is recommended that during the detailed design of this access that the approach be checked to ensure the turning movements can be accommodated by the design vehicle (i.e. the largest truck that would utilize this access).

The Synchro model was updated to reflect the recommended right-in/right-out only access. Results are shown in Table 22. By the 2023 horizon year with Phase 1 of the development in place and after making the access to the development right-in/right out only, the Rothesay Road / Fulton Lane / Access intersection is projected to operate at an overall LOS A with an intersection delay of 2 seconds/vehicle during both the PM and Saturday peak period. The westbound movement during the PM peak period is still projected to operate at LOS F with an average delay of 98 seconds/vehicle. This movement, however, has a very low volume and a v/c ratio that is well below the threshold; delays are unavoidable under two-way stop controlled conditions. All other movements are projected to operate at LOS C or better with average delays of 21 seconds/vehicle or less. All v/c ratios are 0.36 or less, indicating that there is sufficient capacity.

Table 22 - LOS Summary for Rothesay Rd/Fulton Ln/Access with Development (Ph 1)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound | Westbound |  |  | Northbound <br> Rothesay Rd |  |  | Southbound |  |  |
|  |  |  |  | Access | Fulton Ln |  |  |  |  |  | Rothesay Rd |  |  |
|  |  |  |  |  | 4 | $\hat{\mathbf{T}}$ | $\stackrel{R}{R}$ |  | T | $\stackrel{R}{R}$ | 4 | T 1 | $\stackrel{R}{ }$ |
| Projected 2023 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd |  | PM Peak | $\begin{gathered} A \\ 5 \end{gathered}$ | shared F  <br>  52 shared <br>  $[0.66]$  <br>    <br>    <br>    <br>    <br>    | shared | $\begin{gathered} \hline F \\ 190 \\ {[0.38]} \end{gathered}$ | shared | shared | $\begin{gathered} \text { B } \\ 11 \\ {[0.18]} \end{gathered}$ | shared | shared | $\begin{gathered} B \\ 10 \\ {[0.01]} \end{gathered}$ | shared |
| Access |  | Sat Peak | A 3 |    <br> shared 14 shared <br>  $[0.26]$  <br>    | shared | $\begin{gathered} \hline \text { C } \\ 22 \\ {[0.02]} \\ \hline \end{gathered}$ | shared | shared | A 9 $[0.13]$ | shared | shared | $\begin{gathered} \hline \mathrm{A} \\ 8 \\ {[0.00]} \end{gathered}$ | shared |
| Projected 2023 Horizon Year with Development Conditions and Recommended Option |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd <br> @ Fulton Ln / Access | STOP | PM Peak | $\begin{aligned} & A \\ & 2 \end{aligned}$ | $C$  <br> 21 shared <br> $[0.36]$  <br> B  | shared | $\begin{gathered} \hline F \\ 98 \\ {[0.22]} \\ \hline \end{gathered}$ | shared |  |  | low | shared | $\begin{gathered} \hline \text { B } \\ 11 \\ {[0.01]} \end{gathered}$ | shared |
|  |  | Sat Peak | A 2 | B  <br> 12 shared <br> $[0.21]$  | shared | $\begin{gathered} \hline \text { C } \\ 19 \\ {[0.04]} \\ \hline \end{gathered}$ | shared |  |  | low | shared | $\begin{gathered} \hline \text { A } \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | shared |

### 5.1.6 Ashburn Road / Jones Drive

The Ashburn Road / Jones Drive intersection is to be utilized in the future as an access to the development to the south of Ashburn Road. It was assumed, however, that this access would not be utilized by development traffic by the 2023 horizon year with Phase 1 of the development in place.

The LOS for the projected 2023 horizon year traffic volumes for PM and Saturday peak hours with development under existing conditions are presented in Table 23 for the Ashburn Road / Jones Drive intersection. The analysis output can be found in Appendix C.

Minimal changes are projected at the Ashburn Road / Jones Drive intersection by the 2023 horizon year with Phase 1 of the development in place. All movements are projected to operate at LOS C or better with average delays of 16 seconds/vehicle or less during both the PM and Saturday peak period.

No operational deficiencies are projected at the Ashburn Road / Jones Drive intersection by the 2023 horizon year with Phase 1 of the development in place.
The Ashburn Road / Jones Drive intersection will be an access point to the development after full build out. It is recommended to implement separate left turn lanes at all approaches of this intersection to accommodate future internal traffic demand.

Table 23 - LOS Summary for Ashburn Rd/Jones Dr/Access with Development (Ph 1)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  | Westbound |  |  | Northbound |  | Southbound |  |  |
|  |  |  |  | Jones Dr |  |  |  |  | Ashburn Rd |  | Ashburn Rd |  |  |
|  |  |  |  |  |  | 4 | ${ }^{\top}$ |  |  | $\xrightarrow{\text { R }}$ | 4 | ${ }^{\top}$ | $\xrightarrow{R}$ |
| Projected 2023 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Jones Dr | STOP | PM Peak | $\begin{aligned} & \text { A } \\ & 0 \end{aligned}$ | $\begin{gathered} C \\ 16 \\ {[0.01]} \\ \hline \end{gathered}$ | shared |  |  |  |   <br> shared A <br>  8 <br>  $[0.00]$ |  |  | free flow | shared |
|  |  | Sat Peak | A 0 | $\begin{gathered} \hline \text { B } \\ 10 \\ {[0.01]} \end{gathered}$ | shared |  |  |  |   <br> shared A <br>  7 <br>  $[0.00]$ |  |  | free flow | shared |

### 5.1.7 Ashburn Road / Drury Cove Road

The LOS for the projected 2023 horizon year traffic volumes for PM and Saturday peak hours with development are presented in Table 24 for the Ashburn Road / Drury Cove Road intersection. The analysis output can be found in Appendix C.

Minimal changes are projected at the Ashburn Road / Drury Cove Road intersection by the 2023 horizon year with Phase 1 in place. All movements are projected to operate at LOS C or better with average delays of 20 seconds/vehicle or less during both the PM and Saturday peak periods.

No operational deficiencies are projected at the Ashburn Road / Drury Cove Road intersection by the 2023 horizon year with Phase 1 of the development in place. No recommended changes are needed at the Ashburn Road / Drury Cove Road intersection by the 2023 horizon year with Phase 1 of the development in place.

Table 24 - LOS Summary for Ashburn Rd/Drury Cove Rd with Development (Ph 1)


### 5.1.8 Rothesay Avenue / Rothesay Road

The Rothesay Road / Rothesay Avenue intersection is to be the main access to the proposed development. The LOS for the projected 2023 horizon year traffic volumes for PM and Saturday peak hours with development are presented in Table 25 for the Rothesay Road / Rothesay Avenue intersection. The analysis output can be found in Appendix C.

By the 2023 horizon year with Phase 1 of the development in place the Rothesay Road / Rothesay Avenue intersection is projected to operate at an overall LOS F with significant queuing and delays projected at the eastbound and westbound approaches during both the PM and Saturday peak period. All other movements are projected to operate at LOS B or better with average delays of 14 seconds/vehicle or less during both the PM and Saturday peak period.

Significant operational deficiencies are projected at the Rothesay Road / Rothesay Avenue intersection on the eastbound and westbound approaches by the 2023 horizon year with development in place. It is important to note that operational deficiencies are already experienced on the westbound approach under existing conditions.

Two different options were analyzed as potential improvements for the Rothesay Road / Rothesay Avenue intersection. These options included a roundabout (single lane, two multi lane, and full double lane options) as well as a traffic signal and changes in lane geometry. Roundabout configurations for the four different options can be found in the detailed analysis outputs in Appendix C.

## Roundabout Improvement Option

The option for a roundabout at the Rothesay Road / Rothesay Avenue intersection was analyzed using Sidra software. Two options were analyzed including a single lane and a double lane scenario. It is important to note that for the double lane scenario, it was assumed that the second lane at each approach were each 60 metres in length. Results are summarized in Table 25. Detailed reports of the analyses can be found in Appendix C.

The first option analyzed was a single lane roundabout implemented at the Rothesay Road /
Rothesay Avenue intersection. By the 2023 horizon year with the development in place and a single lane roundabout, the intersection is projected to operate at an overall LOS F during both the PM and Saturday peak periods. During the PM peak period, the northbound and eastbound movements are projected to operate at LOS with average delays of 141 seconds/vehicle or greater. The westbound and southbound movements are projected to operate at LOS D with an average delay of 47 seconds/vehicle or less. During the Saturday peak period all individual movements are projected to operate at LOS F with average delays of 128 seconds/vehicle or less. All v/c ratios exceed the threshold of 1.0 during both peak periods, indicating that the demand exceeds the capacity.

The second option analyzed was a multi lane roundabout implemented at the Rothesay Road /
Rothesay Avenue intersection that included two lanes at the northbound and southbound (Rothesay Road) approaches, and single lanes with separate right turn by-pass lanes at the eastbound and westbound (Rothesay Avenue) approaches. By the 2023 horizon year with development in place and a multi lane roundabout, the intersection is projected to operate at an overall LOS C or better with an intersection delay of 28 seconds/vehicle or less during the PM and Saturday peak period. During the PM peak period the northbound movements are projected to operate the lowest in terms of LOS at LOS E or better with average delays of 67 seconds/vehicle or less. The $\mathrm{v} / \mathrm{c}$ ratio on the northbound left turn movement is projected to be 1.02 , indicating the demand exceeds capacity. All other movements are operating at LOS C or better with an average delay of 21 seconds/vehicle or less and a v/c ratio of 0.74 or lower. During the Saturday peak period all individual movements are projected to operate at LOS D or better with average delays of 38 seconds/vehicle or less.

The third option analyzed was a multi lane roundabout described above with the addition of a right turn by-pass lane at the northbound approach. The addition of the northbound right turn by-pass lane is projected to improve conditions at the northbound approach of the Rothesay Road / Rothesay Avenue intersection. During the PM peak period the northbound through and left turn lanes are projected to operate at LOS D with average delays of 48 seconds/vehicle or less and $\mathrm{v} / \mathrm{c}$ ratios of 0.94 or better, indicating that there is sufficient capacity. The right turn slip lane is projected to operate at LOS B with an average delay of 12 seconds/vehicle. During the Saturday peak period the northbound through and left turn lanes are projected to operate at LOS C or better with an average delay of 25 seconds/vehicle or less and $\mathrm{v} / \mathrm{c}$ ratios of 0.60 or lower. The right turn slip lane is projected to operate at LOS B with an average delay of 13 seconds/vehicle.

The final option analyzed was a full double lane roundabout. By the 2023 horizon year with development in place and a double lane roundabout implemented at the Rothesay Road / Rothesay Avenue intersection, the intersection is projected to operate at an overall LOS C or better with an intersection delay of 23 seconds/vehicle or less during both the PM and Saturday peak period. All individual movements are projected to operate at LOS D or better with average delays of 40 seconds/vehicle or less during both peak periods. The v/c ratios for each movement are projected to be below the threshold, indicating that there is sufficient capacity. The $95^{\text {th }}$ percentile queue lengths are all projected to be below 116 metres with the longest queues projected on the northbound approach during the PM peak period.

No operational deficiencies are projected for the multi or double lane roundabout at the Rothesay Road / Rothesay Avenue intersection by the 2023 horizon year with Phase 1 of the development in place.

### 5.1.8.1 Traffic Signal Improvement Option

The second improvement option involves implementing traffic signals at the Rothesay Road / Rothesay Avenue intersection. Rothesay Avenue was assumed to be a 3-lane cross section with two lanes eastbound and one lane westbound. The lane geometry used in the analysis included a separate left turn pocket and a shared through and channelized right turn lane with yield conditions on the northbound approach; a separate left turn pocket, a through lane, and a separate channelized right turn pocket (extending back as far as the bridge structure) with free flow conditions on the westbound (Rothesay Avenue) approach; a separate left turn pocket and a shared through/channelized right turn lane with free flow conditions on the southbound approach and; a separate left turn lane, a through lane, and a separate channelized right turn lane with yield control on the eastbound (development access) approach.

The signal at the Rothesay Road / Rothesay Avenue intersection was analyzed assuming full detection. If the traffic signal option is implemented it is recommended to coordinate all three recommended traffic signals along Rothesay Avenue and Rothesay Road (for the Rothesay Road / Ashburn Road, Rothesay Road / Rothesay Avenue, and Rothesay Avenue / Route 1 off-ramp intersections). The analysis was performed assuming this coordination existed amongst the three intersections. The Synchro model was updated to reflect these changes. Results are summarized in Table 25. Detailed reports of the analyses can be found in Appendix C.

By the 2023 horizon year with the development in place and coordinated traffic signals implemented at the three intersections on Rothesay Road and Rothesay Avenue, the Rothesay Road / Rothesay Avenue intersection is projected to operate at an overall LOS D or better with an intersection delay of 42 seconds/vehicle or less during the PM and Saturday peak period. The eastbound and northbound through movements are projected to operate the lowest in terms of LOS, at LOS E or better with an average delay of 72 seconds/vehicle or less during both the PM and Saturday peak period. All other movements and the southbound and westbound left turn movements are projected to operate at LOS E with an average delay of 80 seconds/vehicle or less. The $\mathrm{v} / \mathrm{c}$ ratio at the northbound through and southbound left turn movement are either at capacity.

No operational deficiencies are projected by 2023 with Phase 1 of the development at the Rothesay Road / Rothesay Avenue intersection with actuated-coordinated signals and recommended geometry. The southbound left turn and northbound through movements have reached capacity.

Given the relatively high cost for the required roundabout solution, and the potential for overbuilt infrastructure if construction of the Ashburn underpass were to proceed, as well as from the operational findings for both options, it is recommended that traffic signals be the preferred solution at the Rothesay Ave / Rothesay Rd intersection to accommodate Phase 1 of the development.

Table 25 - LOS Summary for Rothesay Rd/Rothesay Ave with Development (Ph 1)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOSAverage Delay (seconds per vehicle)[Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Rothesay Ave |  |  | Rothesay Ave |  |  | Rothesay Rd |  |  | Rothesay Rd |  |  |
|  |  |  |  |  |  | $\stackrel{R}{R}$ | $\stackrel{L}{4}$ | ${ }_{\mathbf{T}}^{\mathbf{T}}$ | $\xrightarrow{R}$ |  | $\hat{1}^{\text {T }}$ | $\stackrel{R}{R}$ | 4 |  | $\xrightarrow{R}$ |
| Projected 2023 Horizon Year Conditions with Existing Configuration |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ |  | PM Peak | F | shared | $\begin{gathered} F \\ >300 \\ {[>2.00]} \\ \hline \hline \end{gathered}$ | shared | shared | $\begin{gathered} \hline F \\ >300 \\ {[>2.00]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \mathbf{A} \\ 9 \\ {[0.27]} \\ \hline \hline \end{gathered}$ | free flow | shared | shared | $\begin{gathered} \hline B \\ 14 \\ {[0.61]} \\ \hline \hline \end{gathered}$ | shared |
| Rothesay Ave | ST0P | Sat Peak | F | shared | F $>300$ $[>2.00]$ | shared | shared | F $>300$ $[>2.00]$ | shared | A 8 $[0.22]$ | free flow | shared | shared | A 9 $[0.32]$ | shared |
| Projected 2023 Horizon Year with Development Conditions with Recommendation (single lane roundabout) (option 1) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ |  | PM Peak | F | shared | $\begin{gathered} \hline F \\ 141 \\ {[1.22]} \end{gathered}$ | shared | shared | D 42 $[1.01]$ | shared | shared | $F$ $>300$ $[>2.00]$ | shared | shared | D 47 $[1.02]$ | shared |
| Rothesay Ave |  | Sat Peak | F | shared | $\begin{gathered} \hline F \\ 123 \\ {[1.21]} \\ \hline \end{gathered}$ | shared | shared | $\begin{gathered} \hline F \\ 113 \\ {[1.20]} \\ \hline \end{gathered}$ | shared | shared | $\begin{gathered} \hline F \\ 109 \\ {[1.15]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \hline F \\ 128 \\ {[1.20]} \\ \hline \end{gathered}$ | shared |
| Projected 2023 Horizon Year with Development Conditions with Recommendation (multi lane roundabout) (option 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ |  | PM Peak | $\begin{gathered} C \\ 28 \end{gathered}$ | $\begin{gathered} \text { A } \\ 10 \\ {[0.46]} \\ \hline \end{gathered}$ | shared | $A$ 5 $[0.18]$ | $\begin{gathered} \hline \text { B } \\ 10 \\ {[0.35]} \\ \hline \end{gathered}$ | shared | $B$ 10 $[0.71]$ | E 67 $[1.02]$ | shared | D 45 $[0.93]$ | $\begin{gathered} \hline \mathrm{C} \\ 21 \\ {[0.74]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline B \\ 12 \\ {[0.43]} \\ \hline \end{gathered}$ |
| Rothesay Ave |  | Sat Peak | $\begin{gathered} B \\ 19 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 16 \\ {[0.79]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline A \\ 6 \\ {[0.16]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 12 \\ {[0.74]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \mathbf{A} \\ 5 \\ {[0.28]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 25 \\ {[0.60]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \text { B } \\ 20 \\ {[0.54]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 38 \\ {[0.83]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \text { C } \\ 21 \\ {[0.42]} \\ \hline \end{gathered}$ |
| Projected 2023 Horizon Year with Development Conditions with Recommendation (multi lane roundabout) (option 3) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ |  | PM Peak | $\begin{gathered} \text { C } \\ 22 \end{gathered}$ | $\begin{gathered} \hline \text { A } \\ 10 \\ {[0.46]} \\ \hline \end{gathered}$ | shared | $A$ 5 $[0.18]$ | $\begin{gathered} \hline \text { B } \\ 10 \\ {[0.35]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline B \\ 10 \\ {[0.71]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 48 \\ {[0.94]} \\ \hline \hline \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 35 \\ {[0.85]} \\ \hline \hline \end{gathered}$ | $\begin{gathered} \hline B \\ 12 \\ {[0.15]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 21 \\ {[0.75]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline B \\ 13 \\ {[0.43]} \\ \hline \end{gathered}$ |
| Rothesay Ave | $\cdots$ | Sat Peak | $\begin{gathered} B \\ 18 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 16 \\ {[0.79]} \end{gathered}$ | shared | A 6 $[0.16]$ | $\begin{gathered} \hline B \\ 12 \\ {[0.73]} \\ \hline \end{gathered}$ | shared | A 5 $[0.28]$ | $\begin{gathered} \hline \text { C } \\ 25 \\ {[0.60]} \end{gathered}$ | B 18 $[0.39]$ | $\begin{gathered} \hline B \\ 13 \\ {[0.18]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 37 \\ {[0.83]} \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{C} \\ 21 \\ {[0.42]} \end{gathered}$ |
| Projected 2023 Horizon Year with Development Conditions with Recommendation (double lane roundabout) (option 4) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Rothesay Ave |  | PM Peak | $\begin{gathered} C \\ 23 \end{gathered}$ | A 9 $[0.42]$ | shared | A 8 $[0.31]$ | $\begin{gathered} \hline \text { B } \\ 14 \\ {[0.48]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \text { B } \\ 15 \\ {[0.84]} \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 40 \\ {[0.92]} \end{gathered}$ | shared | $\begin{gathered} \text { D } \\ 35 \\ {[0.91]} \\ \hline \end{gathered}$ | $\begin{gathered} C \\ 21 \\ {[0.79]} \end{gathered}$ | shared | $\begin{gathered} \text { B } \\ 12 \\ {[0.40]} \end{gathered}$ |
|  | - | Sat Peak | $\begin{gathered} B \\ 16 \end{gathered}$ | $\begin{gathered} \hline B \\ 12 \\ {[0.71]} \end{gathered}$ | shared | $\begin{gathered} \hline B \\ 11 \\ {[0.36]} \end{gathered}$ | $\begin{gathered} \hline B \\ 11 \\ {[0.68]} \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{A} \\ 7 \\ 7 \\ {[0.43]} \end{gathered}$ | $\begin{gathered} \hline \hline \text { C } \\ 21 \\ {[0.55]} \end{gathered}$ | shared | $\begin{gathered} \hline \text { B } \\ 15 \\ {[0.47]} \\ \hline \end{gathered}$ | $C$ 32 $[0.79]$ | shared | $\begin{gathered} \hline \text { B } \\ 18 \\ {[0.40]} \\ \hline \end{gathered}$ |
| Projected 2023 Horizon Year with Development Conditions and Recommended Option (Actuated Coordinated Signal) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Rothesay Ave |  | PM Peak | $\begin{gathered} \text { D } \\ 42 \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 27 \\ {[0.01]} \\ \hline \end{gathered}$ | $E$ 80 $[0.93]$ | $\begin{gathered} \hline A \\ 10 \\ {[0.43]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline E \\ 28 \\ {[0.65]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 42 \\ {[0.27]} \\ \hline \hline \end{gathered}$ | $\begin{gathered} \hline A \\ 1 \\ {[0.33]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline B \\ 11 \\ {[0.53]} \\ \hline \end{gathered}$ | $E$ 72 $[1.03]$ | shared | $\begin{gathered} \hline E \\ 62 \\ {[1.00]} \\ \hline \end{gathered}$ | $B$ 14 $[0.27]$ | shared |
|  |  | Sat Peak | $\begin{gathered} \text { C } \\ 30 \end{gathered}$ | $C$ 22 $[0.02]$ | D 51 $[0.89]$ | $A$ 7 $[0.26]$ | $\begin{gathered} \hline \mathrm{D} \\ 48 \\ {[0.91]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline B \\ 11 \\ {[0.43]} \\ \hline \end{gathered}$ | $A$ 0 $[0.19]$ | $\begin{gathered} \hline C \\ 21 \\ {[0.57]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 34 \\ {[0.58]} \\ \hline \end{gathered}$ | shared | D 42 $[0.90]$ | $C$ 28 $[0.26]$ | shared |

### 5.1.9 Rothesay Road / Ashburn Road

The Rothesay Road / Ashburn Road intersection is a secondary access off Rothesay Road to the proposed development. The LOS for the projected 2023 horizon year volumes for PM and Saturday peak hours with development are presented in Table 26 for the Rothesay Road / Ashburn Road intersection. The analysis output can be found in Appendix C.

By the 2023 horizon year with Phase 1 in place, the Rothesay Road / Ashburn Road intersection is projected to operate at an overall LOS C with an intersection delay of 17 seconds/vehicle during the PM peak period and at an overall LOS A with an intersection delay of 5 seconds/vehicle during the Saturday peak period. During the PM peak period, the eastbound left turn movement is projected to operate at an unacceptable LOS F with an average delay of 51 seconds/vehicle, the $\mathrm{v} / \mathrm{c}$ ratio, however, is below the 1.0 threshold indicating that there is sufficient capacity. The westbound movement is projected to operate at LOS E with an average delay of 38 seconds/vehicle. It is
important to note that this movement is associated with extremely low volumes and the $\mathrm{v} / \mathrm{c}$ ratio is 0.03 , indicating there is sufficient capacity. During the Saturday peak period all individual movements are operating at LOS C or better with average delays of 19 seconds/vehicle or less.

Operational deficiencies are projected at the eastbound approach of the Rothesay Road / Ashburn Road intersection on the eastbound approach during the PM peak period by the 2023 horizon year with Phase 1 of the development in place.

It is recommended to implement traffic signals at the Rothesay Road / Ashburn Road intersection. The traffic signals should be fully actuated and coordinated with the Rothesay Road / Rothesay Avenue intersection traffic signals. A separate left turn lane is recommended for the northbound approach.

The Synchro model was updated with the actuated-coordinated traffic signal and recommended changes to lane geometry at the Rothesay Road / Ashburn Road intersection. Note that the traffic volumes were also updated to reflect the right-in/right-only recommendation at the Rothesay Road / Fulton Lane development access; it was assumed that left turning vehicles to and from the truck stop would utilize the Rothesay Road / Ashburn Road intersection.

By the 2023 horizon year with Phase 1 of the development in place and an actuated-coordinated traffic signal and northbound left turn lane implemented, the Rothesay Road / Ashburn Road intersection is projected to operate at an overall LOS A with an intersection delay of 9 seconds/vehicle or less during both the PM and Saturday peak period. All individual movements are projected to operate at LOS D or better with an average delay of 38 seconds/vehicle or less during both the PM and Saturday peak period. All v/c ratios are projected to be 0.78 or less, indicating that there is sufficient capacity.

No operational deficiencies are projected at the Rothesay Road / Ashburn Road intersection with actuated-coordinated traffic signal and an added left turn lane at the northbound approach by the 2023 horizon year with Phase 1 of the development in place.

Table 26 - LOS Summary for Rothesay Rd/Ashburn Rd with Development (Ph 1)

| Intersection |  |  | $\begin{array}{\|c} \text { Overall } \\ \text { LOS \& } \\ \text { Delay } \\ \text { (sec/veh) } \end{array}$ | Turning Movements LOSAverage Delay (seconds per vehicle)[Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Ashburn Rd |  |  | Parking Lot |  |  | Rothesay Rd |  |  | Rothesay Rd |  |  |
|  |  |  |  | L | T | R | L | T | R | L | T | R | L | T | R |
| Projected 2023 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd |  | PM Peak | $\begin{gathered} \text { C } \\ 17 \end{gathered}$ | $\begin{gathered} F \\ 51 \\ {[0.70]} \\ \hline \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ 25 \\ {[0.82]} \\ \hline \end{gathered}$ | shared | shared | $\begin{gathered} \mathrm{E} \\ 38 \\ {[0.03]} \\ \hline \hline \end{gathered}$ | shared | shared | $\begin{gathered} \hline A \\ 8 \\ {[0.14]} \\ \hline \hline \end{gathered}$ | shared | shared | $\begin{gathered} \hline \text { A } \\ 0 \\ {[0.0]} \\ \hline \hline \end{gathered}$ | shared |
| @ Ashburn Rd |  | Sat Peak | $\begin{gathered} \text { A } \\ 5 \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 19 \\ {[0.27]} \end{gathered}$ | $\begin{gathered} \hline B \\ 10 \\ {[0.17]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \mathbf{A} \\ 0 \\ {[0.00]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \text { A } \\ 8 \\ {[0.10]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \text { A } \\ 0 \\ {[0.00]} \end{gathered}$ | shared |
| Projected 2023 Horizon Year with Development Conditions and Recommended Option (Actuated Coordinated Signal) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ Ashburn Rd |  | PM Peak | $\begin{aligned} & \text { A } \\ & 9 \end{aligned}$ | $\begin{gathered} \hline \mathrm{D} \\ 36 \\ {[0.54]} \\ \hline \end{gathered}$ | A 9 $[0.78]$ | shared |    <br> shared 0  <br>  shared  <br>  $[0.01]$  |  |  | $\begin{gathered} \hline \mathbf{A} \\ 4 \\ {[0.52]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathbf{A} \\ 3 \\ {[0.48]} \\ \hline \end{gathered}$ | shared | shared | $\begin{gathered} \hline \text { C } \\ 22 \\ {[0.29]} \\ \hline \end{gathered}$ | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 7 \end{aligned}$ | $\begin{gathered} \hline \hline \mathrm{C} \\ 22 \\ {[0.42]} \end{gathered}$ | $\begin{gathered} \hline \hline A \\ 0 \\ {[0.16]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \hline \mathbf{A} \\ 0 \\ {[0.00]} \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{A} \\ 3 \\ {[0.30]} \end{gathered}$ | $\begin{gathered} \hline \hline A \\ 2 \\ {[0.14]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \hline B \\ 12 \\ {[0.34]} \end{gathered}$ | shared |

### 5.1.10 Rothesay Avenue / NB Route 1 Interchange

The LOS for the projected 2023 horizon year traffic volumes for PM and Saturday peak hours with development are presented in Table 27 for the Rothesay Avenue / Route 1 off-ramp intersection, and Table 28 for the Rothesay Avenue / Route 1 on-ramp intersections (west and east). The analysis outputs can be found in Appendix C.

## Rothesay Avenue / Route 1 off-ramp Intersection

By the 2023 horizon year with Phase 1 of the development in place, the Rothesay Avenue / Route 1 off-ramp intersection is projected to operate at an overall LOS F during the PM and Saturday peak period. The eastbound and westbound approaches are projected to operate at LOS F during both the PM and Saturday peak period. The highest delays are projected during the Saturday peak period, with delays exceeding 300 seconds/vehicle. The eastbound and westbound approaches are projected to experience significant delays and $\mathrm{v} / \mathrm{c}$ ratios are either approaching or exceeding the threshold, indicating that there is not enough capacity for the demand. Significant queueing is projected at these approaches.

Significant operational deficiencies are projected by the 2023 horizon year with Phase 1 of the development in place at the eastbound and westbound approaches of the Rothesay Avenue / Route 1 off-ramp intersection during the PM and Saturday peak period. It is notable that operational deficiencies are projected at this intersection by the 2023 horizon year without the development in place, however, delays and queueing are expected to get worse with the addition of traffic to the development from both the south as well as from Route 1 westbound traffic.

It is recommended to implement traffic signals at the Rothesay Avenue / Route 1 off-ramp intersection as well as a through pocket on the eastbound approach. The signals should be fully actuated and coordinated with traffic signals at the Rothesay Road / Rothesay Avenue intersection.

The Synchro model was updated to reflect an actuated-coordinated traffic signal and change in geometry at the Rothesay Avenue / Route 1 off-ramp intersection. Results are shown in Table 27.

By the 2023 horizon year with Phase 1 of the development in place as well as actuated-coordinated traffic signals and recommended change in geometry, the Rothesay Avenue / Route 1 off-ramp
intersection is projected to operate at an overall LOS A (intersection delay of 8 seconds/vehicle) and LOS C (intersection delay of 23 seconds/vehicle) during the PM and Saturday peak period, respectively. All individual movements are projected to operate at satisfactory LOS D or better with an average delay of 40 seconds/vehicle or less during both peak periods. All v/c ratios are projected to be 0.92 or less. The $95^{\text {th }}$ percentile queue length at the southbound approach is not projected to exceed 170 m , which is well below the length of the off-ramp.

No operational deficiencies are projected at the Rothesay Avenue / Route 1 off-ramp intersection by the 2023 horizon year with Phase 1 of the development in place after an actuated-coordinated traffic signal and eastbound through pocket are implemented along with required infrastructure changes upstream at the Rothesay Road / Rothesay Avenue / Access intersection.

Table 27 - LOS Summary for Rothesay Ave/Rte1 off-ramp with Development (Ph 1)


## Rothesay Avenue / Route 1 on-ramp Intersections

By the 2023 horizon year with Phase 1 of the development in place, both the Rothesay Avenue / Route 1 on-ramp intersections (east and west) are projected to operate at an overall satisfactory LOS D or better with an intersection delay of 33 seconds/vehicle or less. The eastbound movements are projected to operate at LOS F during both peak periods for the intersection furthest west and during the Saturday peak period for the intersection furthest east. The $95^{\text {th }}$ percentile queue lengths indicate that vehicles at the intersection furthest east may spill back to the intersection furthest to the west, as the projected lengths exceed the short distance between the two intersections.

Operational deficiencies are projected by the 2023 with Phase 1 of the development in place at the Rothesay Avenue / Route 1 on-ramp intersection (west) at the eastbound approach during the PM and Saturday peak periods and at the Rothesay Avenue / Route 1 on-ramp intersection (east) at the eastbound approach during the Saturday peak period.

There are limited options with respect to changes to infrastructure geometry to improve traffic conditions at the Rothesay Avenue / Route 1 on-ramp intersections because of the overpass structure just west of this location.

Table 28 - LOS Summary for Rothesay Ave/Rte 1 on-ramp intersections with Development (Ph 1)


### 5.1.11 NB Route 1 Access with Rothesay Road / Rothesay Avenue

The AM peak period was analyzed for the Rothesay Road / Route 1 on-ramp because the directional split on Route 1 westbound is significantly higher during the AM period. The PM peak period was analyzed for the Rothesay Road / Route 1 off-ramp because the directional split on Route 1 eastbound is significantly higher during the PM peak period. Therefore, the critical operational deficiencies occurring at these access ramps as a result of the development would occur during the AM peak period for the on-ramp and during the PM peak period for the off-ramp.

The LOS results for the Rothesay Road / Route 1 Access ramps during the critical peak period are summarized in Table 29. The results for the Rothesay Avenue / Route 1 Access ramps during the critical peak period are summarized in Table 30. Detailed results can be found in Appendix C.

By the 2023 horizon year with Phase 1 of the development in place the Rothesay Road / Route 1 on-ramp is projected to operate at LOS C with an average density of $13.9 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the PM peak period. The Rothesay Road / Route 1 off-ramp is projected to operate at LOS D with an average density of $19.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the Saturday peak period.

No operational deficiencies are projected at the Rothesay Road / Route 1 Access Ramps by the $\mathbf{2 0 2 3}$ horizon year with Phase 1 of the development in place.

Table 29 - LOS Analysis for Rothesay Rd/Rte 1 Access Ramps

| Ramp | LOS <br> Density (pc/km/ln) |
| :--- | :---: |
| Projected 2023 Horizon Year Conditions with Development |  |
| Rte 1 - Rothesay Rd off-ramp | C |
| (PM Peak) | 13.9 |
| Rte 1 - Rothesay Rd on-ramp | D |
| (AM Peak) | 19.6 |

By the 2023 horizon year with Phase 1 of the development in place the Rothesay Avenue / Route 1 on-ramp is projected to operate at LOS C with an average density of $15.8 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the PM peak period. The Rothesay Avenue / Route 1 off-ramp is projected to operate at LOS D with an average density of $21.3 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the Saturday peak period.

No operational deficiencies are projected at the Rothesay Avenue / Route 1 Access Ramps by the 2023 horizon year with Phase 1 of the development in place.

Table 30 - LOS Summary for Rothesay Ave/Rte 1 Access Ramps (Ph 1)

| Ramp | LOS <br> Density (pc/km/ln) |
| :--- | :---: |
| Projected 2023 Horizon Year Conditions with Development |  |
| Rte 1 - Rothesay Ave off-ramp | C |
| (AM Peak) | 15.8 |
| Rte 1 - Rothesay Ave on-ramp | D |
| (PM Peak) | 21.3 |

### 5.1.12 Ashburn Road Site Access Intersections (1-5)

There are 9 proposed access locations to the development located on Ashburn Road (in addition to the Ashburn Road / Jones Drive access). For the 2023 horizon year with Phase 1 of the development in place, it was assumed that the first 5 access points beginning closest to Rothesay Road / Ashburn Road would be in operation. The LOS for the projected 2023 horizon year traffic volumes for PM and Saturday peak hours with development are presented in Table 31 for the 5 accesses on Ashburn Road. Note that the accesses have been analyzed assuming the recommended geometry described below. The analysis output can be found in Appendix C.

It is recommended to implement separate left turn lanes at all access points on all approaches to accommodate future traffic demand at the development. It is also recommended to implement a traffic signal at the main Ashburn Road access to the development (access 5 in this analysis). The traffic signals should have full detection on all approaches.

By 2023 with Phase 1 of the development in place, the first access off of Rothesay Road on Ashburn Road (primarily access to the truck stop, assuming Rothesay Road / Fulton Lane access is right-in/right-out only) is projected to operate at an overall LOS A with an intersection delay of 4 seconds/vehicle or less during both the PM and Saturday peak period. All individual movements are projected to operate at LOS A with average delays of 9 seconds/vehicle or less and $\mathrm{v} / \mathrm{c}$ ratios of 0.10 or less during both the PM and Saturday peak period.

By 2023 with Phase 1 of the development in place, the second access along Ashburn Road (just south of Drury Cove Road, primarily access to Kenworth Dealership) is projected to operate at an overall LOS A with an intersection delay of 1 second/vehicle during both the PM and Saturday peak period. During the PM peak period, the eastbound left turn movement is projected to operate at LOS C (average delay of 21 seconds/vehicle). During the Saturday peak period the eastbound left turn movement is projected to operate at LOS B (average delay of 12 seconds/vehicle). All other movements during both the PM and Saturday peak period are projected to operate at LOS A with an average delay of 9 seconds/vehicle or less.

By 2023 with Phase 1 of the development in place, the third access along Ashburn Road (primarily access to a restaurant) is projected to operate at LOS A during both the PM and Saturday peak period. The westbound left turn and right turn movements are projected to operate at LOS C with an average delay of 22 seconds/vehicle or less during the PM peak period and at LOS B with an average delay of 13 seconds/vehicle or less. The southbound left turn movement is projected to operate at LOS A with an average delay of 10 seconds/vehicle or less during both peak periods.

By 2023 with Phase 1 of the development in place, the fourth access along Ashburn Road (primarily access to the UHaul Storage Facility) is projected to operate at an overall LOS A with minimal intersection delay during both the PM and Saturday peak period. During the PM peak period, the eastbound left turn movement is projected to operate at LOS C (average delay of 21 seconds/vehicle). During the Saturday peak period the eastbound left turn movement is projected to operate at LOS B (average delay of 13 seconds/vehicle). All other movements during both the PM and Saturday peak period are projected to operate at LOS A with an average delay of 10 seconds/vehicle or less.

The main Ashburn Road access from Rothesay Avenue is projected to operate at an overall LOS A with an intersection delay of 7 seconds/vehicle or less during the PM and Saturday peak period by 2023 with Phase 1 of the development in place. All individual movements are projected to operate at LOS B with an average delay of 18 seconds/vehicle or less during both peak periods. The exception is the westbound left turn movement during the PM peak period, which is projected to operate at LOS C with an average delay of 32 seconds/vehicle. The $\mathrm{v} / \mathrm{c}$ ratios for each of the individual movements is 0.48 or less.

No operational deficiencies are projected at the Ashburn Road access intersections under recommended geometry and traffic control conditions by 2023 with Phase 1 of the development in place.

Table 31 - LOS Summary for Ashburn Road Access Points with Development (Ph 1)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOSAverage Delay (seconds per vehicle)[Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Access |  | Access |  |  | Ashburn Rd |  |  | Ashburn Rd |  |  |
|  |  |  |  | $4$ |  | $4$ |  | $\stackrel{R}{R}$ |  | ${ }^{\mathbf{T}}$ | R | $\xrightarrow{4}$ |  | $\xrightarrow{R}$ |
| Projected 2023 Horizon Year with Development Conditions Access 1 (truck stop) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Access 1 | STOP | PM Peak | $\begin{aligned} & \text { A } \\ & 4 \end{aligned}$ | free flow |  | $\begin{gathered} \hline \text { A } \\ 8 \\ {[0.10]} \\ \hline \end{gathered}$ | free flow |  | $\begin{gathered} \mathrm{A} \\ 0 \\ {[0.00]} \\ \hline \end{gathered}$ |  | $\begin{gathered} \mathrm{A} \\ 9 \\ {[0.01]} \\ \hline \end{gathered}$ |  |  |  |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 3 \end{aligned}$ | free flow |  | A 8 $[0.10]$ | free flow |  | A 0 $[0.00]$ |  | $\begin{gathered} \hline \mathrm{A} \\ 9 \\ {[0.01]} \end{gathered}$ |  |  |  |
| Projected 2023 Horizon Year with Development Conditions Access 2 (south of Drury Cove Rd) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Access 2 | STOP | PM Peak | $\begin{gathered} A \\ 1 \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 21 \\ {[0.01]} \\ \hline \end{gathered}$ | $A$ 9 $[0.04]$ |  |  |  | $\begin{gathered} \hline \mathrm{A} \\ 8 \\ {[0.02]} \\ \hline \end{gathered}$ | free flow |  |  | free | low |
|  |  | Sat Peak | A | $\begin{gathered} \hline B \\ 12 \\ {[0.00]} \\ \hline \end{gathered}$ | A 9 $[0.02]$ |  |  |  | $\begin{gathered} \hline \mathrm{A} \\ 8 \\ {[0.03]} \\ \hline \end{gathered}$ | free flow |  |  | free | low |
| Projected 2023 Horizon Year with Development Conditions Access 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Access 3 | STOP | PM Peak | $\begin{aligned} & \mathrm{A} \\ & 0 \end{aligned}$ |  |  | $\begin{gathered} \hline C \\ 22 \\ {[0.08]} \\ \hline \hline \end{gathered}$ |  | $\begin{gathered} \hline C \\ 16 \\ {[0.01]} \\ \hline \end{gathered}$ | free flow |  |  | $\begin{gathered} \hline \text { A } \\ 10 \\ {[0.00]} \\ \hline \end{gathered}$ | free flow |  |
|  |  | Sat Peak | A 1 |  |  | $\begin{gathered} \hline B \\ 13 \\ {[0.07]} \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline B \\ 10 \\ {[0.01]} \\ \hline \end{gathered}$ | free flow |  |  | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | free flow |  |
| Projected 2023 Horizon Year with Development Conditions Access 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Access 4 | STOP | PM Peak | $\begin{aligned} & \mathrm{A} \\ & 0 \end{aligned}$ | $\begin{gathered} \hline \text { C } \\ 21 \\ {[0.01]} \\ \hline \end{gathered}$ | A 10 $[0.00]$ |  |  |  | $\begin{gathered} \text { A } \\ 8 \\ {[0.00]} \\ \hline \end{gathered}$ | free flow |  |  | free | fow |
|  |  | Sat Peak | $\begin{aligned} & \mathrm{A} \\ & 0 \end{aligned}$ | B 13 $[0.00]$ | A 9 $[0.01]$ |  |  |  | A 8 $[0.00]$ | free flow |  |  | free | fow |
| Projected 2023 Horizon Year with Development Conditions Access 5 (main Rothesay Avenue access) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Access 5 (main) |  | PM Peak | $\begin{aligned} & \text { A } \\ & 7 \end{aligned}$ | $\begin{gathered} \hline \text { B } \\ 17 \\ {[0.01]} \\ \hline \hline \end{gathered}$ | B  <br> 18 shared <br> $[0.05]$  <br> $B$  | $\begin{gathered} \hline \text { C } \\ 32 \\ {[0.23]} \\ \hline \hline \end{gathered}$ | $B$ 11 $[0.48]$ | shared | $\begin{gathered} \text { A } \\ 2 \\ {[0.00]} \\ \hline \end{gathered}$ | A 6 $[0.58]$ | shared | $\begin{gathered} \text { A } \\ 5 \\ {[0.25]} \\ \hline \hline \end{gathered}$ | $A$ 3 $[0.10]$ | shared |
|  |  | Sat Peak | $\begin{aligned} & A \\ & 6 \end{aligned}$ | $\begin{gathered} \hline A \\ 10 \\ {[0.01]} \\ \hline \end{gathered}$ | B  <br> 11 shared <br> $[0.06]$  | $\begin{gathered} \hline \hline B \\ 11 \\ {[0.07]} \\ \hline \end{gathered}$ | A 6 $[0.42]$ | shared | $\begin{gathered} \hline \hline \mathrm{A} \\ 5 \\ {[0.00]} \\ \hline \end{gathered}$ | $A$ 5 $[0.21]$ | shared | $\begin{gathered} \hline \text { A } \\ 6 \\ {[0.17]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { A } \\ 5 \\ {[0.08]} \\ \hline \end{gathered}$ | shared |

## 6 Impact of Ashburn Underpass

Following the analysis for Phase 1, it was determined that additional traffic generated by Phase 2 and 3 of the development could not be adequately accommodated without major modifications to the existing road network such as:

1. Major upgrades to the Route 100 interchange area to increase capacity; or
2. Construction of a new underpass near Ashburn Lake Road and Foster Thurston Road.

The NB Department of Transportation \& Infrastructure has been assessing the long-term need for a new underpass connection in the vicinity of the Ashburn Lake Road and Foster Thurston Drive ramps. If/when a new underpass is built, a significant amount of existing traffic is expected to divert away from the Route 100 Interchange, thus alleviating some of the existing operational issues at this location. While a significant portion of newly generated traffic from the development would also use the new Ashburn Lake Road underpass, its construction has merit regardless of whether the development proceeds.

### 6.1 Redistribution of Existing Traffic

Once the new underpass structure is built, there will be an immediate redistribution of traffic. For the purposes of this study, it was assumed the following redistribution will occur:

1. $30 \%$ of existing WB off-ramp traffic at Route 100 interchange will divert to the WB off ramp at the Ashburn underpass;
2. $80 \%$ of the existing left turn movement from Foster Thurston onto Ashburn Road will divert to the new EB on-ramp at Ashburn underpass;
3. Existing traffic from Rothesay Road to Rothesay Avenue (towards Route 1 EB and Rothesay Avenue south) will also decrease by $80 \%$ (as a consequence of traffic being redistributed in Assumption \#2);
4. $30 \%$ of existing through traffic from Rothesay Road (east) to Rothesay Avenue will divert to the new Ashburn underpass, $50 \%$ of existing traffic from Rothesay Road (from Ashburn Road) to Rothesay Avenue will also divert to the new Ashburn underpass from Foster Thurston Drive / Ashburn Road.
5. Existing traffic from Rothesay Avenue to Route 1 WB will decrease by $75 \%$
6. Traffic from Ashburn Lake Road to Route 1 WB will increase by the inverse of the current AM/PM peak hour volumes at the EB off-ramp at Ashburn Lake Road and by the estimated westbound traffic onto Ashburn Lake Road for the Saturday peak hour.

The net redistribution of existing traffic based on the above assumptions is depicted graphically in Figure 15 and applied to the intersections within the Study Area. The anticipated redistribution of existing traffic on the entire road network within the Study Area is shown in Figure 16 and Figure 17.


Figure 15 - Anticipated Traffic Redistribution attributed to new Ashburn Underpass


Figure 16 - Redistributed Existing (2016) Traffic with Ashburn Underpass (1 of 2) - PM/SAT


Figure 17 - Redistributed Existing (2016) Traffic with Ashburn Underpass (2 of 2) - PM/SAT

### 6.2 Revised Trip Assignment

The generated traffic was re-assigned to the Study Area assuming the Ashburn underpass is in place. Trips were assigned to the access points based on origin of the generated traffic as well as anticipated signing for the development as it is expected that Route 1 traffic will be encouraged to use the Ashburn underpass. The assumptions utilized for assigning the generated traffic to the development access points are as follows:

- Traffic from East (Rothesay Road) - 100\% use Rothesay Road / Ashburn Road access;
- Traffic from East (Route 1) - 20\% use Foster Thurston / Ashburn Road access, $65 \%$ use Rothesay Road / Rothesay Avenue access, and 15\% use Rothesay Road / Ashburn Road access;
- Traffic from West (Route 1) - 30\% use Foster Thurston / Ashburn Road access (Ashburn underpass), 60\% use Rothesay Road / Rothesay Avenue access, and 10\% use Rothesay Road / Ashburn Road access;
- Traffic from South - 50\% use Rothesay Avenue / Rothesay Road access from Rothesay Avenue, 10\% use Rothesay Road / Rothesay Avenue access from Ashburn Lake Road onramps to Route 1, and 40\% use Foster Thurston / Ashburn Road access from Ashburn underpass, and;
- Traffic from North - 100\% use Foster Thurston / Ashburn Road access.

Figure 18, Figure 19, and Figure 20 shows the traffic assignment for Phase 1, 2, and 3 (2033 Full Build Out Horizon Year).


Figure 18 - Revised Trip Assignment Full Build Out with Ashburn Underpass (1 of 3) - PM/SAT


Figure 19 - Revised Trip Assignment Full Build Out with Ashburn Underpass (2 of 3) - PM/SAT


Figure 20 - Revised Trip Assignment Full Build Out with Ashburn Underpass (3 of 3) - PM/SAT

## 7 Future Traffic Operations - Phase 2 and 3

### 7.1 2033 Horizon Year Levels of Service (Full Build Out)

The 2033 horizon year operational conditions were established to determine how the street network within the Study Area is projected to function with the full development and the Ashburn underpass in place. Traffic operations within the Study Area were evaluated using projected 2033 traffic volumes with the Ashburn underpass and development, as well as with recommended improvements to accommodate Phase 1 of the development.

It is important to note that the concept of the Ashburn underpass is in the preliminary phase and the exact configuration has not been determined. Results are based on the preliminary configuration described in the Route 1 corridor study performed by exp in 2016. Results for the development access points will not be affected, however, intersections west of the development may change as more details for the Ashburn underpass become available.

### 7.1.1 Foster Thurston Drive / Ashburn Road

The Foster Thurston Drive / Ashburn Road intersection is one of the access points to the proposed development. It is also one of the ramp terminals (northern end) of the potential Ashburn underpass.

At a minimum, it is recommended to implement fully-actuated signals at the Foster Thurston Drive / Ashburn Road ramp terminal intersection as well as implement separate left turn lanes at all four approaches and separate right turn lanes at the northbound and southbound (Ashburn Road) approaches to accommodate the increase in traffic that will be diverted as a result of the Ashburn underpass. All approaches should have channelization and the turning bays long enough that the $95^{\text {th }}$ percentile queues do not block any lanes. Note that the Ashburn underpass concept has not been finalized and the required ramp terminal configuration may change as a result.

The LOS for the projected 2033 horizon year traffic volumes for PM and Saturday peak hours with the Ashburn underpass and full development in place as well as the above recommended road geometry and traffic control are presented in Table 32 for the Foster Thurston Drive / Ashburn Road ramp terminal intersection. The analysis output can be found in Appendix $\mathbf{D}$.

By 2033 with the Ashburn underpass and full development in place and the recommended intersection geometry and traffic control, the Foster Thurston Drive / Ashburn Road ramp terminal intersection is projected to operate at an overall LOS B with an intersection delay of 19 seconds/vehicle or less during both the PM and Saturday peak periods. All individual movements are projected to operate at LOS C or better with average delays of 33 seconds/vehicle or less. All movements have a $\mathrm{v} / \mathrm{c}$ ratio of 0.87 or less. The $95^{\text {th }}$ queue lengths at the westbound approach (i.e. the Route 1 off ramp) are not projected to exceed 75 m , which is well below the length of the ramp.

No operational deficiencies are projected for the Foster Thurston Drive / Ashburn Road ramp terminal intersection by 2033 with the Ashburn underpass and full development in place with the recommended intersection geometry and traffic control.

Table 32 - LOS Summary for Foster Thurston Dr/Ashburn Rd with Development (Full Build Out)

| Intersection |  |  | Overall <br>  <br> Delay <br> (sec/veh) | Turning Movements LOSAverage Delay (seconds per vehicle)[Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street <br> @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound Ashburn Rd |  |  | Southbound <br> Ashburn Rd |  |  |
|  |  |  |  |  | er Thu |  |  | r Thu |  |  |  |  |  |  |  |
|  |  |  |  | $\stackrel{L}{4}$ | $\underline{\mathbf{T}}$ | $\stackrel{R}{R}$ | $4$ | $\stackrel{\mathbf{T}}{\mathbf{1}}$ |  |  | ${ }_{\mathbf{T}}^{\mathbf{T}}$ | $\xrightarrow{R}$ | $4$ |  | $\xrightarrow{R}$ |
| Projected 2033 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Foster Thurston |  | PM Peak | $\begin{gathered} \text { B } \\ 19 \end{gathered}$ | $\begin{gathered} \hline B \\ 13 \\ {[0.48]} \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ 21 \\ {[0.87]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \text { C } \\ 31 \\ {[0.76]} \\ \hline \end{gathered}$ | $\begin{gathered} C \\ 22 \\ {[0.43]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \text { B } \\ 12 \\ {[0.01]} \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ 30 \\ {[0.69]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { A } \\ 6 \\ {[0.49]} \\ \hline \end{gathered}$ | $\begin{gathered} \text { B } \\ 17 \\ {[0.41]} \\ \hline \end{gathered}$ | $\begin{gathered} \text { B } \\ 18 \\ {[0.34]} \\ \hline \end{gathered}$ | $\left.\begin{array}{c}\text { A } \\ 4 \\ {[0.29]}\end{array}\right]$ |
|  |  | Sat Peak | $\begin{gathered} \text { B } \\ 18 \end{gathered}$ | $C$ 20 $[0.46]$ | B 16 $[0.57]$ | shared | C 33 $[0.83]$ | $C$ 28 $[0.65]$ | shared | A 8 $[0.01]$ | $C$ 24 $[0.71]$ | A 5 $[0.57]$ | $B$ 11 $[0.35]$ | $\begin{gathered} \hline \hline B \\ 14 \\ {[0.46]} \\ \hline \end{gathered}$ | A 1 $[0.19]$ |

### 7.1.2 Foster Thurston Drive / NB Route 1 Access Ramps

The AM peak period was analyzed for the Foster Thurston Drive / Route 1 on-ramp and off-ramp because the directional split on Route 1 westbound is significantly higher during this period, therefore, the critical operational deficiencies occurring at these access ramps as a result of the development would occur during the AM peak period.
The results of the LOS analysis under projected 2033 traffic volumes with the Ashburn underpass and the full development are presented in Table 33 for the Foster Thurston Drive / NB Route 1 Access Ramps. The detailed analysis output can be found in Appendix D.
By 2033 with the Ashburn underpass and the full development in place, the Foster Thurston Drive / Route 1 off-ramp is projected to operate at LOS D with an average density of $18.1 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the AM peak period. The Foster Thurston Drive / Route 1 on-ramp is projected to operate at LOS D with an average density of $20.0 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the AM peak period.

No operational deficiencies are projected at the Foster Thurston Drive / Route 1 Access Ramps by 2033 with the Ashburn underpass and full development in place.

It is recommended to extend the acceleration lane from the Route 100 WB on-ramp to the start of the deceleration lane for the Foster Thurston WB off-ramp, introducing a weaving area. This recommendation was first made in the Route 1 Corridor Study performed by exp in 2016.

Table 33 - LOS Summary for Foster Thurston Dr/Rte 1 Access Ramps with Development (Full Build Out)

| Ramp | LOS <br> Density (pc/km/ln) |
| :--- | :---: |
| Projected 2023 Horizon Year Conditions with Development |  |
| Rte 1 - Foster Thurston Dr off-ramp  <br> (AM Peak) D <br> Rte 1 - Foster Thurston Dr on-ramp 18.1 <br> (AM Peak) D <br>  20.0. |  |

### 7.1.3 Ashburn Lake Road / NB Route 1 Access Ramps

The PM peak period was analyzed for the Ashburn Lake Road / Route 1 on-ramp and off-ramp because the directional split on Route 1 eastbound is significantly higher during this period, therefore, the critical operational deficiencies occurring at these access ramps as a result of the development would occur during the PM peak period.

The results of the LOS analysis under projected 2033 traffic volumes with the Ashburn underpass and the full development are presented in Table 34 for the Ashburn Lake Road / NB Route 1 Access Ramps. The detailed analysis output can be found in Appendix D.

By 2033 with the Ashburn underpass and the development in place, the Ashburn Lake Road / Route 1 off-ramp is projected to operate at LOS D with an average density of $20.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the PM peak period. The Ashburn Lake Road / Route 1 on-ramp is projected to operate at an unacceptable LOS F with an average density of $26.9 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the PM peak period. This is primarily a result of the increase in traffic from the north using the Ashburn underpass to access Route 1 eastbound.

No operational deficiencies are projected at the Ashburn Lake Road / Route 1 off-ramp by the 2033 horizon year with the Ashburn underpass and full development in place. The Ashburn Lake Road / Route 1 on-ramp is projected to have operational deficiencies by the 2033 horizon year with the Ashburn underpass and the full development in place.

It is recommended to extend the acceleration lane from the Ashburn Lake Road EB on-ramp to the start of the deceleration lane for the Route 100 EB off-ramp, introducing a weaving area. This will reduce congestion for the EB on-ramp at Ashburn Lake Road and reduce the flow interruptions on the EB lanes. This recommendation was first made in the Route 1 Corridor Study performed by exp in 2016.

Table 34 - LOS Summary for Ashburn Lake Rd/Rte 1 Access Ramps (Full Build Out)

| Ramp | LOS <br> Density (pc/km/ln) |
| :--- | :---: |
| Projected 2023 Horizon Year Conditions with Development |  |
| Rte 1 - Ashburn Lake Rd off-ramp | D |
| (PM Peak) | 20.6 |
| Rte 1 - Ashburn Lake Rd on-ramp | F |
| (PM Peak) | 26.9 |

### 7.1.4 Rothesay Avenue / Retail Drive / Ashburn Lake Road

The results of the LOS analysis under projected 2033 traffic volumes with the Ashburn underpass and full development are presented in Table 35 for the Rothesay Avenue / Retail Drive / Ashburn Lake Road intersection. The detailed analysis output can be found in Appendix D.

Although it was not within the scope of this study to do a detailed design of the potential future realignment at this location, a possible re-alignment lane configuration was completed in Synchro to determine the potential impact. In addition to Phase 1 recommendations, an additional separate right turn slip lane is recommended at the eastbound (Ashburn Lake Road) approach to accommodate the increase in traffic that will be diverted to this intersection as a result of the Ashburn underpass. This geometry may change depending on the final configuration of Ashburn Lake Road (i.e. whether it is a 2, 3, or 4 lane cross section).

By 2033 with the Ashburn underpass and full development in place as well as the additional eastbound right turn slip lane pocket, the Rothesay Avenue / Retail Drive / Ashburn Lake Road intersection is projected to operate at an overall LOS C with an intersection delay of 34 seconds/vehicle or less during both the PM and Saturday peak period. The lowest movements in
terms of LOS are the eastbound and northbound left turn movements during the Saturday peak period, which are projected to operate at LOS E with average delays of 61 seconds/vehicle or less. All other movements are projected to operate at satisfactory LOS D or better with average delays of 53 seconds/vehicle or less during both the PM and Saturday peak periods. The v/c ratio at the westbound approach is approaching capacity at 0.95 during both peak periods.

No operational deficiencies are projected at the Rothesay Avenue / Retail Drive / Ashburn Lake Road intersection by 2033 with the Ashburn underpass and full development in place with the preliminary recommended intersection geometry.

Table 35 - LOS Summary for Rothesay Ave/Retail Dr/Ashburn Lake Rd with Development (Full Build Out)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | ```Turning Movements LOS Average Delay (seconds per vehicle) [95\% Queues (m)]``` |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Ashburn Lake Rd |  |  | Retail Dr |  |  | Rothesay Ave |  |  | Rothesay Ave |  |  |
|  |  |  |  | $4$ |  | $\stackrel{R}{8}$ |  |  |  | $4$ |  | $\stackrel{R}{\text { R }}$ | 4 |  | $\xrightarrow{R}$ |
| Projected 2033 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Ave <br> @ Retail Dr / |  | PM Peak | $\begin{gathered} \text { C } \\ 29 \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 51 \\ {[0.85]} \\ \hline \end{gathered}$ | $\begin{gathered} C \\ 30 \\ {[0.74]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathbf{A} \\ 9 \\ {[0.57]} \\ \hline \end{gathered}$ | $\begin{gathered} \text { B } \\ 18 \\ {[0.41]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 53 \\ {[0.95]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \text { C } \\ 32 \\ {[0.73]} \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ 27 \\ {[0.81]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} C \\ 26 \\ {[0.55]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline B \\ 18 \\ {[0.65]} \\ \hline \end{gathered}$ | shared |
| Ashburn Lake Rd |  | Sat Peak | $\begin{gathered} C \\ 34 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 55 \\ {[0.90]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 26 \\ {[0.72]} \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 5 \\ {[0.45]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline B \\ 16 \\ {[0.41]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 52 \\ {[0.95]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline E \\ 61 \\ {[0.84]} \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 32 \\ {[0.71]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{D} \\ 54 \\ {[0.83]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 28 \\ {[0.80]} \end{gathered}$ | shared |

### 7.1.5 Rothesay Road / Fulton Lane

The LOS for the projected 2033 horizon year traffic volumes for PM and Saturday peak hours with the Ashburn underpass and development are presented in Table 36 for the Rothesay Road / Fulton Lane / Access intersection. The analysis output can be found in Appendix D.

By the 2033 horizon year with the Ashburn underpass and the full development in place, the Rothesay Road / Fulton Lane / Access intersection is projected to operate at an overall LOS A during the PM and Saturday peak period. During the PM peak period, the westbound movement is projected to operate at an unacceptable LOS F with average delays of 78 seconds/vehicle. There are very small volumes associated with the westbound right and left turn movement and the $\mathrm{v} / \mathrm{c}$ ratios at this approach is still well below the threshold despite the higher delays. All other movements are projected to operate at LOS C or better with average delays of 18 seconds/vehicle or less. During the Saturday peak period all movements are projected to operate at LOS C or better with an average delay of 16 seconds/vehicle or less. The v/c ratios are projected to be 0.31 or less during both the PM and Saturday peak period.

Operational deficiencies are projected at the Rothesay Road / Fulton Lane / Access intersection during the PM peak period at the westbound approach by the 2033 horizon year with the Ashburn underpass and the full development in place. This movement is associated with a very small volume and the $\mathrm{v} / \mathrm{c}$ ratio is well below the threshold of 1.0 .

Table 36 - LOS Summary for Rothesay Rd/Fulton Ln/Access with Development (Full Build Out)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOSAverage Delay (seconds per vehicle)[Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound <br> Rothesay Rd |  | Southbound |  |  |
|  |  |  |  | Access |  |  | Fulton Ln |  |  |  |  | Rothesay Rd |  |  |
|  |  |  |  | 4 | $\underline{\mathbf{T}}$ |  |  |  |  | 4 | ${ }^{\top}$ | 4 |  | $\stackrel{R}{ }$ |
| Projected 2023 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd <br> @ Fulton Ln / Access | STOP | PM Peak | $\begin{aligned} & A \\ & 2 \end{aligned}$ |  | $\begin{gathered} \hline \mathrm{C} \\ 18 \\ {[0.31]} \\ \hline \end{gathered}$ | shared | shared | $\begin{gathered} \hline F \\ 78 \\ {[0.18]} \\ \hline \hline \end{gathered}$ | shared |  | free flow | shared | $\begin{gathered} \hline B \\ 11 \\ {[0.01]} \\ \hline \end{gathered}$ | shared |
|  |  | Sat Peak | A 1 |  | $\begin{gathered} \hline B \\ 11 \\ {[0.05]} \end{gathered}$ | shared | shared | $\begin{gathered} \hline \hline \mathrm{C} \\ 16 \\ {[0.03]} \end{gathered}$ | shared |  | free flow | shared | $A$ 8 $[0.00]$ | shared |

### 7.1.6 Ashburn Road / Jones Drive

The Ashburn Road / Jones Drive intersection is to be utilized by the 2033 horizon year as an access to the development from Ashburn Road.

The LOS for the projected 2033 horizon year traffic volumes for PM and Saturday peak hours with the Ashburn underpass and full development in place are presented in Table 37 for the Ashburn Road / Jones Drive intersection. The analysis output can be found in Appendix D.

By the 2033 horizon year with the Ashburn underpass and full development in place, the Ashburn Road / Jones Drive intersection is projected to operate at an overall LOS A during the PM and Saturday peak periods. The eastbound and westbound left turn movements are projected to operate the lowest in terms of LOS at LOS E or better with an average delay of 50 seconds/vehicle or less during both peak periods. These movements were analyzed assuming stop control conditions and are associated with small volumes. All other movements are projected to operate at LOS B or better with average delays of 14 seconds/vehicle or less during both peak periods.

No operational deficiencies are projected at the Ashburn Road / Jones Drive intersection by the 2033 horizon year with the Ashburn underpass and the full development in place. This access should be re-evaluated in the future as more details with respect to the development become available to determine if signals are warranted.

Table 37 - LOS Summary for Ashburn Rd/Jones Dr/Access with Development (Full Build Out)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Jones Dr |  |  |  |  |  |  | Ashburn R |  |  | Ashburn R |  |
|  |  |  |  | $\mathbf{L}$ |  | R |  |  | $\xrightarrow{\mathrm{R}}$ |  | ${ }^{\mathbf{T}}$ |  |  | ${ }^{\mathbf{T}}$ | $\xrightarrow{R}$ |
| Projected 2023 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ashburn Rd @ Jones Dr | STOP | PM Peak | $\begin{gathered} \text { A } \\ 1 \end{gathered}$ | $\begin{gathered} \hline E \\ 39 \\ {[0.02]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 13 \\ {[0.00]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline E \\ 42 \\ {[0.11]} \\ \hline \hline \end{gathered}$ | $\begin{gathered} \hline B \\ 13 \\ {[0.01]} \\ \hline \hline \end{gathered}$ | shared | $\begin{gathered} \hline \text { A } \\ 9 \\ {[0.01]} \\ \hline \end{gathered}$ | free flow | shared | $\begin{gathered} \hline \text { A } \\ 9 \\ {[0.04]} \\ \hline \hline \end{gathered}$ | free flow | shared |
|  |  | Sat Peak | $\begin{aligned} & \text { A } \\ & 2 \end{aligned}$ | $\begin{gathered} \hline \mathrm{D} \\ 34 \\ {[0.02]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline B \\ 11 \\ {[0.00]} \end{gathered}$ | shared | $\begin{gathered} \hline E \\ 50 \\ {[0.39]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline B \\ 14 \\ {[0.03]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \mathrm{A} \\ 9 \\ {[0.00]} \\ \hline \end{gathered}$ | free flow | shared | $\begin{gathered} \hline \mathrm{A} \\ 9 \\ {[0.02]} \end{gathered}$ | free flow | shared |

### 7.1.7 Ashburn Road / Drury Cove Road

The LOS for the projected 2033 horizon year traffic volumes for PM and Saturday peak hours with the Ashburn underpass and the full development in place are presented in Table 38 for the Ashburn Road / Drury Cove Road intersection. The analysis output can be found in Appendix D.

By the 2033 horizon year with the Ashburn underpass and the full development in place, the Ashburn Road / Drury Cove Road is projected to operate at an overall LOS A during both the PM and Saturday peak period. All individual movements are projected to operate at LOS B or better with average delays of 14 seconds/vehicle or less.

No operational deficiencies are projected at the Ashburn Road / Drury Cove Road intersection by the 2033 horizon year with the Ashburn underpass and the full development in place. No recommended changes are needed at the Ashburn Road / Drury Cove Road intersection.

Table 38 - LOS Summary for Ashburn Rd/Drury Cove Rd with Development (Full Build Out)

| Intersection |  |  | Overall <br>  <br> Delay <br> (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  | Westbound |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Ashburn Rd |  | Ashburn Rd |  |  |  |  |  | Co |  |
|  |  |  |  | L $\mathbf{T}$ <br> $\mathbf{1}$  | R | $\stackrel{L}{4}$ |  | 4 | ${ }^{\mathbf{T}}$ | R | $\frac{L}{4}$ | ${ }^{\mathbf{T}}$ | $\xrightarrow{\text { R }}$ |
| Projected 2023 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Drury Cove @ Ashburn Rd | STOP | PM Peak <br> Sat Peak | $\begin{aligned} & \text { A } \\ & 1 \end{aligned}$ | A  <br> 8 shared <br> $[0.00]$  |  |  | free flow |  |  |  | $\begin{gathered} \hline \text { B } \\ 14 \\ {[0.07]} \\ \hline \end{gathered}$ |  | shared |
|  |  |  | A 0 | A  <br> 0 shared <br> $[0.00]$  |  |  | free flow |  |  |  | $\begin{gathered} \hline \text { B } \\ 13 \\ {[0.04]} \\ \hline \end{gathered}$ |  | shared |

### 7.1.8 Rothesay Avenue / Rothesay Road

The Rothesay Road / Rothesay Avenue intersection will be the main access to the proposed development. The LOS for the projected 2033 horizon year traffic volumes with the Ashburn underpass and the full development in place for PM and Saturday peak hours with development are presented in Table 39 for the Rothesay Road / Rothesay Avenue intersection. The analysis output can be found in Appendix $\mathbf{D}$.

By the 2033 horizon year with the Ashburn underpass and the full development in place the Rothesay Road / Rothesay Avenue intersection is projected to operate at an overall LOS C with an intersection delay of 26 seconds/vehicle during the PM peak period and LOS D with an intersection delay of 39 seconds/vehicle during the Saturday peak period. The worst movement in terms of LOS is the northbound left turn movement during the Saturday peak period, which is projected to operate at an acceptable LOS E with an average delay of 68 seconds/vehicle and the eastbound through movement during the PM peak period, which is projected to operate at LOS E with an average delay of 58 seconds/vehicle. The $\mathrm{v} / \mathrm{c}$ ratios at these movements are approaching capacity. All other movements are projected to operate at LOS D or better with average delays of 52 seconds/vehicle or less during both peak periods. The $95^{\text {th }}$ percentile queues are projected to be 166 m or less at the northbound approach, 204 m or less on the westbound through approach, 194 m or less on the eastbound approach, and 77 m or less on the southbound approach during both the PM and Saturday peak period.

No operational deficiencies are projected by the 2033 horizon year with the Ashburn underpass and the full development in place at the Rothesay Road / Rothesay Avenue intersection with fully-actuated, coordinated signals implemented.

Table 39 - LOS Summary for Rothesay Rd/Rothesay Ave with Development (Full Build Out)

| Intersection |  |  | Overall LOS \& Delay (sec/veh) | Turning Movements LOS <br> Average Delay (seconds per vehicle) <br> [Volume to Capacity Ratio (v/c)] |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Rothesay Ave |  |  | Rothesay Ave |  |  | Rothesay Rd |  |  | Rothesay Rd |  |  |
|  |  |  |  |  |  |  |  |  |  | 4 | $\mathbf{T}$ |  | 4 | ${ }^{\top}$ | $\stackrel{R}{R}$ |
| Existing (2016) Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Projected 2033 Horizon Year with Development Conditions and Recommended Option (Actuated Coordinated Signal) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rothesay Rd @ |  | PM Peak | $\begin{gathered} C \\ 26 \end{gathered}$ | $\begin{gathered} \text { C } \\ 26 \\ {[0.12]} \\ \hline \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{E} \\ 58 \\ {[0.90]} \\ \hline \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 7 \\ {[0.48]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 26 \\ {[0.11]} \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ 41 \\ {[0.78]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathbf{A} \\ 0 \\ {[0.30]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 14 \\ {[0.59]} \\ \hline \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ 27 \\ {[0.87]} \\ \hline \end{gathered}$ | shared | $\begin{gathered} \hline \text { C } \\ 31 \\ {[0.75]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 19 \\ {[0.43]} \\ \hline \end{gathered}$ | shared |
| Rothesay Ave |  | Sat Peak | $\begin{gathered} \text { D } \\ 39 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 20 \\ {[0.17]} \end{gathered}$ | $\begin{gathered} \hline \hline \mathrm{D} \\ 52 \\ {[0.95]} \end{gathered}$ | A 8 $[0.39]$ | $\begin{gathered} \hline \hline \mathrm{C} \\ 25 \\ {[0.38]} \end{gathered}$ | $\begin{gathered} \hline \hline \text { D } \\ 49 \\ {[0.91]} \end{gathered}$ | A 0 $[0.17]$ | $\begin{gathered} \hline \hline \mathrm{E} \\ 68 \\ {[0.99]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 27 \\ {[0.51]} \end{gathered}$ | shared | $\begin{gathered} \hline \hline C \\ 23 \\ {[0.57]} \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 42 \\ {[0.71]} \\ \hline \end{gathered}$ | shared |

### 7.1.9 Rothesay Road / Ashburn Road

The Rothesay Road / Ashburn Road intersection is a secondary access off Rothesay Road to the proposed development. The LOS for the projected 2033 horizon year volumes for PM and Saturday peak hours with the Ashburn underpass and full development in place are presented in Table 40 for the Rothesay Road / Ashburn Road intersection. The analysis output can be found in Appendix D.

By the 2033 horizon year with the Ashburn underpass and the full development in place, the Rothesay Road / Ashburn Road intersection is projected to operate at an overall LOS A during the PM and Saturday peak periods The worst movement in terms of LOS is the eastbound left turn movement (from the development), which is projected to operate at LOS D with an average delay of 42 seconds/vehicle during the PM peak period and 40 seconds/vehicle during the Saturday peak period. The $95^{\text {th }}$ percentile queue length on this approach is projected to be 37 m or less during both peak periods. All other movements are projected to operate at LOS A with average delays of 9 seconds/vehicle or less. The v/c ratios are all 0.69 or less.

No operational deficiencies are projected at the Rothesay Road / Ashburn Road intersection by the $\mathbf{2 0 3 3}$ horizon year with the Ashburn underpass and the full development in place.

Table 40 - LOS Summary for Rothesay Rd/Ashburn Rd with Development (Full Build Out)


### 7.1.10 Rothesay Avenue / NB Route 1 Interchange

The LOS for the projected 2033 horizon year traffic volumes for PM and Saturday peak hours with the Ashburn underpass and the full development in place are presented in Table 41 for the Rothesay Avenue / Route 1 off-ramp intersection, and Table 42 for the Rothesay Avenue / Route 1 on-ramp intersections (west and east). The analysis outputs can be found in Appendix D.

## Rothesay Avenue / Route 1 off-ramp Intersection

For analysis purposes, it is assumed that the recommendations made for Rothesay Avenue / Route 1 off-ramp intersection in the Phase 1 TIS will be in place by the 2033 horizon year (Phase 3 of the development). This includes implementing actuated coordinated signals as well as an eastbound through lane pocket to allow for a free-flowing independent right turn lane.

By the 2033 horizon year with the Ashburn underpass and the full development in place as well as coordinated traffic signals and an eastbound through lane pocket implemented, the Rothesay Avenue / Route 1 off-ramp intersection is projected to operate at an overall LOS A with an intersection delay of 8 seconds/vehicle during the PM peak period and at an overall LOS B with an intersection delay of 19 seconds/vehicle during the Saturday peak period. All individual movements are projected to operate at LOS C or better with an average delay of 21 seconds/vehicle or less and $\mathrm{v} / \mathrm{c}$ ratios of 0.57 or less during the PM peak period. During the Saturday peak period the southbound through movement is projected to operate at LOS D with an average delay of 38 seconds/vehicle. All other individual movements are projected to operate at LOS C or better with an average delay of 25 seconds/vehicle or less. The v/c ratio for each movement is 0.84 or less during both the PM and Saturday peak period. The $95^{\text {th }}$ percentile queue length at the southbound approach is not projected to exceed 131 m , which is still less than the length of the off-ramp.

No operational deficiencies are projected by 2033 with the Ashburn underpass and the full development in place at the Rothesay Avenue / Route 1 off-ramp intersection with coordinated signals and an eastbound through movement pocket implemented.

Table 41 - LOS Summary for Rothesay Ave/Rte1 off-ramp with Development (Full Build Out)


## Rothesay Avenue / Route 1 on-ramp Intersections

By the 2033 horizon year with the full development in place, both the Rothesay Avenue / Route 1 on-ramp intersections (east and west) are projected to operate at an overall LOS F during the Saturday peak period. The eastbound movements are projected to operate at LOS F at both the intersections during the Saturday peak period, these movements currently operate under stop control conditions. The intersections are projected to operate sufficiently during the PM peak period. The $95^{\text {th }}$ percentile queue lengths indicate that vehicles at the intersection furthest east may spill back to the
intersection furthest to the west, as the projected lengths exceed the short distance between the two intersections.

Operational deficiencies are projected by the 2033 with the Ashburn underpass as well as the full development in place at the Rothesay Avenue / Route 1 on-ramp intersections (east and west) at the eastbound approach during the Saturday peak periods. It is notable that operational deficiencies were identified at these locations in the TIS for Phase 1 of the development.

There are limited options with respect to changes to infrastructure geometry to improve traffic conditions at the Rothesay Avenue / Route 1 on-ramp intersections because of the overpass structure just west of this location. This location should be re-evaluated in the future when more details with respect to the development become available to determine if signals are warranted.

Table 42 - LOS Summary for Rothesay Ave/Rte 1 on-ramp with Development (Full Build Out)


### 7.1.11 NB Route 1 Access with Rothesay Road / Rothesay Avenue

The AM peak period was analyzed for the Rothesay Road / Route 1 on-ramp because the directional split on Route 1 westbound is significantly higher during the AM period. The PM peak period was analyzed for the Rothesay Road / Route 1 off-ramp because the directional split on Route 1 eastbound is significantly higher during the PM peak period. Therefore, the critical operational deficiencies occurring at these access ramps as a result of the development would occur during the AM peak period for the on-ramp and during the PM peak period for the off-ramp.

The LOS results for the 2033 horizon year with the Ashburn underpass and full development for the Rothesay Road / Route 1 Access ramps during the critical peak period are summarized in Table 43. The results for the Rothesay Avenue / Route 1 Access ramps during the critical peak period are summarized in Table 15. Detailed results can be found in Appendix D.

## Rothesay Road / Route 1 Access Ramps

By the 2033 horizon year with the Ashburn underpass and the full development in place the Rothesay Road / Route 1 on-ramp is projected to operate at LOS D with an average density of 17.5
$\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the PM peak period. The Rothesay Road / Route 1 off-ramp is projected to operate at an unacceptable LOS F with an average density of $23.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the Saturday peak period.

No operational deficiencies are projected at the Rothesay Road / Route 1 off-ramp by the 2033 horizon year with the Ashburn underpass and full development in place. Operational deficiencies are projected at the Rothesay Road / Route 1 Access Ramp on-ramp by the 2033 horizon year with the Ashburn underpass and the full Phase 1 of the development in place.

It is recommended to extend the acceleration lane from the Route 100 WB on-ramp to the start of the deceleration lane for the Foster Thurston WB off-ramp, introducing a weaving area. It is also recommended to extend the acceleration lane from the Ashburn Lake Road EB on-ramp to the start of the deceleration lane for the Route 100 EB off-ramp, introducing a weaving area. This will reduce congestion for the EB on-ramp at Ashburn Lake Road and WB on-ramp at Rothesay Road and reduce the flow interruptions on the EB and WB lanes. These recommendations were first made in the Route 1 Corridor Study performed by exp in 2016.

Table 43 - LOS Summary for Rothesay Rd/Rte 1 Access Ramps (Full Build Out)

| Ramp | LOS <br> Density (pc/km/ln) |
| :--- | :---: |
| Projected 2023 Horizon Year Conditions with Development |  |
| Rte 1 - Rothesay Rd off-ramp | D |
| (PM Peak) | 17.5 |
| Rte 1 - Rothesay Rd on-ramp | F |
| (AM Peak) | 23.2 |

## Rothesay Avenue / Route 1 Access Ramps

By the 2033 horizon year with the Ashburn underpass and the full development in place the Rothesay Avenue / Route 1 on-ramp is projected to operate at LOS D with an average density of $17.5 \mathrm{pc} / \mathrm{km} / \mathrm{In}$ during the PM peak. The Rothesay Avenue / Route 1 off-ramp is projected to operate at an unacceptable LOS $F$ with an average density of $23.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ during the Saturday peak period. It is notable that the Rothesay Avenue / Route 1 on-ramp just reaches unacceptable LOS at the 2033 horizon year, which is primarily due to the anticipated increase in Route 1 background traffic.

No operational deficiencies are projected at the Rothesay Avenue / Route 1 off-ramp by the 2033 horizon year the Ashburn underpass and the full development in place. Operational deficiencies are projected at the Rothesay Avenue / Route 1 on-ramp by the 2033 horizon year with the Ashburn underpass and the full development in place. This ramp should be monitored and re-evaluated as more details about the development are finalized.

Table 44 - LOS Summary for Rothesay Ave/Rte 1 Access Ramps (Full Build Out)

| Ramp | LOS <br> Density (pc/km/ln) |
| :--- | :---: |
| Projected 2023 Horizon Year Conditions with Development |  |
| Rte 1 - Rothesay Ave off-ramp D <br> (AM Peak) 19.2 <br> Rte 1 - Rothesay Ave on-ramp F <br> (PM Peak) 22.2$\$$. |  |

### 7.1.12 Ashburn Road Site Access Intersections (1-9)

There are 9 proposed access locations to the development located on Ashburn Road (in addition to the Ashburn Road / Jones Drive access). The LOS for the projected 2033 horizon year traffic volumes for PM and Saturday peak hours with development and the Ashburn underpass in place are presented in Table 45 for the 9 accesses on Ashburn Road. Note that the accesses have been analyzed assuming the recommended geometry described below. The analysis output can be found in Appendix B.

It is recommended to implement separate left turn lanes at all access points on all approaches to accommodate future traffic demand at the development. It is also recommended to implement a traffic signal at the main Ashburn Road access to the development (access 5 in this analysis). The traffic signals should have full detection on all approaches. In addition, access 8 in this analysis (directly east of Jones Drive) should have full-actuated signals implemented to accommodate the additional left turning traffic onto Ashburn Road towards Foster Thurston Drive as a result of the Ashburn underpass.

By 2033 the Ashburn underpass and full development in place, the first access off of Rothesay Road on Ashburn Road (primarily access to the truck stop, assuming Rothesay Road / Fulton Lane access is right-in/right-out only) is projected to operate at an overall LOS A during both the PM and Saturday peak period. All individual movements are projected to operate at LOS B or better with average delays of 10 seconds/vehicle or less during both the PM and Saturday peak period.

By 2033 with the Ashburn underpass and the full development in place, the second access on Ashburn Road (just south of Drury Cove Road, primarily access to the proposed Kenworth Dealership) is projected to operate at an overall LOS A during both the PM and Saturday peak period. The eastbound left turn movement is projected to operate at LOS C with an average delay of 16 seconds/vehicle during both the PM and Saturday peak period. All other movements during both the PM and Saturday peak period are projected to operate at LOS B or better with an average delay of 10 seconds/vehicle or less.

By 2033 with the Ashburn underpass and the full development in place, the third access on Ashburn Road (primarily access to a proposed restaurant) is projected to operate at LOS A during both the PM and Saturday peak period. The westbound left turn movement is projected to operate at LOS C with an average delay of 17 seconds/vehicle or less during the PM and Saturday peak period. All other movements are projected to operate at LOS B or better with an average delay of 12 seconds/vehicle or less during both peak periods.

By 2033 with the Ashburn underpass and the full development in place, the fourth access on Ashburn Road (primarily access to the proposed UHaul Storage Facility) is projected to operate at an overall LOS A with minimal intersection delay during both the PM and Saturday peak period. The eastbound left turn movement is projected to operate at LOS C with an average delay of 17 seconds/vehicle or less during both peak periods. All other movements during both the PM and Saturday peak period are projected to operate at LOS B or better with an average delay of 11 seconds/vehicle or less.

The main Ashburn Road access from Rothesay Avenue (access 5 of this analysis) is projected to operate at an overall LOS B with an intersection delay of 12 seconds/vehicle during the PM peak period and at an overall LOS A with an intersection delay of 8 seconds/vehicle during the Saturday peak period by 2033 with the Ashburn underpass and the full development in place. All individual movements are projected to operate at LOS B with an average delay of 15 seconds/vehicle or less during both peak periods. The exception is the westbound left turn movement during the PM peak
period, which is projected to operate at LOS C with an average delay of 29 seconds/vehicle. The v/c ratios for each of the individual movements is 0.63 or less.

By 2033 with the Ashburn underpass and the full development in place, the fifth access on Ashburn Road (primarily access to the proposed major retail area) is projected to operate at an overall LOS A during both peak periods. All individual movements are projected to operate at LOS B or better with average delays of 14 seconds/vehicle or less. The exception is the westbound left turn movement, which is projected to operate at LOS D with an average delay of 34 seconds/vehicle during the PM peak and at LOS C with an average delay of 24 seconds/vehicle during the Saturday peak period.

The seventh access along Ashburn Road is primarily an access to the office area. By 2033 with the Ashburn underpass and full development in place, it is projected to operate at an overall LOS A during both peak periods. During the PM peak period, both the eastbound and westbound left turn movements (which operate under stop control conditions) are projected to operate at LOS E with average delays of 49 seconds/vehicle or less. During the Saturday peak period, the eastbound and westbound left turn movements are projected to operate at LOS E or better with average delays of 36 seconds/vehicle or less. The through/right turn movement is projected to operate at LOS C with an average delay of 22 seconds/vehicle or less during both peak periods. All other movements are projected to operate at LOS A during both peak periods. This access may require signalization in the future and should be re-evaluated when more details about the development are known.

The eighth access on Ashburn Road is expected to be the second main access on Ashburn Road in this analysis and primarily provides access to the residential area as well as the main retail area (to the south of Ashburn Road). Under signalized conditions, this access is projected to operate at an overall LOS A during both peak periods by 2033 with the Ashburn underpass and full development in place. The westbound left turn movement is projected to operate at LOS C with an average delay of 25 seconds/vehicle or less during both peak periods. All other movements are projected to operate at LOS B or better with an average delay of 17 seconds/vehicle or less during both peak periods. All movements have a $\mathrm{v} / \mathrm{c}$ ratio of 0.55 or less.

The final access on Ashburn Road is primarily an access to the gas station and convenience retail adjacent to Foster Thurston Drive. By 2033 with the Ashburn underpass and full development in place, this access is projected to operate at LOS A during the PM and Saturday peak periods. The eastbound left turn movement is projected to operate at LOS E with an average delay of 49 seconds/vehicle or less during both peak periods. All other movements are projected to operate at LOS B or better with average delays of 13 seconds/vehicle or less.

No operational deficiencies are projected at the Ashburn Road access intersections under recommended geometry and traffic control conditions by 2033 with the Ashburn underpass and full development in place. Results for the accesses are for proof of concept only. Additional accesses may require traffic signals and/or changes to geometry and should be reevaluated as more details about the development are finalized.

Table 45 - LOS Summary for Ashburn Road Access Points with Development (Full Build Out)


### 7.1.13 Ashburn Underpass Ramps Terminals

The Ashburn underpass ramp terminals include the Foster Thurston Drive / Ashburn Road intersection (analyzed previously) as well as the Ashburn underpass / Ashburn Lake Road intersection. The LOS analysis for the Ashburn underpass / Ashburn Lake Road ramp terminal with the Ashburn underpass and full development in place are shown in Table 46. Detailed analysis can be found in Appendix D.

Although it was not within the scope of this study to do a detailed design of the potential future ramp terminal at this location, a possible configuration was completed in Synchro to determine the potential impact. The configuration included fully actuated traffic signals and separate left turn and right turn pockets at all approaches.

Under this configuration, the Ashburn underpass / Ashburn Lake Road ramp terminal is projected to operate at an overall LOS B with an intersection delay of 19 seconds/vehicle or less during both peak periods. All individual movements are projected to operate at LOS C or better with average delays of 30 seconds/vehicle or less during both the PM and Saturday peak period. All movements have a $\mathrm{v} / \mathrm{c}$ ratio of 0.87 or less.

No operational deficiencies are projected at the Ashburn underpass / Ashburn Lake Road ramp terminal under the above described intersection geometry by 2033 with the Ashburn underpass and full development in place. Results are for proof of concept only and should be re-evaluated when the Ashburn underpass concept is finalized. The geometry for this intersection is also dependent on the final cross-section of Ashburn Lake Road.

Table 46 - LOS Summary for Ashburn underpass/Ashburn Lake Rd Ramp Terminal (Full Build Out)

| Intersection |  |  | Overall <br>  <br> Delay (sec/veh) | ```Turning Movements LOS Average Delay (seconds per vehicle) [95\% Queues (m)]``` |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North South Street @ East West Street | Traffic Control | Time Period |  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
|  |  |  |  | Ashburn Lake Rd |  |  | Retail Dr |  |  | Rothesay Ave |  |  | Rothesay Ave |  |  |
|  |  |  |  | $4$ |  | $\xrightarrow{\mathrm{R}}$ | 4 | ${ }^{\top}$ | $\stackrel{R}{\mathrm{R}}$ | 4 | ${ }^{\text {T }}$ | $\xrightarrow{\mathrm{R}}$ | 4 | ${ }^{\text {a }}$ | $\stackrel{R}{\mathrm{R}}$ |
| Projected 2033 Horizon Year with Development Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Underpass ramp terminal |  | PM Peak | $\begin{gathered} B \\ 13 \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 25 \\ {[0.61]} \end{gathered}$ | $\begin{gathered} \hline B \\ 13 \\ {[0.48]} \end{gathered}$ |  |  | $\begin{gathered} \hline B \\ 16 \\ {[0.64]} \end{gathered}$ | $\begin{gathered} \hline \text { A } \\ 3 \\ {[0.47]} \end{gathered}$ |  |  |  | $\begin{gathered} \hline C \\ 20 \\ {[0.74]} \end{gathered}$ |  | $\begin{gathered} \hline A \\ 6 \\ {[0.43]} \end{gathered}$ |
| / Ashburn Lake Rd |  | Sat Peak | $\begin{gathered} \text { B } \\ 19 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 17 \\ {[0.39]} \end{gathered}$ | $C$ 23 $[0.69]$ |  |  | C 25 $[0.50]$ | $\begin{gathered} \mathrm{A} \\ 8 \\ {[0.77]} \end{gathered}$ |  |  |  | $\begin{gathered} C \\ 30 \\ {[0.87]} \end{gathered}$ |  | $A$ 3 $[0.16]$ |

## 8 Conclusions

Projected traffic generated by Phase 1 of The Crossing can be adequately accommodated with relatively minor improvements to the existing road network (e.g. changes to traffic control, additional turn lanes, intersection realignment, etc).

Projected traffic generated by Phases 2 and 3 of the development will require major modifications to the existing road network such as:

1. Major upgrades to the Route 100 interchange area to increase capacity; or
2. Construction of a new underpass near Ashburn Lake Road and Foster Thurston Road.

Final details regarding recommended improvements will need to be tweaked as details of the development and the Ashburn underpass are finalized.

## Appendix A Site Plan

Figure 1 - Revised Conceptual Rendering of the Developed Site Plan


## Appendix B- <br> LOS Results without Development

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 7.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | \& |  |  | * |  |  | * |  |  | * |  |
| Traffic Vol, veh/h | 2 | 6 | 4 | 3 | 2 | 226 | 127 | 19 | 2 | 12 | 714 | 6 |
| Future Vol, veh/h | 2 | 6 | 4 | 3 | 2 | 226 | 127 | 19 | 2 | 12 | 714 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 7 | 4 | 3 | 2 | 246 | 138 | 21 | 2 | 13 | 776 | 7 |


| Major/Minor | Minor1 |  | Minor2 |  |  |  | Major1 |  |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1227 | 1107 | 22 |  | 1108 | 1104 | 779 |  | 783 | 0 | 0 | 23 | 0 | 0 |
| Stage 1 | 298 | 298 | - |  | 805 | 805 | - |  | - | - | - | - | - | - |
| Stage 2 | 929 | 809 | - |  | 303 | 299 | - |  | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 155 | 210 | 1055 |  | 187 | 211 | 396 |  | 835 | - | - | 1592 | - | - |
| Stage 1 | 711 | 667 | - |  | 376 | 395 | - |  | - | - | - | - | - | - |
| Stage 2 | 321 | 394 | - |  | 706 | 666 | - |  | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | 50 | 172 | 1055 |  | 156 | 173 | 396 |  | 835 | - | - | 1592 | - | - |
| Mov Cap-2 Maneuver | 50 | 172 | - |  | 156 | 173 | - |  | - | - | - | - | - | - |
| Stage 1 | 592 | 556 | - |  | 313 | 389 | - |  | - | - | - | - | - | - |
| Stage 2 | 119 | 388 | - |  | 579 | 555 | - |  | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | NB |  |  |  | SB |  |  |  | SE |  |  | NW |  |  |
| HCM Control Delay, s | 30.7 |  |  |  | 30.4 |  |  |  | 8.7 |  |  | 0.1 |  |  |
| HCM LOS | D |  |  |  | D |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | NWL | NWT | NWR | SEL | SET | SER | SBLn1 |  |  |  |  |  |  |
| Capacity (veh/h) | 153 | 1592 | - | - | 835 | - | - | 384 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.085 | 0.008 | - |  | - 0.165 | - | - | 0.654 |  |  |  |  |  |  |
| HCM Control Delay (s) | 30.7 | 7.3 | 0 | - | 10.2 | 0 | - | 30.4 |  |  |  |  |  |  |
| HCM Lane LOS | D | A | A | - | B | A | - | D |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0.3 | 0 | - | - | 0.6 | - | - | 4.5 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | $\ddagger$ |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 2 | 6 | 4 | 3 | 2 | 242 | 136 | 20 | 2 | 12 | 766 | 7 |
| Future Vol, veh/h | 2 | 6 | 4 | 3 | 2 | 242 | 136 | 20 | 2 | 12 | 766 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 7 | 4 | 3 | 2 | 263 | 148 | 22 | 2 | 13 | 833 | 8 |


| Major/Minor | Minor1 |  | Minor2 |  |  |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1313 | 1184 | 23 |  | 1187 | 1183 | 836 |  | 840 | 0 | 0 | 24 | 0 | 0 |
| Stage 1 | 318 | 318 | - |  | 863 | 863 | - |  | - | - | - | - | - | - |
| Stage 2 | 995 | 866 | - |  | 324 | 320 | - |  | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 135 | 189 | 1054 |  | 165 | 189 | 367 |  | 795 | - | - | 1591 | - | - |
| Stage 1 | 693 | 654 | - |  | 349 | 372 | - |  | - | - | - | - | - | - |
| Stage 2 | 295 | 370 | - |  | 688 | 652 | - |  | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | 32 | 151 | 1054 |  | 134 | 151 | 367 |  | 795 | - | - | 1591 | - | - |
| Mov Cap-2 Maneuver | 32 | 151 | - |  | 134 | 151 | - |  | - | - | - | - | - | - |
| Stage 1 | 562 | 530 | - |  | 283 | 366 | - |  | - | - | - | - | - | - |
| Stage 2 | 82 | 364 | - |  | 549 | 529 | - |  | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | NB |  |  |  | SB |  |  |  | SE |  |  | NW |  |  |
| HCM Control Delay, s | 41 |  |  |  | 40.7 |  |  |  | 9.1 |  |  | 0.1 |  |  |
| HCM LOS | E |  |  |  | E |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | NWL | NWT | NWR | SEL | SET | SER | SBLn1 |  |  |  |  |  |  |
| Capacity (veh/h) | 113 | 1591 | - | - | 795 | - | - | 355 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.115 | 0.008 | - |  | 0.186 | - | - | 0.756 |  |  |  |  |  |  |
| HCM Control Delay (s) | 41 | 7.3 | 0 | - | 10.6 | 0 | - | 40.7 |  |  |  |  |  |  |
| HCM Lane LOS | E | A | A | - | B | A | - | E |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0.4 | 0 | - | - | 0.7 | - | - | 6 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | $\uparrow$ |  |  | \& |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 2 | 6 | 4 | 4 | 2 | 254 | 143 | 21 | 2 | 12 | 805 | 7 |
| Future Vol, veh/h | 2 | 6 | 4 | 4 | 2 | 254 | 143 | 21 | 2 | 12 | 805 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 7 | 4 | 4 | 2 | 276 | 155 | 23 | 2 | 13 | 875 | 8 |


| Major/Minor | Minor1 |  | Minor2 |  |  |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1379 | 1244 | 24 |  | 1245 | 1241 | 879 |  | 883 | 0 | 0 | 25 | 0 | 0 |
| Stage 1 | 335 | 335 | - |  | 905 | 905 | - |  | - | - | - | - | - | - |
| Stage 2 | 1044 | 909 | - |  | 340 | 336 | - |  | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 122 | 174 | 1052 |  | 151 | 175 | 347 |  | 766 | - | - | 1589 | - | - |
| Stage 1 | 679 | 643 | - |  | 331 | 355 | - |  | - | - | - | - | - | - |
| Stage 2 | 277 | 354 | - |  | 675 | 642 | - |  | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | 21 | 136 | 1052 |  | 121 | 137 | 347 |  | 766 | - | - | 1589 | - | - |
| Mov Cap-2 Maneuver | 21 | 136 | - |  | 121 | 137 | - |  | - | - | - | - | - | - |
| Stage 1 | 540 | 511 | - |  | 263 | 349 | - |  | - | - | - | - | - | - |
| Stage 2 | 55 | 348 | - |  | 528 | 510 | - |  | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | NB |  |  |  | SB |  |  |  | SE |  |  | NW |  |  |
| HCM Control Delay, s | 55.6 |  |  |  | 54.5 |  |  |  | 9.4 |  |  | 0.1 |  |  |
| HCM LOS | F |  |  |  | F |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | NWL | NWT | NWR | SEL | SET | SER | SBLn1 |  |  |  |  |  |  |
| Capacity (veh/h) | 84 | 1589 | - | - | 766 | - | - | 333 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.155 | 0.008 | - |  | 0.203 | - | - | 0.849 |  |  |  |  |  |  |
| HCM Control Delay (s) | 55.6 | 7.3 | 0 | - | 10.9 | 0 | - | 54.5 |  |  |  |  |  |  |
| HCM Lane LOS | F | A | A | - | B | A | - | F |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0.5 | 0 | - | - | 0.8 | - | - | 7.6 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 17.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | \& |  |  | \& |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 2 | 6 | 4 | 4 | 2 | 267 | 150 | 22 | 2 | 12 | 846 | 7 |
| Future Vol, veh/h | 2 | 6 | 4 | 4 | 2 | 267 | 150 | 22 | 2 | 12 | 846 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 7 | 4 | 4 | 2 | 290 | 163 | 24 | 2 | 13 | 920 | 8 |


| Major/Minor | Minor1 |  | Minor2 |  |  |  | Major1 |  |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1447 | 1304 | 25 |  | 1306 | 1301 | 923 |  | 927 | 0 | 0 | 26 | 0 | 0 |
| Stage 1 | 351 | 351 | - |  | 949 | 949 | - |  | - | - | - | - | - | - |
| Stage 2 | 1096 | 953 | - |  | 357 | 352 | - |  | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 109 | 160 | 1051 |  | 137 | 161 | 327 |  | 737 | - | - | 1588 | - | - |
| Stage 1 | 666 | 632 | - |  | 313 | 339 | - |  | - | - | - | - | - | - |
| Stage 2 | 259 | 338 | - |  | 661 | 632 | - |  | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | 10 | 122 | 1051 |  | 107 | 123 | 327 |  | 737 | - | - | 1588 | - | - |
| Mov Cap-2 Maneuver | 10 | 122 | - |  | 107 | 123 | - |  | - | - | - | - | - | - |
| Stage 1 | 517 | 490 | - |  | 243 | 333 | - |  | - | - | - | - | - | - |
| Stage 2 | 28 | 332 | - |  | 504 | 490 | - |  | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | NB |  |  |  | SB |  |  |  | SE |  |  | NW |  |  |
| HCM Control Delay, s | 108.8 |  |  |  | 75 |  |  |  | 9.7 |  |  | 0.1 |  |  |
| HCM LOS | F |  |  |  | F |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | NWL | NWT | NWR | SEL | SET | SER | BLn1 |  |  |  |  |  |  |
| Capacity (veh/h) | 47 | 1588 | - | - | 737 | - | - | 314 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.278 | 0.008 | - |  | 0.221 | - | - | 0.945 |  |  |  |  |  |  |
| HCM Control Delay (s) | 108.8 | 7.3 | 0 | - | 11.3 | 0 | - | 75 |  |  |  |  |  |  |
| HCM Lane LOS | F | A | A | - | B | A | - | F |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0.9 | 0 | - | - | 0.8 | - | - | 9.5 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | ¢ |  |  | \& |  |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 0 | 15 | 3 | 7 | 0 | 77 | 664 | 18 | 2 | 10 | 105 | 1 |
| Future Vol, veh/h | 0 | 15 | 3 | 7 | 0 | 77 | 664 | 18 | 2 | 10 | 105 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 16 | 3 | 8 | 0 | 84 | 722 | 20 | 2 | 11 | 114 | 1 |


| Major/Minor | Minor1 |  | Minor2 |  |  |  | Major1 |  |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1642 | 1601 | 21 |  | 1610 | 1601 | 115 |  | 115 | 0 | 0 | 22 | 0 | 0 |
| Stage 1 | 1464 | 1464 | - |  | 136 | 136 | - |  | - | - | - | - | - | - |
| Stage 2 | 178 | 137 | - |  | 1474 | 1465 | - |  | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 80 | 106 | 1056 |  | 84 | 106 | 937 |  | 1474 | - | - | 1593 | - | - |
| Stage 1 | 160 | 193 | - |  | 867 | 784 | - |  | - | - | - | - | - | - |
| Stage 2 | 824 | 783 | - |  | 158 | 193 | - |  | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | 44 | 53 | 1056 |  | 40 | 53 | 937 |  | 1474 | - | - | 1593 | - | - |
| Mov Cap-2 Maneuver | 44 | 53 | - |  | 40 | 53 | - |  | - | - | - | - | - | - |
| Stage 1 | 81 | 97 | - |  | 437 | 779 | - |  | - | - | - | - | - | - |
| Stage 2 | 745 | 778 | - |  | 66 | 97 | - |  | - | - | - | - | - | - |
| Approach | NB |  |  |  | SB |  |  |  | SE |  |  | NW |  |  |
| HCM Control Delay, s | 86 |  |  |  | 20.2 |  |  |  | 9.5 |  |  | 0.6 |  |  |
| HCM LOS | F |  |  |  | C |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | NWL | NWT | NWR | SEL | SET | SER | SBLn1 |  |  |  |  |  |  |
| Capacity (veh/h) | 63 | 1593 | - | - | 1474 | - | - | 327 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.311 | 0.007 | - | - | 0.49 | - | - | 0.279 |  |  |  |  |  |  |
| HCM Control Delay (s) | 86 | 7.3 | 0 | - | 9.8 | 0 | - | 20.2 |  |  |  |  |  |  |
| HCM Lane LOS | F | A | A | - | A | A | - | C |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 1.1 | 0 | - | - | 2.8 | - | - | 1.1 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | ¢ |  |  | \& |  |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 0 | 15 | 3 | 8 | 0 | 82 | 711 | 19 | 2 | 10 | 113 | 1 |
| Future Vol, veh/h | 0 | 15 | 3 | 8 | 0 | 82 | 711 | 19 | 2 | 10 | 113 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 16 | 3 | 9 | 0 | 89 | 773 | 21 | 2 | 11 | 123 | 1 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | ¢ |  |  | \& |  |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 0 | 15 | 3 | 8 | 0 | 86 | 748 | 20 | 2 | 10 | 118 | 1 |
| Future Vol, veh/h | 0 | 15 | 3 | 8 | 0 | 86 | 748 | 20 | 2 | 10 | 118 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 16 | 3 | 9 | 0 | 93 | 813 | 22 | 2 | 11 | 128 | 1 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | $\ddagger$ |  |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 0 | 15 | 3 | 9 | 0 | 91 | 786 | 21 | 2 | 10 | 124 | 1 |
| Future Vol, veh/h | 0 | 15 | 3 | 9 | 0 | 91 | 786 | 21 | 2 | 10 | 124 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 16 | 3 | 10 | 0 | 99 | 854 | 23 | 2 | 11 | 135 | 1 |


| Major/Minor | Minor1 |  | Minor2 |  |  |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1940 | 1891 | 24 |  | 1899 | 1891 | 135 |  | 136 | 0 | 0 | 25 | 0 | 0 |
| Stage 1 | 1733 | 1733 | - |  | 157 | 157 | - |  | - | - | - | - | - | - |
| Stage 2 | 207 | 158 | - |  | 1742 | 1734 | - |  | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 49 | 70 | 1052 |  | 53 | 70 | 914 |  | 1448 | - | - | 1589 | - | - |
| Stage 1 | 112 | 142 | - |  | 845 | 768 | - |  | - | - | - | - | - | - |
| Stage 2 | 795 | 767 | - |  | 110 | 142 | - |  | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | 23 | 28 | 1052 |  | 16 | 28 | 914 |  | 1448 | - | - | 1589 | - | - |
| Mov Cap-2 Maneuver | 23 | 28 | - |  | 16 | 28 | - |  | - | - | - | - | - | - |
| Stage 1 | 45 | 57 | - |  | 340 | 763 | - |  | - | - | - | - | - | - |
| Stage 2 | 704 | 762 | - |  | 31 | 57 | - |  | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | NB |  |  |  | SB |  |  |  | SE |  |  | NW |  |  |
| HCM Control Delay, s | 216.1 |  |  |  | 74 |  |  |  | 10.7 |  |  | 0.5 |  |  |
| HCM LOS | F |  |  |  | F |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | NWL | NWT | NWR | SEL | SET | SER | BLn1 |  |  |  |  |  |  |
| Capacity (veh/h) | 33 | 1589 | - | - | 1448 | - | - | 151 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.593 | 0.007 | - | - | 0.59 | - | - | 0.72 |  |  |  |  |  |  |
| HCM Control Delay (s) | 216.1 | 7.3 | 0 | - | 11 | 0 | - | 74 |  |  |  |  |  |  |
| HCM Lane LOS | F | A | A | - | B | A | - | F |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 2 | 0 | - | - | 4.1 | - | - | 4.3 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | \& |  |  | $\uparrow$ |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 1 | 2 | 5 | 0 | 0 | 68 | 172 | 13 | 2 | 1 | 148 | 3 |
| Future Vol, veh/h | 1 | 2 | 5 | 0 | 0 | 68 | 172 | 13 | 2 | 1 | 148 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 2 | 5 | 0 | 0 | 74 | 187 | 14 | 2 | 1 | 161 | 3 |


| Major/Minor | Minor1 |  | Minor2 |  |  |  | Major1 |  |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 591 | 555 | 15 |  | 558 | 555 | 162 |  | 164 | 0 | 0 | 16 | 0 | 0 |
| Stage 1 | 389 | 389 | - |  | 165 | 165 | - |  | - | - | - | - | - | - |
| Stage 2 | 202 | 166 | - |  | 393 | 390 | - |  | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 419 | 440 | 1065 |  | 440 | 440 | 883 |  | 1414 | - | - | 1602 | - | - |
| Stage 1 | 635 | 608 | - |  | 837 | 762 | - |  | - | - | - | - | - | - |
| Stage 2 | 800 | 761 | - |  | 632 | 608 | - |  | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 345 | 381 | 1065 |  | 391 | 381 | 883 |  | 1414 | - | - | 1602 | - |  |
| Mov Cap-2 Maneuver | 345 | 381 | - |  | 391 | 381 | - |  | - | - | - | - | - |  |
| Stage 1 | 551 | 527 | - |  | 726 | 761 | - |  | - | - | - | - | - |  |
| Stage 2 | 732 | 760 | - |  | 543 | 527 | - |  | - | - | - | - | - |  |
| Approach | NB |  |  |  | SB |  |  |  | SE |  |  | NW |  |  |
| HCM Control Delay, s | 10.9 |  |  |  | 9.4 |  |  |  | 7.3 |  |  | 0 |  |  |
| HCM LOS | B |  |  |  | A |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | NWL | NWT | NWR | SEL | SET | SER | BLn1 |  |  |  |  |  |  |
| Capacity (veh/h) | 623 | 1602 | - | - | 1414 | - | - | 883 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.014 | 0.001 | - | - | 0.132 | - | - | 0.084 |  |  |  |  |  |  |
| HCM Control Delay (s) | 10.9 | 7.2 | 0 | - | 7.9 | 0 | - | 9.4 |  |  |  |  |  |  |
| HCM Lane LOS | B | A | A | - | A | A | - | A |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | 0 | - | - | 0.5 | - | - | 0.3 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | $\uparrow$ |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 1 | 2 | 5 | 0 | 0 | 73 | 184 | 14 | 2 | 1 | 159 | 3 |
| Future Vol, veh/h | 1 | 2 | 5 | 0 | 0 | 73 | 184 | 14 | 2 | 1 | 159 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 2 | 5 | 0 | 0 | 79 | 200 | 15 | 2 | 1 | 173 | 3 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | $\uparrow$ |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 1 | 2 | 5 | 0 | 0 | 77 | 194 | 15 | 2 | 1 | 167 | 3 |
| Future Vol, veh/h | 1 | 2 | 5 | 0 | 0 | 77 | 194 | 15 | 2 | 1 | 167 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 2 | 5 | 0 | 0 | 84 | 211 | 16 | 2 | 1 | 182 | 3 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | \& |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 1 | 2 | 5 | 0 | 0 | 81 | 204 | 15 | 2 | 1 | 175 | 4 |
| Future Vol, veh/h | 1 | 2 | 5 | 0 | 0 | 81 | 204 | 15 | 2 | 1 | 175 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 2 | 5 | 0 | 0 | 88 | 222 | 16 | 2 | 1 | 190 | 4 |



```
Phone:
    Fax:
```

E-mail:
Diverge Analysis
$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2501 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Right

Volume on ramp
1

Length of first accel/decel lane
$60.0 \quad \mathrm{~km} / \mathrm{h}$

Length of second accel/decel lane
$732 \quad \mathrm{vph}$

130 m

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |




Level of Service Determination (if not $F$ ) $\qquad$



```
Phone:
    Fax:
```

E-mail:
Diverge Analysis
$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $2 / 14 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing TIS |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2681 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | 785 |
| Volume on ramp | 130 | $\mathrm{~km} / \mathrm{h}$ |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.909
1.00 3277
Estimation of V12 Diverge Areas

Capacity Checks $\qquad$

|  |  | Actual |
| :---: | :---: | :---: |
| $\mathrm{V}=\mathrm{v}$ |  | 3277 |
| Fi | F |  |
| v |  | 3277 |
| 12 |  |  |
| $\begin{array}{lll} \mathrm{V}= & \mathrm{V}-\mathrm{V} & 2396 \\ \mathrm{FO} & \mathrm{~F} & \mathrm{R} \end{array}$ |  |  |
|  |  |  |
| v |  | 881 |
| R |  |  |


| Maximum | LOS F? |
| :--- | :--- |
| 4600 | No |
| 4400 | No |
| 4600 | No |
| 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



```
Phone:
Fax:
```

E-mail:
Diverge Analysis
$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing TIS |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2820 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | 824 |
| Volume on ramp | 130 | $\mathrm{~km} / \mathrm{h}$ |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


$\qquad$

Capacity Checks $\qquad$


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 3447 | 4600 | No |
| 3447 | 4400 | No |
| 2522 | 4600 | No |
| 925 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



```
Phone:
    Fax:
```

E-mail:
Diverge Analysis
$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing TIS |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2965 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | 865 |
| Volume on ramp | 130 | $\mathrm{~km} / \mathrm{h}$ |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



Heavy vehicle adjustment, fHV
0.909
1.00 3624 .00 971
Estimation of V12 Diverge Areas

Capacity Checks $\qquad$

| V = | v |
| :---: | :---: |
| Fi | F |
| v |  |
| 12 |  |
| $\mathrm{v}=$ | v - V |
| FO | F R |
| v |  |
| R |  |


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 3624 | 4600 | No |
| 3624 | 4400 | No |
| 2653 | 4600 | No |
| 971 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



```
Phone:
Fax:
E-mail:
Merge Analysis
\begin{tabular}{ll} 
Analyst: & Katie Hazzard \\
Agency/Co.: & exp \\
Date performed: & \(2 / 14 / 2017\) \\
Analysis time period: & AM Peak \\
Freeway/Dir of Travel: & Westbond \\
Junction: & Foster Thurston On Ramp \\
Jurisdiction: & Provincial \\
Analysis Year: & 2016 \\
Description: The Crossing TIS
\end{tabular}
```

$\qquad$

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2501 | vph |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 26 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
1.00

Flow rate, vp
$\qquad$
$\mathrm{L}=\quad$ (Equation 25-2 or 25-3)
${ }^{\mathrm{EQ}}=1.000 \quad$ Using Equation 0

FM
$\mathrm{v}=\mathrm{v}(\mathrm{P})=3057$ pcph
$12 \mathrm{~F} \quad \mathrm{FM}$
Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 3086 | 4600 | No |
| V |  |  |  |
| R12 | 3086 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\underset{R}{D}=3.402+0.00456 \underset{R}{v}+0.0048 \mathrm{v}_{12}-0.01278 \mathrm{~L} \quad=16.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $C$
Speed Estimation

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.378$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\mathrm{S}_{\mathrm{R}}=87.5$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=87.5$ | km/h |

```
Phone:
    Fax:
E-mail:
Merge Analysis
\begin{tabular}{ll} 
Analyst: & Katie Hazzard \\
Agency/Co.: & exp \\
Date performed: & \(2 / 14 / 2017\) \\
Analysis time period: & AM Peak \\
Freeway/Dir of Travel: & Westbond \\
Junction: & Foster Thurston On Ramp \\
Jurisdiction: & Provincial \\
Analysis Year: & 2023 \\
Description: The Crossing TIS
\end{tabular}
```

$\qquad$

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2681 | vph |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 27 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
1.00
1.00

Flow rate, vp
3277
30
pcph
Estimation of V12 Merge Areas $\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 3307 | 4600 | No |
| FO |  |  |  |
| V | 3307 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$

Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.399$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=86.8$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=86.8$ | km/h |

```
Phone:
Fax:
E-mail:
Merge Analysis
\begin{tabular}{ll} 
Analyst: & Katie Hazzard \\
Agency/Co.: & exp \\
Date performed: & \(2 / 14 / 2017\) \\
Analysis time period: & AM Peak \\
Freeway/Dir of Travel: & Westbond \\
Junction: & Foster Thurston On Ramp \\
Jurisdiction: & Provincial \\
Analysis Year: & 2028 \\
Description: The Crossing TIS
\end{tabular}
```

$\qquad$

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2820 | vph |


| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | Data__ |  |
| Free-flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 29 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
Flow rate, vp
$\qquad$ Estimation of V12 Merge Areas $\qquad$

| $\begin{gathered} \mathrm{L}= \\ \mathrm{EQ} \end{gathered}$ | on 25-2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}=$ | 1.000 | Usi | Equation | 0 |
| FM |  |  |  |  |
| $\mathrm{V}=$ | ( P ) | 3447 | pcph |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| v | 3480 | 4600 | No |
| FO |  |  |  |
| v | 3480 | 4600 | No |
| R12 |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$

Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


```
Phone:
Fax:
E-mail:
Merge Analysis
```

Analyst:
Agency/Co.:
Date performed:
Analysis time period:
Freeway/Dir of Travel:
Junction:
Jurisdiction:
Analysis Year:
Description: The Crossing
Katie Hazzard
exp
1/23/2017
AM Peak
Westbond
Foster Thurston On Ramp
Provincial
2033
$\qquad$
$\qquad$ Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway
$100.0 \mathrm{~km} / \mathrm{h}$
$2965 \quad v p h$
On Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 30 | m |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  |  |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.909
1.00

3624
34
pcph

Estimation of V12 Merge Areas $\qquad$
$\mathrm{L}=\quad$ (Equation 25-2 or 25-3)
EQ
P = 1.000 Using Equation 0
FM
$\mathrm{v}=\mathrm{v}(\mathrm{P})=3624 \quad \mathrm{pcph}$
$12 \mathrm{~F} \quad \mathrm{FM}$
Capacity Checks $\qquad$

|  | Actual | Capacity Checks___ | Maximum |
| :---: | :--- | :--- | :--- |
| V FO | 3658 | 4600 | LOS F? |
| V 20 | 3658 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\underset{R}{\mathrm{D}}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v} \underset{\mathrm{R}}{\mathrm{v}} \underset{\mathrm{R}}{\mathrm{v}}-0.01278 \mathrm{~L} \quad=19.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.443$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=85.4$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=85.4$ | km/h |

## Phone:

Fax:
E-mail:
Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $2 / 14 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing TIS |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 1014 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 116 | vph |
| Length of first accel/decel lane | 130 | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


$\qquad$

Capacity Checks $\qquad$


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 1239 | 4600 | No |
| 1239 | 4400 | No |
| 1109 | 4600 | No |
| 130 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



```
Phone: Fax:
```

E-mail:

Diverge Analysis $\qquad$

| Analyst: | Don Good |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $2 / 14 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing TIS |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 1087 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-Flow speed on ramp | 60.0 | vph |
| Volume on ramp | 124 | m |
| Length of first accel/decel lane | 130 | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.909
$-1.00$ 1329 139
$\qquad$

Capacity Checks $\qquad$

| $\mathrm{V}=$ | v |
| :---: | :---: |
| Fi | F |
| v |  |
| 12 |  |
| $\mathrm{v}=$ | v - v |
| FO | F $\quad$ R |
| v |  |
| R |  |


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 1329 | 4600 | No |
| 1329 | 4400 | No |
| 1190 | 4600 | No |
| 139 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



## Phone:

Fax:
E-mail:
Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing TIS |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 1144 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 129 | vph |
| Length of first accel/decel lane | 130 | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


$\qquad$

Capacity Checks $\qquad$


| Maximum | LOS F? |
| :--- | :--- |
| 4600 | No |
| 4400 | No |
| 4600 | No |
| 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



## Phone:

Fax:
E-mail:
Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 1202 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 135 | vph |
| Length of first accel/decel lane | 130 | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


 $12 R \quad \mathrm{~F} \quad \mathrm{R} \quad \mathrm{FD}$

Capacity Checks $\qquad$

|  |  |  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{v}=$ | v |  | 1469 | 4600 | No |
| Fi | F |  |  |  |  |
| V |  |  | 1469 | 4400 | No |
| 12 |  |  |  |  |  |
| $\mathrm{v}=$ | V - | v | 1317 | 4600 | No |
| FO | F | R |  |  |  |
| v |  |  | 152 | 2000 | No |
| R |  |  |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$



```
Phone:
Fax:
E-mail:
Merge Analysis
\begin{tabular}{ll} 
Analyst: & Katie Hazzard \\
Agency/Co.: & exp \\
Date performed: & \(2 / 14 / 2017\) \\
Analysis time period: & PM Peak \\
Freeway/Dir of Travel: & Westbond \\
Junction: & Foster Thurston On Ramp \\
Jurisdiction: & Provincial \\
Analysis Year: & 2016 \\
Description: The Crossing TIS
\end{tabular}
```

$\qquad$

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 1014 | vph |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 28 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.990

Driver population factor, fP
$\qquad$

$\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 1270 | 4600 | No |
| V | 1270 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=8.0 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation


```
Phone:
    Fax:
E-mail:
Merge Analysis
\begin{tabular}{ll} 
Analyst: & Katie Hazzard \\
Agency/Co.: & exp \\
Date performed: & \(2 / 14 / 2017\) \\
Analysis time period: & PM Peak \\
Freeway/Dir of Travel: & Westbond \\
Junction: & Foster Thurston On Ramp \\
Jurisdiction: & Provincial \\
Analysis Year: & 2023 \\
Description: The Crossing TIS
\end{tabular}
```

$\qquad$

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 1087 | vph |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 30 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Capacity Checks_____ Maximum | LOS F? |
| :---: | :--- | :--- | :--- |
| V FO | 1363 | 4600 | No |
| V 12 | 1363 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\underset{R}{D}=3.402+0.00456 \underset{R}{v}+0.0048 \mathrm{v}_{\mathrm{R}}-0.01278 \mathrm{~L} \quad=8.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence B
Speed Estimation


```
Phone:
    Fax:
```

E-mail:
Merge Analysis
$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Westbond |
| Junction: | Foster Thurston On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |

Description: The Crossing
Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 1144 | vph |


|  |  |  |
| :--- | :---: | :---: |
| Side of freeway | Right |  |
| Number of lanes in ramp | Data__ |  |
| Free-flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 31 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
Flow rate, vp
$\qquad$

| $\mathrm{L}_{\mathrm{EQ}}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- |
| $\mathrm{P}^{\mathrm{FM}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{~V}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=1398 \mathrm{pcph}$ |  |  | Capacity Checks $\qquad$


|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 1433 | 4600 | No |
| V |  |  |  |
| R12 | 1433 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=8.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.309$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=89.8$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=89.8$ | km/h |

```
Phone:
Fax:
E-mail:
Merge Analysis
```

Analyst:
Agency/Co.:
Date performed:
Analysis time period:
Freeway/Dir of Travel:
Junction:
Jurisdiction:
Analysis Year:
Description: The Crossing
Katie Hazzard
exp
1/23/2017
PM Peak
Westbond
Foster Thurston On Ramp
Provincial
2033
$\qquad$
$\qquad$ Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

2
$100.0 \mathrm{~km} / \mathrm{h}$
1202 vph
$\qquad$ On Ramp Data

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 32 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |
|  |  |  |


| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
1.00
1.00

Flow rate, vp

Estimation of V12 Merge Areas $\qquad$

| $\begin{gathered} \mathrm{L}= \\ \mathrm{EQ} \end{gathered}$ | on 25-2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}=$ | 1.000 | Us | Equation | 0 |
| FM |  |  |  |  |
| $\mathrm{V}=$ | ( P ) | 1469 | pcph |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 1505 | 4600 | No |
| V |  |  |  |
| R12 | 1505 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L} \quad=\quad 9.1 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation


## Phone:

Fax:
E-mail:
Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 644 |
| Volume on freeway | $\mathrm{km} / \mathrm{h}$ |  |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-Flow speed on ramp | 60.0 | vph |
| Volume on ramp | 152 | m |
| Length of first accel/decel lane | 130 | m |
| Length of second accel/decel lane |  |  |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


0.909
0.990
$\qquad$

Capacity Checks $\qquad$


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 787 | 4600 | No |
| 787 | 4400 | No |
| 616 | 4600 | No |
| 171 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



## Phone:

Fax:
E-mail:
Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 690 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | 163 |
| Volume on ramp | 130 | $\mathrm{~km} / \mathrm{h}$ |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



$$
0.990
$$

$\qquad$

Capacity Checks $\qquad$

| V = |  |  |
| :---: | :---: | :---: |
| Fi | F |  |
| v |  |  |
| 12 |  |  |
| v = | v - | v |
| FO | F | R |
| v |  |  |
| R |  |  |


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 843 | 4600 | No |
| 843 | 4400 | No |
| 660 | 4600 | No |
| 183 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



## Phone:

Fax:
E-mail:
Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing TIS |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 725 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 180 | vph |
| Length of first accel/decel lane | 130 | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



Heavy vehicle adjustment, fHV
0.909
1.00 886
0.990
$\qquad$


Capacity Checks $\qquad$


| Maximum | LOS F? |
| :--- | :--- |
| 4600 | No |
| 4400 | No |
| 4600 | No |
| 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$


| Intermediate speed variable, | $D_{S}=0.421$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=86.1$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=86.1$ | km/h |

```
Phone:
    Fax:
```

E-mail:
Diverge Analysis
$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 763 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 180 | vph |
| Length of first accel/decel lane | 130 | m |
| Length of second accel/decel lane |  | m |
| _Adjacent | (if one exists) |  |
| Does adjacent ramp exist? | No |  |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  |  |
| Type of adjacent ramp |  |  |
| Distance to adjacent ramp |  | m |



Heavy vehicle adjustment, fHV
0.909
1.00 933
0.990
$\qquad$


Capacity Checks $\qquad$

|  |  |  | Actual933 |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=$ | v |  |  |
| Fi F |  |  |  |
| v |  |  | 933 |
| 12 |  |  |  |
| $\mathrm{v}=$ | V - | v | 731 |
| FO | F | R |  |
| V 202 |  |  |  |
|  |  |  |  |  |


| Maximum | LOS F? |
| :--- | :--- |
| 4600 | No |
| 4400 | No |
| 4600 | No |
| 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



```
Phone:
Fax:
E-mail:
Merge Analysis
\begin{tabular}{ll} 
Analyst: & Katie Hazzard \\
Agency/Co.: & exp \\
Date performed: & \(1 / 23 / 2017\) \\
Analysis time period: & Sat Peak \\
Freeway/Dir of Travel: & Westbond \\
Junction: & Foster Thurston On Ramp \\
Jurisdiction: & Provincial \\
Analysis Year: & 2016 \\
Description: The Crossing TIS
\end{tabular}
```

$\qquad$

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 644 |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 18 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
1.00

Estimation of V12 Merge Areas $\qquad$

| $\begin{gathered} \mathrm{L}= \\ \mathrm{EQ} \end{gathered}$ |  | n |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}=$ | 1.000 | Using | Equation | 0 |
| FM |  |  |  |  |
| $\mathrm{V}=$ | ( P ) | 7 | cph |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 807 | 4600 | No |
| FO |  |  | No |
| V12 | 807 | 4600 |  |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=5.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $A$

Speed Estimation


```
Phone:
Fax:
E-mail:
Merge Analysis
\begin{tabular}{ll} 
Analyst: & Katie Hazzard \\
Agency/Co.: & exp \\
Date performed: & \(1 / 23 / 2017\) \\
Analysis time period: & Sat Peak \\
Freeway/Dir of Travel: & Westbond \\
Junction: & Foster Thurston On Ramp \\
Jurisdiction: & Provincial \\
Analysis Year: & 2023 \\
Description: The Crossing TIS
\end{tabular}
```

$\qquad$

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 690 | vph |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 19 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
1.00 843 00

21

Estimation of V12 Merge Areas $\qquad$

| $\mathrm{L}_{\mathrm{EQ}}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- |
| $\mathrm{P}^{\mathrm{EM}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{~V}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=843$ | pcph |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 864 | 4600 | No |
| V | 864 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=6.0+\mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation


```
Phone:
    Fax:
```

E-mail:
Merge Analysis
$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat Peak |
| Freeway/Dir of Travel: | Westbond |
| Junction: | Foster Thurston On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |

Description: The Crossing
Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 725 |
| Volume on freeway | $\mathrm{km} / \mathrm{h}$ |  |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 20 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
Flow rate, vp
$\qquad$

| $\mathrm{L}_{\mathrm{EQ}}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- |
| $\mathrm{P}^{\mathrm{FM}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{~V}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=886 \quad \mathrm{pcph}$ |  |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 908 | 4600 | No |
| V | 908 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=6.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.302$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $S_{R}=90.0$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | $\mathrm{km} / \mathrm{h}$ |
| Space mean speed for all vehicles, | $S=90.0$ | km/h |

```
Phone:
Fax:
E-mail:
Merge Analysis
```

Analyst:
Agency/Co.:
Date performed:
Analysis time period:
Freeway/Dir of Travel:
Junction:
Jurisdiction:
Analysis Year:
Description: The Crossing
Katie Hazzard
exp
1/23/2017
Sat Peak
Westbond
Foster Thurston On Ramp
Provincial
2033
$\qquad$
$\qquad$ Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

2
$100.0 \mathrm{~km} / \mathrm{h}$
763 vph

On Ramp Data

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 20 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |
|  |  |  |


| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.990

Driver population factor, fP

Estimation of V12 Merge Areas $\qquad$

| $\mathrm{L}_{\mathrm{EQ}}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- | :--- |
| $\mathrm{P}^{\mathrm{FM}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{~V}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=933$ | pcph |  | Capacity Checks $\qquad$


|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 955 | 4600 | No |
| FO | 955 | 4600 | No |

Level of Service Determination (if not F) $\qquad$
Density, $\underset{R}{D}=3.402+0.00456 \underset{R}{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=6.4 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.302$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\mathrm{S}_{\mathrm{R}}=90.0$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | $\mathrm{km} / \mathrm{h}$ |
| Space mean speed for all vehicles, | $S=90.0$ | km/h |

Phone:
E-mail:

Fax:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $3 / 20 / 2016$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | Eastbound |
| Junction: | Ashburn Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing Study |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 618 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-Flow speed on ramp | 60.0 | vph |
| Volume on ramp | 240 | m |
| Length of first accel/decel lane | 180 | m |
| Length of second accel/decel lane |  |  |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


$\qquad$

Capacity Checks $\qquad$


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 755 | 4500 | No |
| 755 | 4400 | No |
| 486 | 4500 | No |
| 269 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



Phone:
E-mail:

Fax:

Diverge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
Date performed: 1/23/2017
Analysis time period:
AM Peak
Freeway/Dir of Travel: Eastbound
Junction: Ashburn Off Ramp
Jurisdiction: Provincial
Analysis Year:
2023
Description: The Crossing Study

Freeway Data

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 662 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-Flow speed on ramp | 60.0 | vph |
| Volume on ramp | 257 | m |
| Length of first accel/decel lane | 180 | m |
| Length of second accel/decel lane |  |  |

_Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



Heavy vehicle adjustment, fHV
0.909
1.00 809
0.990
$\qquad$


Capacity Checks $\qquad$


| Maximum | LOS F? |
| :--- | :--- |
| 4500 | No |
| 4400 | No |
| 4500 | No |
| 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$


$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $2 / 14 / 2017$ |
| Analysis time period: | AMPeak |
| Freeway/Dir of Travel: | Eastbound |
| Junction: | Ashburn Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing Study |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 696 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | 271 |
| Volume on ramp | 180 | vph |
| Length of first accel/decel lane | m |  |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


$\qquad$

Capacity Checks $\qquad$

|  |  | Actual |
| :---: | :---: | :---: |
| $\underset{\mathrm{Fi}}{\mathrm{~V}}=\mathrm{V}$ |  | 851 |
|  |  |  |
| v |  | 851 |
| 12 |  |  |
| $\begin{aligned} & \mathrm{v}=\mathrm{v}-\mathrm{V} \\ & \mathrm{FO} \quad \mathrm{~F} \quad \mathrm{R} \end{aligned}$ |  | 547 |
|  |  |  |
| v R |  | 304 |
|  |  |  |


| Maximum | LOS F? |
| :--- | :--- |
| 4500 | No |
| 4400 | No |
| 4500 | No |
| 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



Phone:
E-mail:

Fax:

Diverge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
Date performed: 1/23/2017
Analysis time period:
AM Peak
Freeway/Dir of Travel: Eastbound
Junction: Ashburn Off Ramp
Jurisdiction: Provincial
Analysis Year:
2033
Description: The Crossing Study

Freeway Data

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 732 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-Flow speed on ramp | 60.0 | vph |
| Volume on ramp | 281 | m |
| Length of first accel/decel lane | 180 | m |
| Length of second accel/decel lane |  |  |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


$\qquad$

Capacity Checks $\qquad$

| $\mathrm{V}=$ | v |
| :---: | :---: |
| Fi | F |
| v |  |
| 12 |  |
| $\mathrm{v}=$ | v - v |
| FO | F $\quad$ R |
| v |  |
| R |  |


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 895 | 4500 | No |
| 895 | 4400 | No |
| 580 | 4500 | No |
| 315 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: AM Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2016
Description: The Crossing
Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 618 |
| Volume on freeway | $\mathrm{km} / \mathrm{h}$ |  |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 47 | vph |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
1.00
1.00

Flow rate, vp
755
53
pcph
Estimation of V12 Merge Areas $\qquad$

| $\begin{gathered} \mathrm{L}= \\ \mathrm{EQ} \end{gathered}$ |  | (Equation 25-2 or 25-3) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}=$ | 1.000 | Using | Equation | 0 |
| FM |  |  |  |  |
| $\mathrm{V}=$ | ( P ) | 5 | pcph |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 808 | 4600 | No |
| FO |  |  |  |
| R12 | 808 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}_{\mathrm{R}}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L} \quad=5.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $A$
Speed Estimation


## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: AM Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2023
Description: The Crossing
Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

| 2 |  |
| :--- | :--- |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 662 | vph |

On Ramp Data

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 150 | vph |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
1.00
1.00

809
57
pcph

Estimation of V12 Merge Areas $\qquad$

| $\begin{gathered} \mathrm{L}= \\ \mathrm{EQ} \end{gathered}$ | (Equation 25-2 or 25-3) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| $\mathrm{P}=$ | 1.000 |  | Using Equation |  |  |
| FM |  |  |  |  |  |
| $\mathrm{V}=$ | $(\mathrm{P})=$ | 809 | 9 pcph |  |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 866 | 4600 | No |
| V |  |  |  |
| R12 | 866 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}_{\mathrm{R}}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L} \quad=\quad 5.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $A$
Speed Estimation

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.294$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $S_{R}=90.3$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=90.3$ | km/h |

## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: AM Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2028
Description: The Crossing
Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

| 2 |  |
| :--- | :--- |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 696 | vph |

On Ramp Data

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 150 | m |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  |  |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :--- | :--- | :--- |
| V | Checks_ | No |  |
| FO | 910 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\underset{R}{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L} \quad=\quad 5.8 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence A
Speed Estimation


## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: AM Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2033
Description: The Crossing
Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

2
$100.0 \mathrm{~km} / \mathrm{h}$
732
vph

On Ramp Data



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP Flow rate, vp
1.00
1.00

895
63
pcph

Estimation of V12 Merge Areas $\qquad$

| $\begin{gathered} \mathrm{L}= \\ \mathrm{EQ} \end{gathered}$ |  | (Equation 25-2 or 25-3) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}=$ | 1.000 | Using | Equation | 0 |
| FM |  |  |  |  |
| $\mathrm{V}=$ | ( P ) | 5 | pcph |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 958 | 4600 | No |
| V |  |  |  |
| R12 | 958 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\underset{R}{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L} \quad=\quad 6.1 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.295$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $S_{R}=90.3$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=90.3$ | km/h |

Phone:
E-mail:

Fax:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $2 / 14 / 207$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Eastbound |
| Junction: | Ashburn Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing Study |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2721 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 278 | vph |
| Length of first accel/decel lane | 180 | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



Heavy vehicle adjustment, fHV
0.909
1.00 3326 Flow rate, vp1.00
Estimation of V12 Diverge Areas

Capacity Checks $\qquad$

| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 3326 | 4500 | No |
| 3326 | 4400 | No |
| 3014 | 4500 | No |
| 312 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



Phone:
E-mail:

Fax:

Diverge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
Date performed: 1/23/2017
Analysis time period: PM Peak
Freeway/Dir of Travel: Eastbound
Junction: Ashburn Off Ramp
Jurisdiction: Provincial
Analysis Year: 2023
Description: The Crossing Study
Freeway Data

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2918 | vph |

Off Ramp Data $\qquad$
Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Right

Length of first accel/decel lane
$60.0 \quad \mathrm{~km} / \mathrm{h}$

298
180
vph
Length of second accel/decel lane

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |




Level of Service Determination (if not $F$ ) $\qquad$



Phone:
E-mail:

Fax:

Diverge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
Date performed: 1/23/2017
Analysis time period: PM Peak
Freeway/Dir of Travel: Eastbound
Junction: Ashburn Off Ramp
Jurisdiction: Provincial
Analysis Year: 2028
Description: The Crossing Study
Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3066 | vph |

Off Ramp Data $\qquad$
Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane
Right
1
$60.0 \quad \mathrm{~km} / \mathrm{h}$
$314 \quad \mathrm{vph}$
180 m

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



$$
0.990
$$

$\qquad$

Capacity Checks $\qquad$

|  |  | Actual |
| :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ |  | 3747 |
| Fi F |  |  |
| v |  | 3747 |
| 12 |  |  |
| $\mathrm{v}=$ | v - v | 3395 |
| FO | F R |  |
| V |  | 352 |
| R |  |  |


| Maximum | LOS F? |
| :--- | :--- |
| 4500 | No |
| 4400 | No |
| 4500 | No |
| 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$


$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Eastbound |
| Junction: | Ashburn Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing Study |  |

Freeway Data

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3224 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 180 | vph |
| Length of first accel/decel lane | m |  |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



Heavy vehicle adjustment, fHV
Diver population factor, fP Flow rate, vp
0.909
0.990
1.00 3940 370
$\qquad$


Capacity Checks $\qquad$

| $\mathrm{v}=$ | v |  |
| :---: | :---: | :---: |
| Fi | F |  |
| v |  |  |
| 12 |  |  |
| $\mathrm{v}=$ | V - | V |
| FO | F | R |
| V |  |  |
| R |  |  |


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 3940 | 4500 | No |
| 3940 | 4400 | No |
| 3570 | 4500 | No |
| 370 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed:
2/14/2017
Analysis time period:
PM Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2016
Description: The Crossing
Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

| 2 |  |
| :--- | :--- |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 2721 | vph |

On Ramp Data

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 326 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.909
. 00
3326

Estimation of V12 Merge Areas $\qquad$
$\mathrm{L}=$ (Equation 25-2 or 25-3)


P = 1.000 Using Equation 0
FM
$\mathrm{v}=\mathrm{v}(\mathrm{P})=332$
12 F FM
Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 3692 | 4600 | No |
| V |  |  |  |
| R12 | 3692 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\underset{R}{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L} \quad=19.1 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $D$

Speed Estimation


## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: PM Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2023
Description: The Crossing
Freeway Data $\qquad$
Type of analysis

| Merge |  |
| :--- | :--- |
| 2 |  |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 2918 | vph |

On Ramp Data
vph

| Number of lanes in freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| :--- | :--- | :--- |
| Free-flow speed on freeway | 100.0 | 2918 |

$\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 159 | m |
| Length of first accel/decel lane | 150 | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Driver population factor, fP
Flow rate, vp
$1.00 \quad 1.00$
$\qquad$

| $\mathrm{L}_{\mathrm{EQ}}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- |
| $\mathrm{P}^{\mathrm{EM}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{~V}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=3566$ pcph |  |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 3958 | 4600 | No |
| V |  |  |  |
| R12 | 3958 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\underset{R}{\mathrm{D}}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v} \underset{\mathrm{R}}{\mathrm{v}}-0.01278 \mathrm{~L} \quad=\quad 20.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $D$

Speed Estimation


## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: PM Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2028
Description: The Crossing
Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3066 | vph |


|  | On Ramp |  |
| :--- | :---: | :---: |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 367 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.990

Driver population factor, fP
$\qquad$

| $\mathrm{L}_{\mathrm{EQ}}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- |
| $\mathrm{P}^{\mathrm{FM}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{~V}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=3747 \mathrm{pcph}$ |  |  | Capacity Checks $\qquad$


|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 4159 | 4600 | No |
| v | 4159 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=21.3 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $D$

Speed Estimation


## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: PM Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2033
Description: The Crossing
Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

| 2 |  |
| :--- | :--- |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 3224 | vph |

On Ramp Data
vph

|  | On Ramp |  |
| :--- | :---: | :---: |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 385 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.990

Diver population factor, fP
Flow rate, vp
1.00

Estimation of V12 Merge Areas $\qquad$

| $\mathrm{L}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- |
| $\mathrm{PQ}^{\mathrm{EQ}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{VM}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=3940$ | pcph |  | Capacity Checks $\qquad$


|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 4372 | 4600 | No |
| V | 4372 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\underset{R}{\mathrm{D}}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v} \underset{\mathrm{R}}{\mathrm{v}}-0.01278 \mathrm{~L} \quad=\quad 22.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $E$

Speed Estimation


Phone:
E-mail:

Fax:

Diverge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
1/23/2017
Date performed:
$\begin{array}{ll}\text { Analysis time period: } & \text { Sat Peak } \\ \text { Freeway/Dir of Travel: } & \text { Eastbound }\end{array}$
Junction: Ashburn Off Ramp
Jurisdiction: Provincial
Analysis Year: 2016
Description: The Crossing Study
Freeway Data

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 767 | vph |

Off Ramp Data $\qquad$
Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Right

Length of first accel/decel lane
1
$60.0 \mathrm{~km} / \mathrm{h}$
$385 \quad \mathrm{vph}$
Length of second accel/decel lane
m
m

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |

$\left.\begin{array}{lllll} & \text { Freeway } & \text { Ramp } & \begin{array}{l}\text { Adjacent } \\ \text { Junction Components }\end{array} & \\ \text { Ramp }\end{array}\right]$
$\qquad$

Capacity Checks $\qquad$


| Maximum | LOS F? |
| :--- | :--- |
| 4500 | No |
| 4400 | No |
| 4500 | No |
| 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$



Phone:
E-mail:

Fax:

Diverge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
1/23/2017
Date performed:
$\begin{array}{ll}\text { Analysis time period: } & \text { Sat Peak } \\ \text { Freeway/Dir of Travel: } & \text { Eastbound }\end{array}$
Junction: Ashburn Off Ramp
Jurisdiction: Provincial
Analysis Year: 2023
Description: The Crossing Study
Freeway Data

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 823 | vph |

Off Ramp Data $\qquad$
Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane
Right
1
$60.0 \quad \mathrm{~km} / \mathrm{h}$
$413 \quad$ vph
180 m
m
$m$

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |



Heavy vehicle adjustment, fHV
0.909
1.00

$$
1.00
$$ 1006 463

Estimation of V12 Diverge Areas

Capacity Checks $\qquad$


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 1006 | 4500 | No |
| 1006 | 4400 | No |
| 543 | 4500 | No |
| 463 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$


$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat Peak |
| Freeway/Dir of Travel: | Eastbound |
| Junction: | Ashburn Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing Study |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 856 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-Flow speed on ramp | 60.0 | 456 |
| Volume on ramp | 180 | $\mathrm{~km} / \mathrm{h}$ |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


 $12 R \quad F \quad R \quad F D$

Capacity Checks $\qquad$


Level of Service Determination (if not $F$ ) $\qquad$


| Intermediate speed variable, | $\mathrm{D}_{\mathrm{S}}=0.449$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=79.7$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=79.7$ | km/h |

$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat Peak |
| Freeway/Dir of Travel: | Eastbound |
| Junction: | Ashburn Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing Study |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 899 | vph |

Off Ramp Data $\qquad$

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-Flow speed on ramp | 60.0 | vph |
| Volume on ramp | 189 | m |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  |  |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent ramp |  |
| Position of adjacent ramp |  |
| Type of adjacent ramp |  |
| Distance to adjacent ramp | m |


$\qquad$

Capacity Checks $\qquad$


| Actual | Maximum | LOS F? |
| :--- | :--- | :--- |
| 1099 | 4500 | No |
| 1099 | 4400 | No |
| 561 | 4500 | No |
| 538 | 2000 | No |

Level of Service Determination (if not $F$ ) $\qquad$


| Intermediate speed variable, | $\mathrm{D}_{\mathrm{S}}=0.451$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\mathrm{S}_{\mathrm{R}}=79.6$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=79.6$ | km/h |

## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: Sat Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2016
Description: The Crossing
Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

| 2 |  |
| :--- | :--- |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 767 | vph |

On Ramp Data

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 158 | m |
| Length of first accel/decel lane | 150 | m |

Adjacent Ramp Data (if one exists)

| Does adjacent ramp exist? | No |
| :--- | :--- |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
Driver population factor, fP
0.909
0.990

Flow rate, vp

Estimation of V12 Merge Areas $\qquad$

| $\mathrm{L}_{\mathrm{EQ}}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- | :--- |
| $\mathrm{P}^{\mathrm{FM}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{~V}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=937$ | pcph |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 1114 | 4600 | No |
| V |  |  |  |
| R12 | 1114 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=6.8 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation


## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: Sat Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2023
Description: The Crossing
Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

| 2 |  |
| :--- | :--- |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 823 | vph |

On Ramp Data

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 169 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
Driver population factor, fP
Flow rate, vp
0.909
0.990 1.00 1006 190
$\qquad$
$\mathrm{L}=$ (Equation 25-2 or 25-3)
EQ
P = 1.000 Using Equation 0
FM
$\mathrm{V}=\mathrm{v}(\mathrm{P})=1006 \mathrm{pcph}$
$12 \mathrm{~F} \quad \mathrm{FM}$
Capacity Checks
$\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 1196 | 4600 | No |
| FO | 1196 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=7.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation


## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: Sat Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2028
Description: The Crossing
Freeway Data $\qquad$
Type of analysis
Merge
Number of lanes in freeway
Free-flow speed on freeway
Volume on freeway

| 2 |  |
| :--- | :--- |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 856 | vph |

On Ramp Data

| Side of freeway | Right |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | 187 |
| Volume on ramp | 150 | $\mathrm{~km} / \mathrm{h}$ |
| Length of first accel/decel lane |  | m |
| Length of second accel/decel lane |  | m |

Adjacent Ramp Data (if one exists) $\qquad$

| Does adjacent ramp exist? | No |
| :--- | :---: |
| Volume on adjacent Ramp |  |
| Position of adjacent Ramp |  |
| Type of adjacent Ramp |  |
| Distance to adjacent Ramp | m |



Heavy vehicle adjustment, fHV
0.909
0.909

Estimation of V12 Merge Areas $\qquad$

| $\mathrm{L}_{\mathrm{EQ}}=$ |  | (Equation 25-2 or 25-3) |
| :--- | :--- | :--- |
| $\mathrm{P}^{\mathrm{EM}}=$ | 1.000 | Using Equation 0 |
| $\mathrm{~V}^{\mathrm{FM}}=\mathrm{V}(\mathrm{P})=1046$ pcph |  |  |

Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 1256 | 4600 | No |
| V |  |  |  |
| R12 | 1256 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=7.5 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation


## Phone:

Fax:
E-mail:

Merge Analysis $\qquad$
Analyst:
Katie Hazzard
Agency/Co.:
exp
Date performed: 1/23/2017
Analysis time period: Sat Peak
Freeway/Dir of Travel: Eastbond
Junction: Ashburn On Ramp
Jurisdiction: Provincial
Analysis Year: 2033
Description: The Crossing
Freeway Data $\qquad$
Type of analysis

| Merge |  |
| :--- | :--- |
| 2 |  |
| 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| 899 | vph |

On Ramp Data



Heavy vehicle adjustment, fHV
0.909
0.909
1.00 1099 221

Estimation of V12 Merge Areas $\qquad$
$\mathrm{L}=$ (Equation 25-2 or 25-3)


P = 1.000 Using Equation 0
FM
$\mathrm{v}=\mathrm{v}(\mathrm{P})=1099 \quad \mathrm{pcph}$
12 F FM
Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 1320 | 4600 | No |
| V |  |  |  |
| R12 | 1320 | 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=7.8 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
Level of service for ramp-freeway junction areas of influence $B$

Speed Estimation



|  |  | pren |  |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBT | NBR | SBL | SBT | NWL | NWR |
| Turn Bay Length ( m ) |  |  |  |  |  |  |
| Base Capacity (vph) | 2494 |  |  | 2256 | 270 | 353 |
| Starvation Cap Reductn | 1576 |  |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 |  |  | 218 | 0 | 0 |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.54 |  |  | 0.42 | 0.41 | 0.17 |
| Intersection Summary |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:NBSB, Start of 1st Green |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.41 |  |  |  |  |  |  |
| Intersection Signal Delay: 8.3 |  |  |  | Intersection LOS: A |  |  |
| Intersection Capacity Utilization 52.9\% |  |  |  |  | Leve | Service A |
| Analysis Period (min) 15 |  |  |  |  |  |  |

Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
dl Defacto Left Lane. Recode with 1 though lane as a left lane.
Splits and Phases: 9:




|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 9:


|  |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.
dl Defacto Left Lane. Recode with 1 though lane as a left lane.
Splits and Phases: 9:




Splits and Phases: 3:



Analysis Period (min) 15
Splits and Phases: 3 :



Analysis Period (min) 15
Splits and Phases: 3 :


|  | 4 |  | $4$ |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | */ |  |  | ¢4 | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 259 | 94 | 52 | 353 | 885 | 75 |
| Future Volume (vph) | 259 | 94 | 52 | 353 | 885 | 75 |
| Satd. Flow (prot) | 1752 | 0 | 0 | 3557 | 3536 | 0 |
| Flt Permitted | 0.965 |  |  | 0.754 |  |  |
| Satd. Flow (perm) | 1752 | 0 | 0 | 2698 | 3536 | 0 |
| Satd. Flow (RTOR) | 39 |  |  |  | 23 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |
| Mid-Block Traffic (\%) | 0\% |  |  | 0\% | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 384 | 0 | 0 | 441 | 1044 | 0 |
| Turn Type | Perm |  | Perm | NA | NA |  |
| Protected Phases |  |  |  | 2 | 6 |  |
| Permitted Phases | 4 |  | 2 |  |  |  |
| Total Split (s) | 22.0 |  | 28.0 | 28.0 | 28.0 |  |
| Total Lost Time (s) | 5.0 |  |  | 5.0 | 5.0 |  |
| Act Effct Green (s) | 17.0 |  |  | 23.0 | 23.0 |  |
| Actuated g/C Ratio | 0.34 |  |  | 0.46 | 0.46 |  |
| v/c Ratio | 0.62 |  |  | 0.36 | 0.64 |  |
| Control Delay | 17.5 |  |  | 9.8 | 10.0 |  |
| Queue Delay | 0.0 |  |  | 0.0 | 1.7 |  |
| Total Delay | 17.5 |  |  | 9.8 | 11.6 |  |
| LOS | B |  |  | A | B |  |
| Approach Delay | 17.5 |  |  | 9.8 | 11.6 |  |
| Approach LOS | B |  |  | A | B |  |
| Queue Length 50th (m) | 24.6 |  |  | 12.2 | 28.0 |  |
| Queue Length 95th (m) | 47.0 |  |  | 20.4 | 49.7 |  |
| Internal Link Dist (m) | 240.8 |  |  | 282.1 | 29.7 |  |
| Turn Bay Length (m) |  |  |  |  |  |  |
| Base Capacity (vph) | 621 |  |  | 1241 | 1638 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 398 |  |
| Spillback Cap Reductn | 0 |  |  | 53 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.62 |  |  | 0.37 | 0.84 |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 50 |  |  |  |  |  |  |
| Actuated Cycle Length: 50 |  |  |  |  |  |  |
| Offset: 45 (90\%), Referenced to phase 2:NBTL, Start of 1st Green |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.64 |  |  |  |  |  |  |
| Intersection Signal Delay: 12.4 |  |  |  | Intersection LOS: B |  |  |
| Intersection Capacity Utilization 78.6\% |  |  |  | ICU Level of Service D |  |  |

Analysis Period (min) 15
Splits and Phases: 3 :



|  |  |  | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBR | NBL | NBT | SBT | SBR |
| Turn Bay Length ( m ) |  |  |  |  |  |
| Base Capacity (vph) 612 |  |  | 1200 | 1642 |  |
| Starvation Cap Reductn 0 |  |  | 0 | 665 |  |
| Spillback Cap Reductn 15 |  |  | 19 | 0 |  |
| Storage Cap Reductn 0 |  |  | 0 | 0 |  |
| Reduced v/c Ratio 0.79 |  |  | 0.82 | 0.95 |  |
| Intersection Summary |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |
| Cycle Length: 50 |  |  |  |  |  |
| Actuated Cycle Length: 50 |  |  |  |  |  |
| Offset: 45 (90\%), Referenced to phase 2:NBSB, Start of 1st Green |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |
| Maximum v/c Ratio: 0.81 |  |  |  |  |  |
| Intersection Signal Delay: 19.5 |  |  | Intersection LOS: B |  |  |
| Intersection Capacity Utilization 85.8\% |  |  | ICU Level of Service |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |
| m Volume for 95th percentile queue | etere | ups | sig |  |  |

Splits and Phases: 3


|  | 4 |  | 4 |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | * |  |  | ¢4 | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 427 | 39 | 98 | 860 | 722 | 191 |
| Future Volume (vph) | 427 | 39 | 98 | 860 | 722 | 191 |
| Satd. Flow (prot) | 1781 | 0 | 0 | 3561 | 3468 | 0 |
| Flt Permitted | 0.956 |  |  | 0.692 |  |  |
| Satd. Flow (perm) | 1781 | 0 | 0 | 2476 | 3468 | 0 |
| Satd. Flow (RTOR) | 10 |  |  |  | 88 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |
| Mid-Block Traffic (\%) | 0\% |  |  | 0\% | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 506 | 0 | 0 | 1042 | 993 | 0 |
| Turn Type | Perm |  | Perm | NA | NA |  |
| Protected Phases |  |  |  | 2 | 6 |  |
| Permitted Phases | 4 |  | 2 |  |  |  |
| Total Split (s) | 22.0 |  | 28.0 | 28.0 | 28.0 |  |
| Total Lost Time (s) | 5.0 |  |  | 5.0 | 5.0 |  |
| Act Effct Green (s) | 17.0 |  |  | 23.0 | 23.0 |  |
| Actuated g/C Ratio | 0.34 |  |  | 0.46 | 0.46 |  |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.83 |  |  | 0.92 | 0.60 |  |
| Control Delay | 29.6 |  |  | 28.0 | 10.2 |  |
| Queue Delay | 1.0 |  |  | 1.6 | 26.6 |  |
| Total Delay | 30.7 |  |  | 29.6 | 36.9 |  |
| LOS | C |  |  | C | D |  |
| Approach Delay | 30.7 |  |  | 29.6 | 36.9 |  |
| Approach LOS | C |  |  | C | D |  |
| Queue Length 50th (m) | 39.3 |  |  | 42.1 | 36.2 |  |
| Queue Length 95th (m) | \#84.3 |  |  | \#79.2 | m40.6 |  |
| Internal Link Dist (m) | 240.8 |  |  | 282.1 | 29.7 |  |
| Turn Bay Length (m) |  |  |  |  |  |  |
| Base Capacity (vph) | 612 |  |  | 1138 | 1642 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 686 |  |
| Spillback Cap Reductn | 21 |  |  | 29 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.86 |  |  | 0.94 | 1.04 |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 50 |  |  |  |  |  |  |
| Actuated Cycle Length: 50 |  |  |  |  |  |  |
| Offset: 45 (90\%), Referenced to phase 2:NBTL, Start of 1st Green |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.92 |  |  |  |  |  |  |
| Intersection Signal Delay: 32.7 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 91.2\% |  |  |  | ICU Level of Service F |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3:


|  | 4 |  | $4$ |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | * ${ }^{\text {r }}$ |  |  | ¢4 | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 448 | 41 | 103 | 904 | 758 | 201 |
| Future Volume (vph) | 448 | 41 | 103 | 904 | 758 | 201 |
| Satd. Flow (prot) | 1781 | 0 | 0 | 3561 | 3468 | 0 |
| Flt Permitted | 0.956 |  |  | 0.668 |  |  |
| Satd. Flow (perm) | 1781 | 0 | 0 | 2390 | 3468 | 0 |
| Satd. Flow (RTOR) | 10 |  |  |  | 88 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |
| Mid-Block Traffic (\%) | 0\% |  |  | 0\% | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 532 | 0 | 0 | 1095 | 1042 | 0 |
| Turn Type | Perm |  | Perm | NA | NA |  |
| Protected Phases |  |  |  | 2 | 6 |  |
| Permitted Phases | 4 |  | 2 |  |  |  |
| Total Split (s) | 22.0 |  | 28.0 | 28.0 | 28.0 |  |
| Total Lost Time (s) | 5.0 |  |  | 5.0 | 5.0 |  |
| Act Effct Green (s) | 17.0 |  |  | 23.0 | 23.0 |  |
| Actuated g/C Ratio | 0.34 |  |  | 0.46 | 0.46 |  |
| v/c Ratio | 0.87 |  |  | 1.00 | 0.63 |  |
| Control Delay | 33.9 |  |  | 43.4 | 10.7 |  |
| Queue Delay | 8.6 |  |  | 7.0 | 50.0 |  |
| Total Delay | 42.5 |  |  | 50.4 | 60.7 |  |
| LOS | D |  |  | D | E |  |
| Approach Delay | 42.5 |  |  | 50.4 | 60.7 |  |
| Approach LOS | D |  |  | D | E |  |
| Queue Length 50th (m) | 42.3 |  |  | 47.2 | 39.3 |  |
| Queue Length 95th (m) | \#90.6 |  |  | \#87.1 | m42.1 |  |
| Internal Link Dist (m) | 240.8 |  |  | 282.1 | 29.7 |  |
| Turn Bay Length (m) |  |  |  |  |  |  |
| Base Capacity (vph) | 612 |  |  | 1099 | 1642 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 699 |  |
| Spillback Cap Reductn | 60 |  |  | 28 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.96 |  |  | 1.02 | 1.10 |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 50 |  |  |  |  |  |  |
| Actuated Cycle Length: 50 |  |  |  |  |  |  |
| Offset: 45 (90\%), Referenced to phase 2:NBTL, Start of 1st Green |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.00 |  |  |  |  |  |  |
| Intersection Signal Delay: 52.8 |  |  |  | Intersection LOS: D |  |  |
| Intersection Capacity Utilization 95.2\% |  |  |  | ICU Level of Service F |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3:


|  |  |  | $4$ |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | */ |  |  | *4 | 中 ${ }^{\text {P }}$ |  |
| Traffic Volume (vph) | 471 | 43 | 108 | 950 | 797 | 211 |
| Future Volume (vph) | 471 | 43 | 108 | 950 | 797 | 211 |
| Satd. Flow (prot) | 1781 | 0 | 0 | 3561 | 3468 | 0 |
| Flt Permitted | 0.956 |  |  | 0.643 |  |  |
| Satd. Flow (perm) | 1781 | 0 | 0 | 2301 | 3468 | 0 |
| Satd. Flow (RTOR) | 10 |  |  |  | 88 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |
| Mid-Block Traffic (\%) | 0\% |  |  | 0\% | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 559 | 0 | 0 | 1150 | 1095 | 0 |
| Turn Type | Perm |  | Perm | NA | NA |  |
| Protected Phases |  |  |  | 2 | 6 |  |
| Permitted Phases | 4 |  | 2 |  |  |  |
| Total Split (s) | 22.0 |  | 28.0 | 28.0 | 28.0 |  |
| Total Lost Time (s) | 5.0 |  |  | 5.0 | 5.0 |  |
| Act Effct Green (s) | 17.0 |  |  | 23.0 | 23.0 |  |
| Actuated g/C Ratio | 0.34 |  |  | 0.46 | 0.46 |  |
| v/c Ratio | 0.91 |  |  | 1.09 | 0.67 |  |
| Control Delay | 39.7 |  |  | 72.3 | 11.0 |  |
| Queue Delay | 19.0 |  |  | 5.5 | 50.0 |  |
| Total Delay | 58.8 |  |  | 77.8 | 61.1 |  |
| LOS | E |  |  | E | E |  |
| Approach Delay | 58.8 |  |  | 77.8 | 61.1 |  |
| Approach LOS | E |  |  | E | E |  |
| Queue Length 50th (m) | 45.5 |  |  | $\sim 63.5$ | 41.3 |  |
| Queue Length 95th (m) | \#96.9 |  |  | \#95.3 | m43.5 |  |
| Internal Link Dist (m) | 240.8 |  |  | 282.1 | 29.7 |  |
| Turn Bay Length (m) |  |  |  |  |  |  |
| Base Capacity (vph) | 612 |  |  | 1058 | 1642 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 711 |  |
| Spillback Cap Reductn | 65 |  |  | 27 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 |  |
| Reduced v/c Ratio | 1.02 |  |  | 1.12 | 1.18 |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 50 |  |  |  |  |  |  |
| Actuated Cycle Length: 50 |  |  |  |  |  |  |
| Offset: 45 (90\%), Referenced to phase 2:NBTL, Start of 1st Green |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.09 |  |  |  |  |  |  |
| Intersection Signal Delay: 67.5 |  |  |  | Intersection LOS: E |  |  |
| Intersection Capacity Utilization 99.4\% |  |  |  | ICU Level of Service F |  |  |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3:



|  |  |  | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBR | NBL | NBT | SBT | SBR |
| Turn Bay Length ( m ) |  |  |  |  |  |
| Base Capacity (vph) 611 |  |  | 1484 | 1637 |  |
| Starvation Cap Reductn |  |  | 0 | 765 |  |
| Spillback Cap Reductn |  |  | 112 | 0 |  |
| Storage Cap Reductn |  |  | 0 | 0 |  |
| Reduced v/c Ratio 0.65 |  |  | 0.44 | 0.85 |  |
| Intersection Summary |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |
| Cycle Length: 50 |  |  |  |  |  |
| Actuated Cycle Length: 50 |  |  |  |  |  |
| Offset: 45 (90\%), Referenced to phase 2:NBSB, Start of 1st Green |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |
| Maximum v/c Ratio: 0.65 |  |  |  |  |  |
| Intersection Signal Delay: 13.1 |  |  | Intersection LOS: B |  |  |
| Intersection Capacity Utilization 63.3\% |  |  | ICU Level of Service B |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |
| m Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |  |  |

Splits and Phases: 3:


|  | 4 |  | $4$ |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | */ |  |  | ¢4 | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 371 | 21 | 29 | 565 | 615 | 116 |
| Future Volume (vph) | 371 | 21 | 29 | 565 | 615 | 116 |
| Satd. Flow (prot) | 1786 | 0 | 0 | 3571 | 3493 | 0 |
| Flt Permitted | 0.955 |  |  | 0.894 |  |  |
| Satd. Flow (perm) | 1786 | 0 | 0 | 3199 | 3493 | 0 |
| Satd. Flow (RTOR) | 6 |  |  |  | 58 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |
| Mid-Block Traffic (\%) | 0\% |  |  | 0\% | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 426 | 0 | 0 | 646 | 794 | 0 |
| Turn Type | Perm |  | Perm | NA | NA |  |
| Protected Phases |  |  |  | 2 | 6 |  |
| Permitted Phases | 4 |  | 2 |  |  |  |
| Total Split (s) | 22.0 |  | 28.0 | 28.0 | 28.0 |  |
| Total Lost Time (s) | 5.0 |  |  | 5.0 | 5.0 |  |
| Act Effct Green (s) | 17.0 |  |  | 23.0 | 23.0 |  |
| Actuated g/C Ratio | 0.34 |  |  | 0.46 | 0.46 |  |
| v/c Ratio | 0.70 |  |  | 0.44 | 0.48 |  |
| Control Delay | 21.9 |  |  | 10.3 | 9.5 |  |
| Queue Delay | 0.0 |  |  | 0.1 | 5.8 |  |
| Total Delay | 21.9 |  |  | 10.4 | 15.2 |  |
| LOS | C |  |  | B | B |  |
| Approach Delay | 21.9 |  |  | 10.4 | 15.2 |  |
| Approach LOS | C |  |  | B | B |  |
| Queue Length 50th (m) | 31.4 |  |  | 18.8 | 27.4 |  |
| Queue Length 95th (m) | \#65.5 |  |  | 29.2 | m34.3 |  |
| Internal Link Dist (m) | 240.8 |  |  | 282.1 | 29.7 |  |
| Turn Bay Length (m) |  |  |  |  |  |  |
| Base Capacity (vph) | 611 |  |  | 1471 | 1638 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 774 |  |
| Spillback Cap Reductn | 0 |  |  | 128 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.70 |  |  | 0.48 | 0.92 |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 50 |  |  |  |  |  |  |
| Actuated Cycle Length: 50 |  |  |  |  |  |  |
| Offset: 45 (90\%), Referenced to phase 2:NBTL, Start of 1st Green |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.70 |  |  |  |  |  |  |
| Intersection Signal Delay: 15.1 |  |  |  | Intersection LOS: B |  |  |
| Intersection Capacity Utilization 67.3\% |  |  |  | ICU Level of Service C |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3:


|  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3:


|  | 4 |  | $4$ |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | */ |  |  | ¢4 | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 410 | 24 | 32 | 624 | 680 | 128 |
| Future Volume (vph) | 410 | 24 | 32 | 624 | 680 | 128 |
| Satd. Flow (prot) | 1786 | 0 | 0 | 3571 | 3493 | 0 |
| Flt Permitted | 0.955 |  |  | 0.885 |  |  |
| Satd. Flow (perm) | 1786 | 0 | 0 | 3167 | 3493 | 0 |
| Satd. Flow (RTOR) | 6 |  |  |  | 57 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |
| Mid-Block Traffic (\%) | 0\% |  |  | 0\% | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 472 | 0 | 0 | 713 | 878 | 0 |
| Turn Type | Perm |  | Perm | NA | NA |  |
| Protected Phases |  |  |  | 2 | 6 |  |
| Permitted Phases | 4 |  | 2 |  |  |  |
| Total Split (s) | 22.0 |  | 28.0 | 28.0 | 28.0 |  |
| Total Lost Time (s) | 5.0 |  |  | 5.0 | 5.0 |  |
| Act Effct Green (s) | 17.0 |  |  | 23.0 | 23.0 |  |
| Actuated g/C Ratio | 0.34 |  |  | 0.46 | 0.46 |  |
| v/c Ratio | 0.77 |  |  | 0.49 | 0.54 |  |
| Control Delay | 25.9 |  |  | 10.9 | 10.2 |  |
| Queue Delay | 0.2 |  |  | 0.0 | 25.7 |  |
| Total Delay | 26.1 |  |  | 10.9 | 35.9 |  |
| LOS | C |  |  | B | D |  |
| Approach Delay | 26.1 |  |  | 10.9 | 35.9 |  |
| Approach LOS | C |  |  | B | D |  |
| Queue Length 50th (m) | 36.1 |  |  | 21.5 | 32.2 |  |
| Queue Length 95th (m) | \#76.6 |  |  | 33.0 | m38.9 |  |
| Internal Link Dist (m) | 240.8 |  |  | 282.1 | 29.7 |  |
| Turn Bay Length (m) |  |  |  |  |  |  |
| Base Capacity (vph) | 611 |  |  | 1456 | 1637 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 787 |  |
| Spillback Cap Reductn | 8 |  |  | 21 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.78 |  |  | 0.50 | 1.03 |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 50 |  |  |  |  |  |  |
| Actuated Cycle Length: 50 |  |  |  |  |  |  |
| Offset: 45 (90\%), Referenced to phase 2:NBTL, Start of 1st Green |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.77 |  |  |  |  |  |  |
| Intersection Signal Delay: 25.0 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 73.5\% |  |  |  | ICU Level of Service D |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3:


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 3 | 1 | 178 | 2 | 6 | 463 |
| Future Vol, veh/h | 3 | 1 | 178 | 2 | 6 | 463 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 1 | 193 | 2 | 7 | 503 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 0.1 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | F |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 3 | 1 | 191 | 2 | 6 | 496 |
| Future Vol, veh/h | 3 | 1 | 191 | 2 | 6 | 496 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 1 | 208 | 2 | 7 | 539 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 1 |  | 1 |  |  |  |
| Traffic Vol, veh/h | 3 | 1 | 201 | 2 | 6 | 522 |
| Future Vol, veh/h | 3 | 1 | 201 | 2 | 6 | 522 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 1 | 218 | 2 | 7 | 567 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 1 |  | 1 |  | -1 |  |
| Traffic Vol, veh/h | 3 | 1 | 211 | 2 | 6 | 548 |
| Future Vol, veh/h | 3 | 1 | 211 | 2 | 6 | 548 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 1 | 229 | 2 | 7 | 596 |







| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 1 |  | 6 |  | 4 |  |
| Traffic Vol, veh/h | 5 | 5 | 861 | 4 | 4 | 763 |
| Future Vol, veh/h | 5 | 5 | 861 | 4 | 4 | 763 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 5 | 936 | 4 | 4 | 829 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 0.3 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | F |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 5 | 5 | 905 | 4 | 4 | 802 |
| Future Vol, veh/h | 5 | 5 | 905 | 4 | 4 | 802 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 5 | 984 | 4 | 4 | 872 |



| Intersection |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | 1 | 1 |  | -1 |  |  |  |
| Traffic Vol, veh/h | 2 | 2 | 226 | 1 | 2 | 313 |  |
| Future Vol, veh/h | 2 | 2 | 226 | 1 | 2 | 313 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Free | Free | Free | Free |  |
| RT Channelized | - | None | - | None | - | None |  |
| Storage Length | 0 | - | - | - | - | - |  |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |  |
| Grade, \% | 0 | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 2 | 2 | 246 | 1 | 2 | 340 |  |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | F |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 2 | 2 | 242 | 1 | 2 | 336 |
| Future Vol, veh/h | 2 | 2 | 242 | 1 | 2 | 336 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 2 | 2 | 263 | 1 | 2 | 365 |



| Intersection |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | 1 | 1 |  | -1 |  |  |  |
| Traffic Vol, veh/h | 2 | 2 | 255 | 1 | 2 | 353 |  |
| Future Vol, veh/h | 2 | 2 | 255 | 1 | 2 | 353 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Free | Free | Free | Free |  |
| RT Channelized | - | None | - | None | - | None |  |
| Storage Length | 0 | - | - | - | - | - |  |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |  |
| Grade, \% | 0 | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 2 | 2 | 277 | 1 | 2 | 384 |  |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * ${ }^{\prime}$ |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 2 | 2 | 268 | 1 | 2 | 371 |
| Future Vol, veh/h | 2 | 2 | 268 | 1 | 2 | 371 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | St | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 2 | 291 | 1 | 2 | 403 |



|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay, s/veh }} 0.2$ |  |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations |  | $\uparrow$ | $\hat{\beta}$ |  | M |  |
| Traffic Vol, veh/h | 1 | 132 | 130 | 1 | 3 | 2 |
| Future Vol, veh/h | 1 | 132 | 130 | 1 | 3 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 143 | 141 | 1 | 3 | 2 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | M |  |
| Traffic Vol, veh/h | 1 | 142 | 139 | 1 | 3 | 2 |
| Future Vol, veh/h | 1 | 142 | 139 | 1 | 3 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 1 | 154 | 151 | 1 | 3 | 2 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | M |  |
| Traffic Vol, veh/h | 1 | 149 | 146 | 1 | 3 | 2 |
| Future Vol, veh/h | 1 | 149 | 146 | 1 | 3 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 1 | 162 | 159 | 1 | 3 | 2 |



|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay, s/veh }} 0.2$ |  |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations |  | $\uparrow$ | $\hat{\dagger}$ |  | M |  |
| Traffic Vol, veh/h | 1 | 156 | 154 | 1 | 3 | 2 |
| Future Vol, veh/h | 1 | 156 | 154 | 1 | 3 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 170 | 167 | 1 | 3 | 2 |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations |  | $\uparrow$ | $\hat{\beta}$ |  | M |  |
| Traffic Vol, veh/h | 5 | 762 | 134 | 1 | 3 | 1 |
| Future Vol, veh/h | 5 | 762 | 134 | 1 | 3 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 828 | 146 | 1 | 3 | 1 |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay, s/veh }} 0.2$ |  |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations |  | $\uparrow$ |  |  | M |  |
| Traffic Vol, veh/h | 3 | 192 | 77 | 1 | 3 | 1 |
| Future Vol, veh/h | 3 | 192 | 77 | 1 | 3 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 209 | 84 | 1 | 3 | 1 |



|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay, s/veh }} 0.2$ |  |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations |  | $\uparrow$ | $\hat{\beta}$ |  | M |  |
| Traffic Vol, veh/h | 3 | 202 | 81 | 1 | 3 | 1 |
| Future Vol, veh/h | 3 | 202 | 81 | 1 | 3 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 220 | 88 | 1 |  | 1 |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.6 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | * |  |
| Traffic Vol, veh/h | 2 | 161 | 128 | 32 | 14 | 3 |
| Future Vol, veh/h | 2 | 161 | 128 | 32 | 14 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 175 | 139 | 35 | 15 | 3 |



|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay, s/veh }} 0.5$ |  |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\hat{\dagger}$ |  | M |  |
| Traffic Vol, veh/h | 2 | 173 | 137 | 32 | 14 | 3 |
| Future Vol, veh/h | 2 | 173 | 137 | 32 | 14 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 188 | 149 | 35 | 15 | 3 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement |  | EBL | EBT | WBT | WBR | SBL |
| Lane Configurations |  | A | 1 |  | SBR |  |
| Traffic Vol, veh/h | 2 | 181 | 144 | 32 | 14 |  |
| Future Vol, veh/h | 2 | 181 | 144 | 32 | 14 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 197 | 157 | 35 | 15 | 3 |





|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay, s/veh }} 0.6$ |  |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\hat{1}$ |  | M |  |
| Traffic Vol, veh/h | 2 | 558 | 114 | 20 | 28 | 0 |
| Future Vol, veh/h | 2 | 558 | 114 | 20 | 28 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 607 | 124 | 22 | 30 | 0 |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |





|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IntersectionInt Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | M |  |
| Traffic Vol, veh/h | 0 | 192 | 75 | 16 | 12 | 3 |
| Future Vol, veh/h | 0 | 192 | 75 | 16 | 12 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 209 | 82 | 17 | 13 | 3 |





| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | M |  |
| Traffic Vol, veh/h | 0 | 212 | 83 | 16 | 12 | 3 |
| Future Vol, veh/h | 0 | 212 | 83 | 16 | 12 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 230 | 90 | 17 | 13 | 3 |



HCM 2010 TWSC
43: Rothesay Ave \& Rothesay Rd

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 63.6 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 164 |  | 126 |  | 4 | 4 |
| Traffic Vol, veh/h | 164 | 63 | 64 | 329 | 458 |  |
| Future Vol, veh/h | 164 | 126 | 63 | 64 | 329 | 458 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 178 | 137 | 68 | 70 | 358 | 498 |



HCM 2010 TWSC
43: Rothesay Ave \& Rothesay Rd

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 100 | 100.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | \$ |  | F |  | ${ }^{7}$ | 4 |
| Traffic Vol, veh/h | 176 | 135 | 68 | 69 | 352 | 491 |
| Future Vol, veh/h | 176 | 135 | 68 | 69 | 352 | 491 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 191 | 147 | 74 | 75 | 383 | 534 |



HCM 2010 TWSC
43: Rothesay Ave \& Rothesay Rd



HCM 2010 TWSC
43: Rothesay Ave \& Rothesay Rd

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 178.1 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | F |  | ${ }^{1}$ | 4 |
| Traffic Vol, veh/h | 194 | 149 | 75 | 76 | 389 | 542 |
| Future Vol, veh/h | 194 | 149 | 75 | 76 | 389 | 542 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 211 | 162 | 82 | 83 | 423 | 589 |


| Major/Minor | Minor |  |  |  | Major1 |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 151 |  | 82 |  | 0 | - | 82 | 0 |  |
| Stage 1 | 8 |  | - |  | - | - | - | - |  |
| Stage 2 | 143 |  | - |  | - | - | - | - |  |
| Critical Hdwy | 6.4 |  | 6.22 |  | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.4 |  | - |  | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.4 |  | - |  | - | - | - | - |  |
| Follow-up Hdwy | 3.51 |  | 3.318 |  | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | $\sim 13$ |  | 978 |  | - | 0 | 1515 | - |  |
| Stage 1 | 94 |  | - |  | - | 0 | - | - |  |
| Stage 2 | 21 |  | - |  | - | 0 | - | - |  |
| Platoon blocked, \% |  |  |  |  | - |  |  | - |  |
| Mov Cap-1 Maneuver | $\sim 9$ |  | 978 |  | - | - | 1515 | - |  |
| Mov Cap-2 Maneuver | $\sim 9$ |  | - |  | - | - | - | - |  |
| Stage 1 | 94 |  | - |  | - | - | - | - |  |
| Stage 2 | $\sim 15$ |  | - |  | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |
| Approach | W |  |  |  | NB |  | SB |  |  |
| HCM Control Delay, s | \$ 69 |  |  |  | 0 |  | 3.5 |  |  |
| HCM LOS |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | BLn1 | SBL | SBT |  |  |  |  |  |
| Capacity (veh/h) |  | 156 | 1515 | - |  |  |  |  |  |
| HCM Lane V/C Ratio |  | 2.39 | 0.279 | - |  |  |  |  |  |
| HCM Control Delay (s) |  | \$ 691 | 8.3 | - |  |  |  |  |  |
| HCM Lane LOS |  | F | A | - |  |  |  |  |  |
| HCM 95th \%tile Q(veh) |  | 31.5 | 1.2 | - |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds cap | \$: Delay exceeds 300s |  |  |  | +: Computation Not Defined |  | *: All major volume in platoon |  |  |

HCM 2010 TWSC
44: Rothesay Ave \& Rothesay Rd

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | $\uparrow$ |  | ${ }^{7}$ | 4 |
| Traffic Vol, veh/h | 88 | 363 | 445 | 75 | 422 | 140 |
| Future Vol, veh/h | 88 | 363 | 445 | 75 | 422 | 140 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 96 | 395 | 484 | 82 | 459 | 152 |



HCM 2010 TWSC
44: Rothesay Ave \& Rothesay Rd

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 225.9 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | $T$ |  | 1 |  | 4 | 4 |
| Traffic Vol, veh/h | 95 | 390 | 477 | 80 | 453 | 150 |
| Future Vol, veh/h | 95 | 390 | 477 | 80 | 453 | 150 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 103 | 424 | 518 | 87 | 492 | 163 |



HCM 2010 TWSC
44: Rothesay Ave \& Rothesay Rd

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 310.3 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 1 |  | 1 |  | 4 | 4 |
| Traffic Vol, veh/h | 99 | 409 | 502 | 84 | 476 | 157 |
| Future Vol, veh/h | 99 | 409 | 502 | 84 | 476 | 157 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 108 | 445 | 546 | 91 | 517 | 171 |



HCM 2010 TWSC
44: Rothesay Ave \& Rothesay Rd

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 411.1 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | F |  | ${ }^{1}$ | 4 |
| Traffic Vol, veh/h | 104 | 430 | 527 | 88 | 500 | 165 |
| Future Vol, veh/h | 104 | 430 | 527 | 88 | 500 | 165 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 113 | 467 | 573 | 96 | 543 | 179 |


| Major/Minor | Minor1 |  |  | Major1 |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1839 | 573 |  | 0 | - | 573 | 0 |  |
| Stage 1 | 573 | - |  | - | - | - | - |  |
| Stage 2 | 1266 | - |  | - | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 |  | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.42 | - |  | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - |  | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 |  | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | $\sim 83$ | 519 |  | - | 0 | 1000 | - |  |
| Stage 1 | 564 | - |  | - | 0 | - | - |  |
| Stage 2 | 265 | - |  | - | 0 | - | - |  |
| Platoon blocked, \% |  |  |  | - |  |  | - |  |
| Mov Cap-1 Maneuver | $\sim 38$ | 519 |  | - | - | 1000 | - |  |
| Mov Cap-2 Maneuver | $\sim 38$ | - |  | - | - | - | - |  |
| Stage 1 | 564 | - |  | - | - | - | - |  |
| Stage 2 | 121 | - |  | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |
| Approach | WB |  |  | NB |  | SB |  |  |
| HCM Control Delay, s | \$ 1316.9 |  |  | 0 |  | 9.6 |  |  |
| HCM LOS | F |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBTWBLn1 | SBL | SBT |  |  |  |  |  |
| Capacity (veh/h) | - 153 | 1000 | - |  |  |  |  |  |
| HCM Lane V/C Ratio | - 3.794 | 0.543 | - |  |  |  |  |  |
| HCM Control Delay (s) | \$1316.9 | 12.8 | - |  |  |  |  |  |
| HCM Lane LOS | - F | B | - |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | - 57.2 | 3.4 | - |  |  |  |  |  |
| $\frac{\text { Notes }}{\sim}$ Volume exceeds capacity $\quad \$$. Delay exceeds 300s + Computation Not Defined * All major volume in platoon |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

HCM 2010 TWSC
43: Rothesay Ave \& Rothesay Rd



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 77.8 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | $\uparrow$ |  | * | 4 |
| Traffic Vol, veh/h | 258 | 178 | 66 | 99 | 291 | 69 |
| Future Vol, veh/h | 258 | 178 | 66 | 99 | 291 | 69 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 280 | 193 | 72 | 108 | 316 | 75 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 85 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | $\uparrow$ |  | * | 4 |
| Traffic Vol, veh/h | 272 | 187 | 70 | 104 | 305 | 72 |
| Future Vol, veh/h | 272 | 187 | 70 | 104 | 305 | 72 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Stop | - | Free | - | None |
| Storage Length | 0 | - | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 296 | 203 | 76 | 113 | 332 | 78 |





| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.3 |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 |  | $\uparrow$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 22 | 161 | 108 | 80 | 308 | 60 |
| Future Vol, veh/h | 22 | 161 | 108 | 80 | 308 | 60 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 800 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 24 | 175 | 117 | 87 | 335 | 65 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.5 |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 |  | $\uparrow$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 24 | 173 | 116 | 86 | 330 | 64 |
| Future Vol, veh/h | 24 | 173 | 116 | 86 | 330 | 64 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 800 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 26 | 188 | 126 | 93 | 359 | 70 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 |  | $\uparrow$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 26 | 191 | 128 | 95 | 365 | 71 |
| Future Vol, veh/h | 26 | 191 | 128 | 95 | 365 | 71 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 800 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 28 | 208 | 139 | 103 | 397 | 77 |





| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | * |  |  | * |  |  | \& |  |
| Traffic Vol, veh/h | 112 | 1 | 575 | 1 | 0 | 2 | 128 | 281 | 5 | 0 | 155 | 18 |
| Future Vol, veh/h | 112 | 1 | 575 | 1 | 0 | 2 | 128 | 281 | 5 | 0 | 155 | 18 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 800 | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 122 | 1 | 625 | 1 | 0 | 2 | 139 | 305 | 5 | 0 | 168 | 20 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | \$ |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 117 | 1 | 604 | 1 | 0 | 2 | 134 | 295 | 5 | 0 | 163 | 19 |
| Future Vol, veh/h | 117 | 1 | 604 | 1 | 0 | 2 | 134 | 295 | 5 | 0 | 163 | 19 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 800 | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 127 | 1 | 657 | 1 | 0 | 2 | 146 | 321 | 5 | 0 | 177 | 21 |


| Major/Minor | Minor2 |  | Minor1 |  |  |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 804 | 805 | 188 |  | 803 | 813 | 323 |  | 198 | 0 | 0 | 326 | 0 | 0 |
| Stage 1 | 188 | 188 | - |  | 615 | 615 | - |  | - | - | - | - | - | - |
| Stage 2 | 616 | 617 | - |  | 188 | 198 | - |  | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 301 | 316 | 854 |  | 302 | 313 | 718 |  | 1375 | - | - | 1234 | - | - |
| Stage 1 | 814 | 745 | - |  | 479 | 482 | - |  | - | - | - | - | - |  |
| Stage 2 | 478 | 481 | - |  | 814 | 737 | - |  | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 270 | 275 | 854 |  | 63 | 272 | 718 |  | 1375 | - | - | 1234 | - |  |
| Mov Cap-2 Maneuver | 270 | 275 | - |  | 63 | 272 | - |  | - | - | - | - | - |  |
| Stage 1 | 708 | 745 | - |  | 417 | 419 | - |  | - | - | - | - | - |  |
| Stage 2 | 415 | 418 | - |  | 188 | 737 | - |  | - | - | - | - | - |  |
| Approach | EB |  |  |  | WB |  |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 23 |  |  |  | 27.8 |  |  |  | 2.4 |  |  | 0 |  |  |
| HCM LOS | C |  |  |  | D |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | BLn1 | EBLn2 | NBLn1 | SBL | SBT | SBR |  |  |  |  |  |
| Capacity (veh/h) | 1375 | - | - | 270 | 854 | 161 | 1234 | - | - |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.106 | - | - | 0.475 | 0.769 | 0.02 | - | - | - |  |  |  |  |  |
| HCM Control Delay (s) | 7.9 | 0 | - | 29.8 | 21.7 | 27.8 | 0 | - | - |  |  |  |  |  |
| HCM Lane LOS | A | A | - | D | C | D | A | - | - |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0.4 | - | - | 2.4 | 7.6 | 0.1 | 0 | - | - |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 15.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | \& |  |  | \& |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 123 | 1 | 635 | 1 | 0 | 2 | 141 | 310 | 5 | 0 | 172 | 20 |
| Future Vol, veh/h | 123 | 1 | 635 | 1 | 0 | 2 | 141 | 310 | 5 | 0 | 172 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 800 | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 134 | 1 | 690 | 1 | 0 | 2 | 153 | 337 | 5 | 0 | 187 | 22 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 |  | $\uparrow$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 49 | 155 | 59 | 159 | 158 | 21 |
| Future Vol, veh/h | 49 | 155 | 59 | 159 | 158 | 21 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 800 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 53 | 168 | 64 | 173 | 172 | 23 |





| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.6 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 |  | $\uparrow$ | 个 |  |
| Traffic Vol, veh/h | 55 | 175 | 66 | 179 | 178 | 24 |
| Future Vol, veh/h | 55 | 175 | 66 | 179 | 178 | 24 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | St | None | - | None | - | None |
| Storage Length | 0 | 800 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 60 | 190 | 72 | 195 | 193 | 26 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 |  | $\uparrow$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 58 | 184 | 70 | 188 | 187 | 25 |
| Future Vol, veh/h | 58 | 184 | 70 | 188 | 187 | 25 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 800 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 63 | 200 | 76 | 204 | 203 | 27 |




|  | 4 |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{}$ |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 0 | 71 | 350 | 0 | 298 | 0 | 0 | 0 | 0 | 0 | 800 | 24 |
| Future Volume (Veh/h) | 0 | 71 | 350 | 0 | 298 | 0 | 0 | 0 | 0 | 0 | 800 | 24 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 77 | 380 | 0 | 324 | 0 | 0 | 0 | 0 | 0 | 870 | 26 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 1032 | 870 | 870 | 908 | 870 | 0 | 870 |  |  | 0 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1032 | 870 | 870 | 908 | 870 | 0 | 870 |  |  | 0 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 0 | 73 | 0 | 0 | 0 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 0 | 290 | 351 | 0 | 290 | 1085 | 775 |  |  | 1623 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SB 1 | SB 2 |  |  |  |  |  |  |  |  |
| Volume Total | 457 | 324 | 870 | 26 |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |
| Volume Right | 380 | 0 | 0 | 26 |  |  |  |  |  |  |  |  |
| cSH | 339 | 290 | 1700 | 1700 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 1.35 | 1.12 | 0.51 | 0.02 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 170.4 | 101.6 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 206.4 | 127.5 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 206.4 | 127.5 | 0.0 |  |  |  |  |  |  |  |  |  |
| Approach LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 80.9 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 74.1\% | ICU Level of Service |  |  |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |






|  | 4 | $\rightarrow$ | $\checkmark$ | 7 |  | 4 | 4 | $\dagger$ | \% |  | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | 4 |  |  |  |  |  | 4 | 「 |
| Traffic Volume (veh/h) | 0 | 227 | 332 | 0 | 515 | 0 | 0 | 0 | 0 | 0 | 282 | 9 |
| Future Volume (Veh/h) | 0 | 227 | 332 | 0 | 515 | 0 | 0 | 0 | 0 | 0 | 282 | 9 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 247 | 361 | 0 | 560 | 0 | 0 | 0 | 0 | 0 | 307 | 10 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 587 | 307 | 307 | 430 | 307 | 0 | 307 |  |  | 0 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC 2 , stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 587 | 307 | 307 | 430 | 307 | 0 | 307 |  |  | 0 |  |  |
| tC , single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 59 | 51 | 100 | 8 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 81 | 607 | 733 | 185 | 607 | 1085 | 1254 |  |  | 1623 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SB 1 | SB 2 |  |  |  |  |  |  |  |  |
| Volume Total | 608 | 560 | 307 | 10 |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |
| Volume Right | 361 | 0 | 0 | 10 |  |  |  |  |  |  |  |  |
| cSH | 676 | 607 | 1700 | 1700 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.90 | 0.92 | 0.18 | 0.01 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 87.0 | 90.1 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 39.4 | 46.1 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | E | E |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 39.4 | 46.1 | 0.0 |  |  |  |  |  |  |  |  |  |
| Approach LOS | E | E |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 33.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 53.8\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |



|  | 4 |  |  | $\downarrow$ |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{}$ |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 0 | 73 | 290 | 0 | 433 | 0 | 0 | 0 | 0 | 0 | 720 | 13 |
| Future Volume (Veh/h) | 0 | 73 | 290 | 0 | 433 | 0 | 0 | 0 | 0 | 0 | 720 | 13 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | , | 79 | 315 | 0 | 471 | 0 | 0 | 0 | 0 | 0 | 783 | 14 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 1018 | 783 | 783 | 822 | 783 | 0 | 783 |  |  | 0 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 1018 | 783 | 783 | 822 | 783 | 0 | 783 |  |  | 0 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 0 | 76 | 20 | 100 | 0 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 0 | 325 | 394 | 48 | 325 | 1085 | 835 |  |  | 1623 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SB 1 | SB 2 |  |  |  |  |  |  |  |  |
| Volume Total | 394 | 471 | 783 | 14 |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |
| Volume Right | 315 | 0 | 0 | 14 |  |  |  |  |  |  |  |  |
| cSH | 378 | 325 | 1700 | 1700 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 1.04 | 1.45 | 0.46 | 0.01 |  |  |  |  |  |  |  |  |
| Queue Length 95th ( m ) | 100.4 | 191.6 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 91.7 | 248.4 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 91.7 | 248.4 | 0.0 |  |  |  |  |  |  |  |  |  |
| Approach LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 92.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 67.4\% | ICU Level of Service |  |  |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |


|  | 4 |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{\square}$ |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 0 | 78 | 311 | 0 | 464 | 0 | 0 | 0 | 0 | 0 | 772 | 14 |
| Future Volume (Veh/h) | 0 | 78 | 311 | 0 | 464 | 0 | 0 | 0 | 0 | 0 | 772 | 14 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 85 | 338 | 0 | 504 | 0 | 0 | 0 | 0 | 0 | 839 | 15 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 1091 | 839 | 839 | 882 | 839 | 0 | 839 |  |  | 0 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1091 | 839 | 839 | 882 | 839 | 0 | 839 |  |  | 0 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 0 | 72 | 8 | 100 | 0 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 0 | 302 | 366 | 16 | 302 | 1085 | 796 |  |  | 1623 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SB 1 | SB 2 |  |  |  |  |  |  |  |  |
| Volume Total | 423 | 504 | 839 | 15 |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |
| Volume Right | 338 | 0 | 0 | 15 |  |  |  |  |  |  |  |  |
| cSH | 351 | 302 | 1700 | 1700 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 1.21 | 1.67 | 0.49 | 0.01 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 136.0 | 237.8 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 149.5 | 345.3 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 149.5 | 345.3 | 0.0 |  |  |  |  |  |  |  |  |  |
| Approach LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 133.2 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 71.7\% | ICU Level of Service |  |  |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |


|  | 4 |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{\square}$ |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 0 | 82 | 327 | 0 | 488 | 0 | 0 | 0 | 0 | 0 | 811 | 15 |
| Future Volume (Veh/h) | 0 | 82 | 327 | 0 | 488 | 0 | 0 | 0 | 0 | 0 | 811 | 15 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 89 | 355 | 0 | 530 | 0 | 0 | 0 | 0 | 0 | 882 | 16 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 1147 | 882 | 882 | 926 | 882 | 0 | 882 |  |  | 0 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1147 | 882 | 882 | 926 | 882 | 0 | 882 |  |  | 0 |  |  |
| tC , single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 0 | 69 | 0 | 0 | 0 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 0 | 285 | 345 | 0 | 285 | 1085 | 767 |  |  | 1623 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SB 1 | SB 2 |  |  |  |  |  |  |  |  |
| Volume Total | 444 | 530 | 882 | 16 |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |
| Volume Right | 355 | 0 | 0 | 16 |  |  |  |  |  |  |  |  |
| cSH | 331 | 285 | 1700 | 1700 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 1.34 | 1.86 | 0.52 | 0.01 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 165.3 | 274.5 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 203.8 | 430.0 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 203.8 | 430.0 | 0.0 |  |  |  |  |  |  |  |  |  |
| Approach LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 170.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 75.0\% | ICU Level of Service |  |  |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |


|  | 4 |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{\square}$ |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 0 | 86 | 343 | 0 | 513 | 0 | 0 | 0 | 0 | 0 | 853 | 15 |
| Future Volume (Veh/h) | 0 | 86 | 343 | 0 | 513 | 0 | 0 | 0 | 0 | 0 | 853 | 15 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 93 | 373 | 0 | 558 | 0 | 0 | 0 | 0 | 0 | 927 | 16 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 1206 | 927 | 927 | 974 | 927 | 0 | 927 |  |  | 0 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1206 | 927 | 927 | 974 | 927 | 0 | 927 |  |  | 0 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 0 | 65 | 0 | 0 | 0 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 0 | 268 | 325 | 0 | 268 | 1085 | 737 |  |  | 1623 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SB 1 | SB 2 |  |  |  |  |  |  |  |  |
| Volume Total | 466 | 558 | 927 | 16 |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |
| Volume Right | 373 | 0 | 0 | 16 |  |  |  |  |  |  |  |  |
| cSH | 312 | 268 | 1700 | 1700 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 1.49 | 2.08 | 0.55 | 0.01 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 197.4 | 313.7 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 269.2 | 528.9 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 269.2 | 528.9 | 0.0 |  |  |  |  |  |  |  |  |  |
| Approach LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 213.8 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 78.6\% | ICU Level of Service |  |  |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |





|  | 4 |  |  | $\dagger$ |  |  |  | $\dagger$ |  |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (veh/h) | 0 | 202 | 0 | 0 | 0 | 0 | 0 | 457 | 0 | 0 | 0 | 0 |
| Future Volume (Veh/h) | 0 | 202 | 0 | 0 | 0 | 0 | 0 | 457 | 0 | 0 | 0 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 220 | 0 | 0 | 0 | 0 | 0 | 497 | 0 | 0 | 0 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 497 | 497 | 0 | 607 | 497 | 497 | 0 |  |  | 497 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 497 | 497 | 0 | 607 | 497 | 497 | 0 |  |  | 497 |  |  |
| tC , single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 54 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 483 | 475 | 1085 | 260 | 475 | 573 | 1623 |  |  | 1067 |  |  |
| Direction, Lane \# | EB 1 | NB 1 |  |  |  |  |  |  |  |  |  |  |
| Volume Total | 220 | 497 |  |  |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| Volume Right | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| cSH | 475 | 1700 |  |  |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.46 | 0.29 |  |  |  |  |  |  |  |  |  |  |
| Queue Length 95th ( m ) | 18.3 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 19.0 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Lane LOS | C |  |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 19.0 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 5.8 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 41.4\% |  | U Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |




|  | 4 |  |  | $\dagger$ |  |  |  | 4 |  |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (veh/h) | 0 | 239 | 0 | 0 | 0 | 0 | 0 | 541 | 0 | 0 | 0 | 0 |
| Future Volume (Veh/h) | 0 | 239 | 0 | 0 | 0 | 0 | 0 | 541 | 0 | 0 | 0 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 260 | 0 | 0 | 0 | 0 | 0 | 588 | 0 | 0 | 0 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 588 | 588 | 0 | 718 | 588 | 588 | 0 |  |  | 588 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 588 | 588 | 0 | 718 | 588 | 588 | 0 |  |  | 588 |  |  |
| tC , single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 38 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 421 | 421 | 1085 | 174 | 421 | 509 | 1623 |  |  | 987 |  |  |
| Direction, Lane \# | EB 1 | NB 1 |  |  |  |  |  |  |  |  |  |  |
| Volume Total | 260 | 588 |  |  |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| Volume Right | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| cSH | 421 | 1700 |  |  |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.62 | 0.35 |  |  |  |  |  |  |  |  |  |  |
| Queue Length 95th ( m ) | 30.6 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 26.4 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Lane LOS | D |  |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 26.4 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Approach LOS | D |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 8.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 47.7\% |  | U Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |



|  | 4 |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (veh/h) | 0 | 78 | 0 | 0 | 0 | 0 | 0 | 464 | 0 | 0 | 0 | 0 |
| Future Volume (Veh/h) | 0 | 78 | 0 | 0 | 0 | 0 | 0 | 464 | 0 | 0 | 0 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 504 | 0 | 0 | 0 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 504 | 504 | 0 | 546 | 504 | 504 | 0 |  |  | 504 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 504 | 504 | 0 | 546 | 504 | 504 | 0 |  |  | 504 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 82 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 478 | 470 | 1085 | 386 | 470 | 568 | 1623 |  |  | 1061 |  |  |
| Direction, Lane \# | EB 1 | NB 1 |  |  |  |  |  |  |  |  |  |  |
| Volume Total | 85 | 504 |  |  |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| Volume Right | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| cSH | 470 | 1700 |  |  |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.18 | 0.30 |  |  |  |  |  |  |  |  |  |  |
| Queue Length 95th ( m ) | 5.0 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 14.3 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Lane LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 14.3 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 35.2\% | ICU Level of Service |  |  |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (veh/h) | 0 | 82 | 0 | 0 | 0 | 0 | 0 | 488 | 0 | 0 | 0 | 0 |
| Future Volume (Veh/h) | 0 | 82 | 0 | 0 | 0 | 0 | 0 | 488 | 0 | 0 | 0 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 89 | 0 | 0 | 0 | 0 | 0 | 530 | 0 | 0 | 0 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 530 | 530 | 0 | 574 | 530 | 530 | 0 |  |  | 530 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 530 | 530 | 0 | 574 | 530 | 530 | 0 |  |  | 530 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 80 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 460 | 455 | 1085 | 365 | 455 | 549 | 1623 |  |  | 1037 |  |  |
| Direction, Lane \# | EB 1 | NB 1 |  |  |  |  |  |  |  |  |  |  |
| Volume Total | 89 | 530 |  |  |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| Volume Right | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| cSH | 455 | 1700 |  |  |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.20 | 0.31 |  |  |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 5.5 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 14.8 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Lane LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 14.8 | 0.0 |  |  |  |  |  |  |  |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 36.7\% | ICU Level of Service |  |  |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
















$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 514 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$151 \quad \mathrm{vph}$
300 m
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  | m |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{V}$ | 628 | 4600 | No |
| Fi F |  |  |  |
| v | 628 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 459 | 4600 | No |
| FO F R |  |  |  |
| v | 169 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$


## Phone:

Fax:
E-mail:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 551 | vph |


|  | Off Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-Flow speed on ramp | 60.0 | vph |
| Volume on ramp | 162 | m |
| Length of first accel/decel lane | 300 | m |
| Length of second accel/decel lane |  |  |

Does adjacent ramp exist?
Volume on adjacent ramp
Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp

No
vph

$\qquad$


Capacity Checks

|  |  |  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathrm{V} \\ \mathrm{Fi} \end{gathered}$ |  |  | 673 | 4600 | No |
|  |  |  |  |  |  |
| v |  |  | 673 | 4400 | No |
| 12 |  |  |  |  |  |
| v FO $=$ | v - | v | 491 | 4600 | No |
|  | F | R |  |  |  |
| v ${ }_{\text {R }}$ |  |  | 182 | 2000 | No |
|  |  |  |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$

| Density, | $\mathrm{D}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L}$ | $=0.7 \mathrm{D}$ | $\mathrm{pc} / \mathrm{km} / \mathrm{ln}$ |
| ---: | :--- | ---: | :--- |
| Level of service for ramp-freeway junction areas of influence A |  |  |  |

Speed Estimation $\qquad$


## Phone:

Fax:
E-mail:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 579 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$170 \quad$ vph
300 m
m

Adjacent Ramp Data (if one exists) $\qquad$
Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
m

$\qquad$


Capacity Checks $\qquad$


Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$


## Phone:

Fax:
E-mail:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 609 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$179 \quad$ vph
300 m
m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
m

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 744 | 4600 | No |
| Fi F |  |  |  |
| v | 744 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 543 | 4600 | No |
| FO F R |  |  |  |
| V | 201 | 2000 | No |
| R |  |  |  |



```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | Katie Hazzard |
| :---: | :---: |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | Eastbond |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Cross | ng |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on freeway | 100.0 | 2587 |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 646 | vph |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 3887 | 4600 | No |
| FO | 3887 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=18.3 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 2774 |


|  | Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 692 | m |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 4167 | 4600 | No |
| V | 4167 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=19.6 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation $\qquad$


```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2916 | vph |


|  | Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 728 | m |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 4381 | 4600 | No |
| FO | 4381 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=20.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3498 | vph |


|  | Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 782 | m |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$
v
Actual
5153
5153
Maximum
4600
4600

LOS F?
Yes
FO
v
5153
4600
Yes
R12
Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=24.3 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $F$
Speed Estimation

$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2464 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$583 \quad \mathrm{vph}$
300 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3012 | 4600 | No |
| Fi F |  |  |  |
| v | 3012 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2358 | 4600 | No |
| FO F R |  |  |  |
| v | 654 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\quad \mathrm{D}_{\mathrm{R}}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L} \quad=13.1 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$

Level of service for ramp-freeway junction areas of influence $C$

Speed Estimation $\qquad$

$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2642 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$625 \quad \mathrm{vph}$
300 m
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  | m |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3229 | 4600 | No |
| Fi F |  |  |  |
| v | 3229 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2528 | 4600 | No |
| FO F R |  |  |  |
| v | 701 | 2000 | No |
| R |  |  |  |


$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2776 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$657 \quad \mathrm{vph}$
300 m
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  | m |


$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3393 | 4600 | No |
| Fi F |  |  |  |
| v | 3393 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2656 | 4600 | No |
| FO F R |  |  |  |
| v | 737 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\quad \mathrm{D}_{\mathrm{R}}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L} \quad=15.1 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$

Level of service for ramp-freeway junction areas of influence C

Speed Estimation
Intermediate speed variable,
Space mean speed in ramp influence area,
Space mean speed in outer lanes,
Space mean speed for all vehicles,

| $D$ | $=0.469$ |  |
| :--- | :--- | :--- |
| $S$ |  |  |
| $S$ | $=84.5$ | $\mathrm{~km} / \mathrm{h}$ |
| $R$ |  |  |
| $S$ | $=\mathrm{N} / \mathrm{A}$ | $\mathrm{km} / \mathrm{h}$ |
| 0 |  |  |
| $S$ | $=84.5$ | $\mathrm{~km} / \mathrm{h}$ |

$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2919 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Length of first accel/decel lane
Length of second accel/decel lane
$690 \quad \mathrm{vph}$
300 m
Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
m
m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3568 | 4600 | No |
| Fi F |  |  |  |
| v | 3568 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2794 | 4600 | No |
| FO F R |  |  |  |
| v | 774 | 2000 | No |
| R |  |  |  |



```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 839 |

On Ramp Data

Side of freeway
Number of lanes in ramp
Free-flow speed on ramp
Volume on ramp 291
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$291 \quad v p h$
280 m
m

Adjacent Ramp Data (if one exists) $\qquad$

Does adjacent ramp exist?
Volume on adjacent Ramp
No

Position of adjacent Ramp
Type of adjacent Ramp
Distance to adjacent Ramp
m

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :--- | :--- | :--- |
| V FO | 1352 | 4600 | No |
| V 12 | 1352 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=6.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 899 |

On Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$312 \quad v p h$
280 m
m

Adjacent Ramp Data (if one exists) $\qquad$

Does adjacent ramp exist?
Volume on adjacent Ramp
No

Position of adjacent Ramp
Type of adjacent Ramp
Distance to adjacent Ramp
m

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 1449 | 4600 | No |
| FO | 1449 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=6.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation


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Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 945 | vph |


|  | Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 328 | m |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 1523 | 4600 | No |
| FO | 1523 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=7.0 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 993 |


|  | Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 344 | m |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 1600 | 4600 | No |
| FO | 1600 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=7.4 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation

$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 691 |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$234 \quad \mathrm{vph}$
230 m
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  | m |


$\qquad$


Capacity Checks $\qquad$

| $\mathrm{V}_{\mathrm{Fi}}=\mathrm{v}$ |  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 845 | 4600 | No |
|  |  |  |  |  |
| v 12 |  | 845 | 4400 | No |
|  |  |  |  |  |
| $\begin{aligned} & \mathrm{V}=\mathrm{V}-\mathrm{V} \\ & \mathrm{FO} \quad \mathrm{~F} \quad \mathrm{R} \end{aligned}$ |  | 582 | 4600 | No |
|  |  |  |  |  |
|  |  | 263 | 2000 | No |
| ${ }^{\mathrm{v}} \mathrm{R}$ |  |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

| Intermediate speed variable, | $\mathrm{D}_{\mathrm{S}}=0.427$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=85.9$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=85.9$ | km/h |

$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 741 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$251 \quad \mathrm{vph}$
230 m
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  | m |


$\qquad$


Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 779 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
$264 \quad v p h$
230 m
Right
1
1
$60.0 \mathrm{~km} / \mathrm{h}$
m

Length of first accel/decel lane
Length of second accel/decel lane
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  | m |


$\qquad$


Capacity Checks $\qquad$

| $\mathrm{V}_{\mathrm{Fi}}=\mathrm{v}$ |  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 952 | 4600 | No |
|  |  |  |  |  |
| v 12 |  | 952 | 4400 | No |
|  |  |  |  |  |
| $\begin{aligned} & \mathrm{v}=\mathrm{v}-\mathrm{v} \\ & \mathrm{FO} \quad \mathrm{~F} \quad \mathrm{R} \end{aligned}$ |  | 656 | 4600 | No |
|  |  |  |  |  |
|  |  | 296 | 2000 | No |
| ${ }_{\mathrm{V}}^{\mathrm{R}}$ |  |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 819 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$277 \quad$ vph
230 m

Adjacent Ramp Data (if one exists) $\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 1001 | 4600 | No |
| Fi F |  |  |  |
| v | 1001 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 690 | 4600 | No |
| FO F R |  |  |  |
| v | 311 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$


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Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 451 |


|  | Ramp |  |
| :--- | :---: | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 345 | m |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 938 | 4600 | No |
| FO |  |  |  |
| V12 | 938 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=4.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $A$
Speed Estimation


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Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 483 |


|  | Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 370 | m |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 1005 | 4600 | No |
| FO | 1005 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=4.5 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $A$
Speed Estimation


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Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 508 |

On Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-flow speed on ramp
Volume on ramp 389
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$389 \quad v p h$
280 m
m
$\qquad$
Does adjacent ramp exist?
Volume on adjacent Ramp
No

Position of adjacent Ramp
Type of adjacent Ramp
Distance to adjacent Ramp
m

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 1058 | 4600 | No |
| FO | 1058 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=4.8 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $A$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | WB |
| Junction: | Rte 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 534 |

On Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-flow speed on ramp
Volume on ramp 409
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$409 \quad$ vph
280 m
m

Adjacent Ramp Data (if one exists) $\qquad$
Does adjacent ramp exist?
Volume on adjacent Ramp
No

Position of adjacent Ramp
Type of adjacent Ramp
Distance to adjacent Ramp
m

$\qquad$


Capacity Checks $\qquad$
v
Actual
Maximum
LOS F? 4600

No
FO
v
1112
4600
No
R12
Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=5.1 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence A
Speed Estimation

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 17 / 2017$ |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2587 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$769 \quad$ vph
240 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3162 | 4600 | No |
| Fi F |  |  |  |
| v | 3162 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2299 | 4600 | No |
| FO F R |  |  |  |
| v | 863 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$

| Density, | $\mathrm{D}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L} \quad=\quad 15.0 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ |
| ---: | :--- |
| Level of service for ramp-freeway junction areas of influence | $C$ |

Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 17 / 2017$ |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2774 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$824 \quad \mathrm{vph}$
240 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3390 | 4600 | No |
| Fi F |  |  |  |
| v | 3390 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2465 | 4600 | No |
| FO F R |  |  |  |
| v | 925 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\quad \mathrm{D}_{\mathrm{R}}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L} \quad=16.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$

Level of service for ramp-freeway junction areas of influence $C$

Speed Estimation

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 17 / 2017$ |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2916 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$866 \quad v p h$
240 m
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  | m |


$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3564 | 4600 | No |
| Fi F |  |  |  |
| v | 3564 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2592 | 4600 | No |
| FO F R |  |  |  |
| v | 972 | 2000 | No |
| R |  |  |  |




Speed Estimation

| Intermediate speed variable, | $\mathrm{D}_{\mathrm{S}}=0.490$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=83.8$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=83.8$ | km/h |

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 17 / 2017$ |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3065 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$910 \quad \mathrm{vph}$
240 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3746 | 4600 | No |
| Fi F |  |  |  |
| v | 3746 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2725 | 4600 | No |
| FO F R |  |  |  |
| v | 1021 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$


```
Phone:
Fax:
```

E-mail:

Merge Analysis

|  |  |
| :--- | :--- |
| Analyst: | KEH |
| Agency/Co.: Analysis____ | exp |
| Date performed: | $1 / 17 / 2017$ |
| Analysis time period: | AM |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 514 |

On Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
217 vph
150 m
m

Adjacent Ramp Data (if one exists) $\qquad$
Does adjacent ramp exist?
Volume on adjacent Ramp
No

Position of adjacent Ramp
Type of adjacent Ramp
Distance to adjacent Ramp
m

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 872 | 4600 | No |
| FO | 872 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=5.6 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $A$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis

|  |  |
| :--- | :--- |
| Analyst: | KEH |
| Agency/Co.: | exp Analysis____ |
| Date performed: | $1 / 17 / 2017$ |
| Analysis time period: | AM |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 551 |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 233 | vph |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 934 | 4600 | No |
| FO | 934 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=5.9 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $A$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | AM |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 579 |


|  | Ren Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 245 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 983 | 4600 | No |
| FO | 983 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=6.1 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | AM |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 609 |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 257 | vph |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$
v
Actual

Maximum
LOS F? 4600

No

1032
4600
No
v
R12

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=6.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 839 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Length of first accel/decel lane
Length of second accel/decel lane
258 vph

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$258 \quad \mathrm{vph}$
240 m

Adjacent Ramp Data (if one exists) $\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
m

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 1025 | 4600 | No |
| Fi F |  |  |  |
| v | 1025 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 735 | 4600 | No |
| FO F R |  |  |  |
| v | 290 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route lo0 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 899 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$

277 vph
240 m

Adjacent Ramp Data (if one exists) $\qquad$
Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
m

$\qquad$


|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 1099 | 4600 | No |
| Fi F |  |  |  |
| v | 1099 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 788 | 4600 | No |
| FO F R |  |  |  |
| v | 311 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 945 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$291 \quad \mathrm{vph}$
240 m
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  | m |


$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 1155 | 4600 | No |
| Fi F |  |  |  |
| v | 1155 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 828 | 4600 | No |
| FO F R |  |  |  |
| v | 327 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 993 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$306 \quad$ vph
240 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 1214 | 4600 | No |
| Fi F |  |  |  |
| v | 1214 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 871 | 4600 | No |
| FO F R |  |  |  |
| v | 343 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$


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Phone:
Fax:
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E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Evening Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on freeway | 100.0 | 2464 |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 709 | vph |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 3808 | 4600 | No |
| FO | 3808 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=19.6 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


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Phone:
Fax:
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E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Evening Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on freeway | 100.0 | 2642 |


|  | Ramp |  |
| :--- | :---: | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 760 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 4082 | 4600 | No |
| V | 4082 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=20.9 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Evening Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2776 | vph |


| Side of freeway | Ramp |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | Right |  |
| Free-flow speed on ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 60.0 | vph |
| Length of first accel/decel lane | 799 | m |
| Length of second accel/decel lane | 150 | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 4290 | 4600 | No |
| FO | 4290 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=21.9 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Evening Peak |
| Freeway/Dir of Travel: | Westbond |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on freeway | 100.0 | 2919 |


|  | Rata__On Ramp |  |
| :--- | :---: | :---: |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 839 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 4510 | 4600 | No |
| FO | 4510 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=22.9 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $E$
Speed Estimation

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 451 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
733 vph
240 m

Adjacent Ramp Data (if one exists) $\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 551 | 4600 | No |
| Fi F |  |  |  |
| v | 551 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | -272 | 4600 | No |
| FO F R |  |  |  |
| v | 823 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 483 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$786 \quad \mathrm{vph}$
240 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 590 | 4600 | No |
| Fi F |  |  |  |
| v | 590 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | -292 | 4600 | No |
| FO F R |  |  |  |
| v | 882 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 508 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$826 \quad \mathrm{vph}$
240 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks $\qquad$


Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 534 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$868 \quad \mathrm{vph}$
240 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 653 | 4600 | No |
| Fi F |  |  |  |
| v | 653 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | -321 | 4600 | No |
| FO F R |  |  |  |
| v | 974 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$


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Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | K Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 691 |


|  | Rata__On Ramp |  |
| :--- | :---: | :---: |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 756 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 1693 | 4600 | No |
| FO |  |  |  |
| R12 | 1693 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=9.4 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 741 |


| Side of freeway | Ramp |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | Right |  |
| Free-flow speed on ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 60.0 | vph |
| Length of first accel/decel lane | 811 | m |
| Length of second accel/decel lane | 150 | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |



| 0.909 | 0.990 |
| :--- | :--- |
| 1.00 | 1.00 |
| 906 | 910 |

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 1816 | 4600 | No |
| V |  |  |  |
| R12 | 1816 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=10.0 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation $\qquad$

| Intermediate speed variable, | $\mathrm{M}_{\mathrm{S}}=0.309$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=89.8$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles | $\mathrm{S}=89.8$ | km/h |

```
Phone:
Fax:
```

E-mail:

Merge Analysis

|  |  |
| :--- | :--- |
| Analyst: | KEH |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Sat |
| Freeway/Dir of Travel:_ | Westbond |
| Junction: | Route loo On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2028 |
| Description: The Crossing |  |


| Type of analysis | Merge |  |
| :---: | :---: | :---: |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | km/h |
| Volume on freeway | 779 | vph |
| On Ramp Data |  |  |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 852 | vph |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 1908 | 4600 | No |
| FO | 1908 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=10.4 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation


```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Sat |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | 819 |


|  | Ramp |  |
| :--- | :---: | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 895 | m |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$
v
Actual 2005

2005
v
R12

| Maximum | LOS F? |
| :--- | :--- |
| 4600 | No |
| 4600 | No |

Level of Service Determination (if not F) $\qquad$

Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=10.9 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $B$
Speed Estimation $\qquad$


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 15.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | \& |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 0 | 15 | 3 | 8 | 0 | 129 | 759 | 19 | 2 | 10 | 113 | 1 |
| Future Vol, veh/h | 0 | 15 | 3 | 8 | 0 | 129 | 759 | 19 | 2 | 10 | 113 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 16 | 3 | 9 | 0 | 140 | 825 | 21 | 2 | 11 | 123 | 1 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | $\ddagger$ |  |  | * |  |  | \& |  |
| Traffic Vol, veh/h | 1 | 2 | 5 | 1 | 0 | 98 | 210 | 13 | 2 | 1 | 159 | 3 |
| Future Vol, veh/h | 1 | 2 | 5 | 1 | 0 | 98 | 210 | 13 | 2 | 1 | 159 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 2 | 5 | 1 | 0 | 107 | 228 | 14 | 2 | 1 | 173 | 3 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | $\uparrow$ | 「 |  | * |  |  | * |  |
| Traffic Vol, veh/h | 0 | 15 | 3 | 8 | 0 | 129 | 759 | 19 | 2 | 10 | 113 | 1 |
| Future Vol, veh/h | 0 | 15 | 3 | 8 | 0 | 129 | 759 | 19 | 2 | 10 | 113 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | 750 | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 16 | 3 | 9 | 0 | 140 | 825 | 21 | 2 | 11 | 123 | 1 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | $\uparrow$ | 「 |  | * |  |  | \& |  |
| Traffic Vol, veh/h | 1 | 2 | 5 | 1 | 0 | 98 | 210 | 13 | 2 | 1 | 159 | 3 |
| Future Vol, veh/h | 1 | 2 | 5 | 1 | 0 | 98 | 210 | 13 | 2 | 1 | 159 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | 750 | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 2 | 5 | 1 | 0 | 107 | 228 | 14 | 2 | 1 | 173 | 3 |


| Major/Minor | Minor1 |  | Minor2 |  |  | Major1 |  |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 649 | 650 | 15 | 653 | 650 | 174 |  | 176 | 0 | 0 | 16 | 0 | 0 |
| Stage 1 | 472 | 472 | - | 177 | 177 | - |  | - | - | - | - | - |  |
| Stage 2 | 177 | 178 | - | 476 | 473 | - |  | - | - | - | - | - |  |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 | - |  | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 | - |  | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 383 | 388 | 1065 | 380 | 388 | 869 |  | 1400 | - | - | 1602 | - |  |
| Stage 1 | 573 | 559 | - | 825 | 753 | - |  | - | - | - | - | - |  |
| Stage 2 | 825 | 752 | - | 570 | 558 | - |  | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 294 | 324 | 1065 | 329 | 324 | 869 |  | 1400 | - | - | 1602 | - |  |
| Mov Cap-2 Maneuver | 294 | 324 | - | 329 | 324 | - |  | - | - | - | - | - | - |
| Stage 1 | 479 | 467 | - | 690 | 752 | - |  | - | - | - | - | - | - |
| Stage 2 | 723 | 751 | - | 472 | 466 | - |  | - | - | - | - | - | - |
| Approach | NB |  |  | SB |  |  |  | SE |  |  | NW |  |  |
| HCM Control Delay, s | 11.5 |  |  | 9.8 |  |  |  | 7.5 |  |  | 0 |  |  |
| HCM LOS | B |  |  | A |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | NWL | NWT | SEL | SET | SER | BLn1 | SBLn2 |  |  |  |  |  |
| Capacity (veh/h) | 561 | 1602 | - | 1400 | - | - | 329 | 869 |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.016 | 0.001 | - | 0.163 | - | - | 0.003 | 0.123 |  |  |  |  |  |
| HCM Control Delay (s) | 11.5 | 7.2 | 0 | 8.1 | 0 | - | 16 | 9.7 |  |  |  |  |  |
| HCM Lane LOS | B | A | A | A | A | - | C | A |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | 0 | - | 0.6 | - | - | 0 | 0.4 |  |  |  |  |  |

## Phone:

Fax:
E-mail:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2672 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp 785
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$785 \quad$ vph
130 m
m

Adjacent Ramp Data (if one exists) $\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
m

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3266 | 4600 | No |
| Fi F |  |  |  |
| v | 3266 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2385 | 4600 | No |
| FO F R |  |  |  |
| v | 881 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$


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Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbond |
| Junction: | Foster Thurston On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |


|  | Freeway |  |
| :--- | :--- | :--- |
| Type of analysis |  |  |
| Number of lanes in freeway | Merge |  |
| Free-flow speed on freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 100.0 | vph |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 27 | vph |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :--- | :--- | :--- |
| V FO | 3296 | 4600 | No |
| V 12 | 3296 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=17.7 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


## Phone:

Fax:
E-mail:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Evening Peak |
| Freeway/Dir of Travel: | Eastbound |
| Junction: | Ashburn Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing Study |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3124 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp 298
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$298 \quad v p h$
180 m
m
$\qquad$
Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3818 | 4500 | No |
| Fi F |  |  |  |
| v | 3818 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 3484 | 4500 | No |
| FO F R |  |  |  |
| v | 334 | 2000 | No |
| R |  |  |  |




Speed Estimation $\qquad$


```
Phone:
Fax:
```

E-mail:

Merge Analysis

|  |  |
| :--- | :--- |
| Analyst: | Matie Hazzard Analysis___ |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | Evening Peak |
| Freeway/Dir of Travel: | Eastbond |
| Junction: | Ashburn On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on freeway | 100.0 | 3124 |


| Side of freeway | Ramp |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | Right |  |
| Free-flow speed on ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 60.0 | vph |
| Length of first accel/decel lane | 471 | m |
| Length of second accel/decel lane | 150 | m |

Does adjacent ramp exist?
Volume on adjacent Ramp
Position of adjacent Ramp
Type of adjacent Ramp
Distance to adjacent Ramp

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 4347 | 4600 | No |
| FO | 4347 | 4600 | No |
| R12 |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=22.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $E$
Speed Estimation


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | \& |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 7 | 0 | 117 | 5 | 0 | 5 | 131 | 869 | 4 | 4 | 793 | 3 |
| Future Vol, veh/h | 7 | 0 | 117 | 5 | 0 | 5 | 131 | 869 | 4 | 4 | 793 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 8 | 0 | 127 | 5 | 0 | 5 | 142 | 945 | 4 | 4 | 862 | 3 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | * |  |  | * |  |  | \& |  |
| Traffic Vol, veh/h | 7 | 0 | 124 | 2 | 0 | 2 | 135 | 300 | 1 | 2 | 399 | 6 |
| Future Vol, veh/h | 7 | 0 | 124 | 2 | 0 | 2 | 135 | 300 | 1 | 2 | 399 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 8 | 0 | 135 | 2 | 0 | 2 | 147 | 326 | 1 | 2 | 434 | 7 |



|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection  <br> Int Delay, s/veh 1.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\hat{}$ |  |  | \$ |  |  | $\hat{1}$ |  |  | ¢ |  |  |
| Traffic Vol, veh/h | 0 | 0 | 117 | 5 | 0 | 5 | 0 | 1000 | 4 | 4 | 793 | 3 |
| Future Vol, veh/h | 0 | 0 | 117 | 5 | 0 | 5 | 0 | 1000 | 4 | 4 | 793 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - |  | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 127 | 5 | 0 | 5 | 0 | 1087 | 4 | 4 | 862 | 3 |


| Major/Minor | Minor2 |  | Minor1 |  |  |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 1963 | 864 |  | 2025 | 1963 | 1089 | - | 0 | 0 | 1091 | 0 | 0 |
| Stage 1 | - | 872 | - |  | 1089 | 1089 |  | - | - | - | - | - |  |
| Stage 2 | - | 1091 |  |  | 936 | 874 | - | - | - |  |  | - |  |
| Critical Hdwy | - | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 | - | - |  | 4.12 | - |  |
| Critical Hdwy Stg 1 | - | 5.52 | - |  | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | 5.52 | - |  | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Follow-up Hdwy | - | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 | - | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 0 | 63 | 354 |  | 43 | 63 | 262 | 0 | - | - | 640 | - |  |
| Stage 1 | 0 | 368 | - |  | 261 | 291 | - | 0 | - | - | - | - |  |
| Stage 2 | 0 | 291 | - |  | 318 | 367 | - | 0 | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | - | 62 | 354 |  | 27 | 62 | 262 | - | - | - | 640 | - |  |
| Mov Cap-2 Maneuver | - | 62 | - |  | 27 | 62 | - | - | - | - | - | - |  |
| Stage 1 | - | 364 | - |  | 261 | 291 | - | - | - | - | - | - |  |
| Stage 2 | - | 291 |  |  | 201 | 363 | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 20.8 |  |  |  | 98.3 |  |  | 0 |  |  | 0.1 |  |  |
| HCM LOS | C |  |  |  | F |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBT | NBR | EBLn1 | VBLn1 | SBL | SBT | SBR |  |  |  |  |  |  |
| Capacity (veh/h) | - | - | 354 | 49 | 640 | - |  |  |  |  |  |  |  |
| HCM Lane V/C Ratio | - | - | 0.359 | 0.222 | 0.007 | - |  |  |  |  |  |  |  |
| HCM Control Delay (s) | - | - | 20.8 | 98.3 | 10.7 | 0 |  |  |  |  |  |  |  |
| HCM Lane LOS | - | - | C | F | B | A |  |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | - | - | 1.6 | 0.7 | 0 | - | - |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\hat{\beta}$ |  |  | ¢ |  |  | $\hat{\dagger}$ |  |  | $\dagger$ |  |  |
| Traffic Vol, veh/h | 0 | 0 | 124 | 5 | 0 | 5 | 0 | 435 | 1 | 2 | 399 | 6 |
| Future Vol, veh/h | 0 | 0 | 124 | 5 | 0 | 5 | 0 | 435 | 1 | 2 | 399 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - |  | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 135 | 5 | 0 | 5 | 0 | 473 | 1 | 2 | 434 | 7 |


| Major/Minor | Minor2 |  | Minor1 |  |  |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 915 | 437 |  | 982 | 918 | 473 | - | 0 | 0 | 474 | 0 | 0 |
| Stage 1 | - | 441 | - |  | 473 | 473 | - | - | - | - | - | - |  |
| Stage 2 | - | 474 | - |  | 509 | 445 | - | - | - |  |  | - |  |
| Critical Hdwy | - | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 | - | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | - | 5.52 | - |  | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | 5.52 | - |  | 6.12 | 5.52 | - | - | - | - |  | - |  |
| Follow-up Hdwy | - | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 | - | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 0 | 273 | 620 |  | 228 | 272 | 591 | 0 | - | - | 1088 | - |  |
| Stage 1 | 0 | 577 | - |  | 572 | 558 | - | 0 | - | - | - | - |  |
| Stage 2 | 0 | 558 | - |  | 547 | 575 | - | 0 | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | - | 272 | 620 |  | 178 | 271 | 591 | - | - | - | 1088 | - |  |
| Mov Cap-2 Maneuver | - | 272 | - |  | 178 | 271 | - | - | - | - | - | - |  |
| Stage 1 | - | 576 | - |  | 572 | 558 | - | - | - | - | - | - |  |
| Stage 2 | - | 558 | - |  | 427 | 574 | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 12.4 |  |  |  | 18.7 |  |  | 0 |  |  | 0 |  |  |
| HCM LOS | B |  |  |  | C |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBT | NBR | EBLn1 | BLn1 | SBL | SBT | SBR |  |  |  |  |  |  |
| Capacity (veh/h) | - | - | 620 | 274 | 1088 | - | - |  |  |  |  |  |  |
| HCM Lane V/C Ratio | - | - | 0.217 | 0.04 | 0.002 | - | - |  |  |  |  |  |  |
| HCM Control Delay (s) | - | - | 12.4 | 18.7 | 8.3 | 0 | - |  |  |  |  |  |  |
| HCM Lane LOS | - | - | B | C | A | A | - |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | - | - | 0.8 | 0.1 | 0 | - | - |  |  |  |  |  |  |


|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay, s/veh }} 0.2$ |  |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations |  | $\uparrow$ | $\hat{\beta}$ |  | M |  |
| Traffic Vol, veh/h | 5 | 737 | 168 | 1 | 3 | 1 |
| Future Vol, veh/h | 5 | 737 | 168 | 1 | 3 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 801 | 183 | 1 | 3 | 1 |



| Intersection |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.6 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | * |  |
| Traffic Vol, veh/h | 2 | 700 | 182 | 20 | 28 | 0 |
| Future Vol, veh/h | 2 | 700 | 182 | 20 | 28 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 761 | 198 | 22 | 30 | 0 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\hat{\dagger}$ |  | M |  |
| Traffic Vol, veh/h | 0 | 292 | 152 | 16 | 12 | 3 |
| Future Vol, veh/h | 0 | 292 | 152 | 16 | 12 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 0 | 317 | 165 | 17 | 13 | 3 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ¢ |  |  | $\dagger$ |  |  | ¢ |  |  | ${ }^{7}$ | $\hat{\dagger}$ |  |
| Traffic Vol, veh/h | 3 | 242 | 149 | 93 | 188 | 481 | 321 | 548 | 77 | 552 | 231 | 1 |
| Future Vol, veh/h | 3 | 242 | 149 | 93 | 188 | 481 | 321 | 548 | 77 | 552 | 231 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | Stop | - | - | Free | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - |  | 500 | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - |  | 0 |  |  | 0 |  |
| Grade, \% | - | 0 |  | - | 0 | - |  | 0 |  |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 263 | 162 | 101 | 204 | 523 | 349 | 596 | 84 | 600 | 251 | 1 |


| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2848 | 2745 | 252 | 2957 | 2745 | 596 | 252 | 0 | - | 596 | 0 | 0 |
| Stage 1 | 1452 | 1452 | - | 1293 | 1293 |  | - | - | - | - | - |  |
| Stage 2 | 1396 | 1293 | - | 1664 | 1452 |  |  | - | - |  | - |  |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 |  | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 |  | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 11 | ~20 | 787 | ~9 | $\sim 20$ | $\sim 504$ | 1313 | - | 0 | 980 | - |  |
| Stage 1 | 162 | ~195 | - | 200 | 233 |  | - | - | 0 | - | - |  |
| Stage 2 | 175 | $\sim 233$ | - | 122 | $\sim 195$ |  | - | - | 0 | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  | - |  |  | - |  |
| Mov Cap-1 Maneuver | - | $\sim 5$ | 787 | - | $\sim 5$ | $\sim 504$ | 1313 | - | - | 980 | - |  |
| Mov Cap-2 Maneuver | - | $\sim 5$ | - | - | $\sim 5$ |  | - | - | - | - | - |  |
| Stage 1 | 98 |  | - | 121 |  |  | - | - | - | - | - |  |
| Stage 2 | $\sim 2$ | $\sim 140$ | - | - | $\sim 76$ |  | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s |  |  |  |  |  |  | 3.2 |  |  | 10.1 |  |  |
| HCM LOS | - |  |  | - |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | 1 SBL | SBT | SBR |  |  |  |  |  |  |
| Capacity (veh/h) | 1313 | - | - | 980 |  |  |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.266 | - | - | - 0.612 | - |  |  |  |  |  |  |  |
| HCM Control Delay (s) | 8.7 | 0 | - | - 14.3 | - |  |  |  |  |  |  |  |
| HCM Lane LOS | A | A | - | B | - |  |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 1.1 | - | - | 4.3 | - | - |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds capa | \$: De | lay exc | eeds 3 | +: Comp | utation | Not D | *: All |  | e in |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | $\uparrow$ |  |  | \& |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 5 | 447 | 133 | 244 | 301 | 274 | 300 | 146 | 90 | 417 | 125 | 3 |
| Future Vol, veh/h | 5 | 447 | 133 | 244 | 301 | 274 | 300 | 146 | 90 | 417 | 125 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | Stop | - | - | Free | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | 500 | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 486 | 145 | 265 | 327 | 298 | 326 | 159 | 98 | 453 | 136 | 3 |


| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2018 | 1855 | 138 | 2170 | 1857 | 159 | 139 | 0 | - | 159 | 0 | 0 |
| Stage 1 | 1044 | 1044 | - | 811 | 811 | - | - | - |  | - | - |  |
| Stage 2 | 974 | 811 | - | 1359 | 1046 | - | - | - |  |  | - |  |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - |  | 4.12 | - |  |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.12 | 5.52 |  | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 43 | $\sim 74$ | 910 | ~34 | ~74 | 886 | 1445 | - | 0 | 1420 | - |  |
| Stage 1 | 277 | ~306 | - | 373 | 393 | - | - | - | 0 | - | - |  |
| Stage 2 | 303 | $\sim 393$ | - | $\sim 183$ | $\sim 305$ | - | - | - | 0 | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  | - |  |  | - |  |
| Mov Cap-1 Maneuver | - | ~38 | 910 | - | ~ 38 | 886 | 1445 | - | - | 1420 | - |  |
| Mov Cap-2 Maneuver | - | ~ 38 | - | - | ~38 | - | - | - | - | - | - |  |
| Stage 1 | 209 |  | - | 281 | $\sim 296$ | - | - | - | - | - | - |  |
| Stage 2 | - | $\sim 296$ | - | - | $\sim 208$ | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s |  |  |  |  |  |  | 5.5 |  |  | 6.7 |  |  |
| HCM LOS | - |  |  | - |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | 1 SBL | SBT | SBR |  |  |  |  |  |  |
| Capacity (veh/h) | 1445 | - | - | - 1420 |  |  |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.226 | - | - | - 0.319 |  |  |  |  |  |  |  |  |
| HCM Control Delay (s) | 8.2 | 0 | - | - 8.7 | - |  |  |  |  |  |  |  |
| HCM Lane LOS | A | A | - | - A | - | - |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0.9 | - | - | 1.4 | - | - |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds cap | \$: D | lay exc | ceds 3 | +: Com | putatio | Not D | *: All | or v |  |  |  |  |

## SITE LAYOUT

$\theta$ Site: 101 [Crossing 2023 PM (Single Lane)]
Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Single Lane Option
Roundabout


## INPUT VOLUMES

## Vehicles and pedestrians per 60 minutes

Site: 101 [Crossing 2023 PM (Single Lane)]
Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Single Lane Option
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: Rte 1 Ramps | 946 | 927 | 19 |
| E: Rothesay Ave WB | 667 | 654 | 13 |
| N: Rothesay Rd SB | 784 | 768 | 16 |
| W: Crossing Access EB | 394 | 386 | 8 |
| Total | 2791 | 2735 | 56 |

## LANE SUMMARY

## Site: 101 [Crossing 2023 PM (Single Lane)]

Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Single Lane Option
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand F Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \text { Bac } \\ \text { Veh } \end{gathered}$ | Queue Dist m | Lane Config | Lane Length m | Cap. Adj. <br> \% | Prob. Block. \% |
| South: Rte 1 Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 996 | 2.0 | 443 | 2.247 | 100 | 585.6 | LOS F | 193.8 | 1379.9 | Full | 500 | 0.0 | 67.7 |
| Approach | 996 | 2.0 |  | 2.247 |  | 585.6 | LOS F | 193.8 | 1379.9 |  |  |  |  |
| East: Rothesay Ave WB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 702 | 2.0 | 699 | 1.005 | 100 | 42.0 | LOS D | 29.6 | 210.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 702 | 2.0 |  | 1.005 |  | 42.0 | LOS D | 29.6 | 210.8 |  |  |  |  |
| North: Rothesay Rd SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 825 | 2.0 | 810 | 1.018 | 100 | 47.4 | LOS D | 35.4 | 252.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 825 | 2.0 |  | 1.018 |  | 47.4 | LOS D | 35.4 | 252.0 |  |  |  |  |
| West: Crossing Access EB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 415 | 2.0 | 340 | 1.221 | 100 | 140.9 | LOS F | 38.4 | 273.2 | Full | 500 | 0.0 | 0.0 |
| Approach | 415 | 2.0 |  | 1.221 |  | 140.9 | LOS F | 38.4 | 273.2 |  |  |  |  |
| Intersection | 2938 | 2.0 |  | 2.247 |  | 241.7 | LOS F | 193.8 | 1379.9 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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## INPUT VOLUMES

## Vehicles and pedestrians per 60 minutes

$\theta$ Site: 101 [Crossing 2023 Sat (Single Lane)]
Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Single Lane Option
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: Rte 1 Ramps | 536 | 525 | 11 |
| E: Rothesay Ave WB | 819 | 803 | 16 |
| N: Rothesay Rd SB | 545 | 534 | 11 |
| W: Crossing Access EB | 585 | 573 | 12 |
| Total | 2485 | 2435 | 50 |

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## LANE SUMMARY

## Site: 101 [Crossing 2023 Sat (Single Lane)]

Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Single Lane Option
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Bac Veh | Queue Dist m | Lane Config | Lane Length m | Cap. <br> Adj. <br> \% | Prob. Block. \% |
| South: Rte 1 Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 564 | 2.0 | 491 | 1.149 | 100 | 108.8 | LOS F | 41.0 | 292.2 | Full | 500 | 0.0 | 0.0 |
| Approach | 564 | 2.0 |  | 1.149 |  | 108.8 | LOS F | 41.0 | 292.2 |  |  |  |  |
| East: Rothesay Ave WB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 862 | 2.0 | 717 | 1.202 | 100 | 113.1 | LOS F | 67.5 | 480.5 | Full | 500 | 0.0 | 3.8 |
| Approach | 862 | 2.0 |  | 1.202 |  | 113.1 | LOS F | 67.5 | 480.5 |  |  |  |  |
| North: Rothesay Rd SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 574 | 2.0 | 479 | 1.197 | 100 | 127.8 | LOS F | 46.8 | 333.5 | Full | 500 | 0.0 | 0.0 |
| Approach | 574 | 2.0 |  | 1.197 |  | 127.8 | LOS F | 46.8 | 333.5 |  |  |  |  |
| West: Crossing Access EB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 616 | 2.0 | 511 | 1.205 | 100 | 123.0 | LOS F | 50.5 | 359.9 | Full | 500 | 0.0 | 0.0 |
| Approach | 616 | 2.0 |  | 1.205 |  | 123.0 | LOS F | 50.5 | 359.9 |  |  |  |  |
| Intersection | 2616 | 2.0 |  | 1.205 |  | 117.7 | LOS F | 67.5 | 480.5 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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## SITE LAYOUT

© Site: 101 [Crossing 2023 PM (Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Multi-Lane Option
Roundabout


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\Crossing_2023wDevelopment.sip7

## INPUT VOLUMES

## Vehicles and pedestrians per 60 minutes

© 9 Site: 101 [Crossing 2023 PM (Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Multi-Lane Option
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: Rte 1 Ramps | 946 | 927 | 19 |
| E: Rothesay Ave WB | 667 | 654 | 13 |
| N: Rothesay Rd SB | 784 | 768 | 16 |
| W: Crossing Access EB | 394 | 386 | 8 |
| Total | 2791 | 2735 | 56 |

## LANE SUMMARY

## Site: 101 [Crossing 2023 PM (Multi-Lane)]

Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Multi-Lane Option
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back Veh | $\begin{gathered} \text { Queue } \\ \text { Dist } \\ \mathrm{m} \end{gathered}$ | Lane Config | Lane Length m | Cap. <br> Adj. \% | Prob. Block. \% |
| South: Rte 1 Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 551 | 2.0 | 540 | 1.020 | 100 | 66.6 | LOS E | 27.3 | 194.7 | Short | 60 | 0.0 | NA |
| Lane 2 | 445 | 2.0 | 480 | 0.927 | $91^{6}$ | 45.4 | LOS D | 16.8 | 119.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 996 | 2.0 |  | 1.020 |  | 57.1 | LOS E | 27.3 | 194.7 |  |  |  |  |
| East: Rothesay Ave WB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 196 | 2.0 | 558 | 0.351 | 100 | 10.4 | LOS B | 1.8 | 12.8 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 506 | 2.0 | 718 | 0.705 | 100 | 10.0 | LOS B | 6.0 | 42.5 | Short | 60 | 0.0 | NA |
| Approach | 702 | 2.0 |  | 0.705 |  | 10.1 | LOS B | 6.0 | 42.5 |  |  |  |  |
| North: Rothesay Rd SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 581 | 2.0 | 782 | 0.743 | 100 | 20.8 | LOS C | 9.4 | 67.2 | Short | 60 | 0.0 | NA |
| Lane 2 | 244 | 2.0 | 570 | 0.429 | $58^{5}$ | 12.4 | LOS B | 2.8 | 20.2 | Full | 500 | 0.0 | 0.0 |
| Approach | 825 | 2.0 |  | 0.743 |  | 18.3 | LOS B | 9.4 | 67.2 |  |  |  |  |
| West: Crossing Access EB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 258 | 2.0 | 561 | 0.460 | 100 | 9.7 | LOS A | 2.7 | 19.2 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 157 | 2.0 | 885 | 0.177 | 100 | 5.4 | LOS A | 0.8 | 5.6 | Short | 60 | 0.0 | NA |
| Approach | 415 | 2.0 |  | 0.460 |  | 8.1 | LOS A | 2.7 | 19.2 |  |  |  |  |
| Intersection | 2938 | 2.0 |  | 1.020 |  | 28.1 | LOS C | 27.3 | 194.7 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
6 Lane under-utilisation due to downstream effects
d Dominant lane on roundabout approach

## INPUT VOLUMES

## Vehicles and pedestrians per 60 minutes

$\Rightarrow$ Site: 101 [Crossing 2023 Sat (Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Multi-Lane Option
Roundabout

## Volume Display Method: Total and \%



|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: Rte 1 Ramps | 536 | 525 | 11 |
| E: Rothesay Ave WB | 819 | 803 | 16 |
| N: Rothesay Rd SB | 545 | 534 | 11 |
| W: Crossing Access EB | 585 | 573 | 12 |
| Total | 2485 | 2435 | 50 |

## LANE SUMMARY

## Site: 101 [Crossing 2023 Sat (Multi-Lane)]

Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Multi-Lane Option
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Bac <br> Veh | $\begin{array}{r} \text { Queue } \\ \text { Dist } \\ \mathrm{m} \end{array}$ | Lane Config | Lane Length m | Cap. Adj. \% | Prob. Block. \% |
| South: Rte 1 Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 316 | 2.0 | 527 | 0.600 | 100 | 25.2 | LOS C | 5.8 | 41.1 | Short | 60 | 0.0 | NA |
| Lane 2 | 248 | 2.0 | 461 | 0.539 | $90^{5}$ | 20.0 | LOS B | 4.5 | 32.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 564 | 2.0 |  | 0.600 |  | 22.9 | LOS C | 5.8 | 41.1 |  |  |  |  |
| East: Rothesay Ave WB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 574 | 2.0 | 780 | 0.736 | 100 | 12.3 | LOS B | 7.0 | 49.9 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 288 | 2.0 | 1035 | 0.279 | 100 | 4.7 | LOS A | 1.6 | 11.3 | Short | 60 | 0.0 | NA |
| Approach | 862 | 2.0 |  | 0.736 |  | 9.8 | LOS A | 7.0 | 49.9 |  |  |  |  |
| North: Rothesay Rd SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 439 | 2.0 | 530 | 0.829 | 100 | 37.5 | LOS D | 12.3 | 87.2 | Short | 60 | 0.0 | NA |
| Lane 2 | 135 | 2.0 | 320 | 0.421 | $51^{5}$ | 20.7 | LOS C | 2.7 | 19.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 574 | 2.0 |  | 0.829 |  | 33.5 | LOS C | 12.3 | 87.2 |  |  |  |  |
| West: Crossing Access EB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 476 | 2.0 | 606 | 0.786 | 100 | 16.0 | LOS B | 7.7 | 55.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 140 | 2.0 | 855 | 0.164 | 100 | 5.5 | LOS A | 0.7 | 5.1 | Short | 60 | 0.0 | NA |
| Approach | 616 | 2.0 |  | 0.786 |  | 13.6 | LOS B | 7.7 | 55.0 |  |  |  |  |
| Intersection | 2616 | 2.0 |  | 0.829 |  | 18.7 | LOS B | 12.3 | 87.2 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
d Dominant lane on roundabout approach
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## SITE LAYOUT

Site: 101 [Crossing 2023 Sat (Opt 3 Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Multi-Lane Option 3
Roundabout


## INPUT VOLUMES

## Vehicles and pedestrians per 60 minutes

Site: 101 [Crossing 2023 PM (Opt 3 Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Multi-Lane Option 3
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: Rte 1 Ramps | 946 | 927 | 19 |
| E: Rothesay Ave WB | 667 | 654 | 13 |
| N: Rothesay Rd SB | 784 | 768 | 16 |
| W: Crossing Access EB | 394 | 386 | 8 |
| Total | 2791 | 2735 | 56 |

## LANE SUMMARY

## Site: 101 [Crossing 2023 PM (Opt 3 Multi-Lane)]

Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Multi-Lane Option 3
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Veh | Queue Dist m | Lane Config | Lane Length m | Cap. Adj. \% | Prob. Block. \% |
| South: Rte 1 Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 506 | 2.0 | 539 | 0.939 | 100 | 48.2 | LOS D | 19.0 | 135.4 | Short | 60 | 0.0 | NA |
| Lane 2 | 409 | 2.0 | 479 | 0.853 | $91^{6}$ | 35.1 | LOS D | 12.4 | 88.5 | Full | 500 | 0.0 | 0.0 |
| Lane 3 | 81 | 2.0 | 540 | 0.150 | 100 | 11.8 | LOS B | 1.0 | 6.9 | Short | 60 | 0.0 | NA |
| Approach | 996 | 2.0 |  | 0.939 |  | 39.9 | LOS D | 19.0 | 135.4 |  |  |  |  |
| East: Rothesay Ave WB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 196 | 2.0 | 556 | 0.352 | 100 | 10.4 | LOS B | 1.8 | 12.6 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 506 | 2.0 | 713 | 0.710 | 100 | 10.3 | LOS B | 6.2 | 44.0 | Short | 60 | 0.0 | NA |
| Approach | 702 | 2.0 |  | 0.710 |  | 10.4 | LOS B | 6.2 | 44.0 |  |  |  |  |
| North: Rothesay Rd SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 581 | 2.0 | 776 | 0.749 | 100 | 21.2 | LOS C | 9.6 | 68.6 | Short | 60 | 0.0 | NA |
| Lane 2 | 244 | 2.0 | 565 | 0.432 | $58^{5}$ | 12.5 | LOS B | 2.9 | 20.5 | Full | 500 | 0.0 | 0.0 |
| Approach | 825 | 2.0 |  | 0.749 |  | 18.6 | LOS B | 9.6 | 68.6 |  |  |  |  |
| West: Crossing Access EB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 258 | 2.0 | 560 | 0.461 | 100 | 9.8 | LOS A | 2.7 | 19.3 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 157 | 2.0 | 885 | 0.177 | 100 | 5.4 | LOS A | 0.8 | 5.6 | Short | 60 | 0.0 | NA |
| Approach | 415 | 2.0 |  | 0.461 |  | 8.1 | LOS A | 2.7 | 19.3 |  |  |  |  |
| Intersection | 2938 | 2.0 |  | 0.939 |  | 22.4 | LOS C | 19.0 | 135.4 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
6 Lane under-utilisation due to downstream effects
d Dominant lane on roundabout approach

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## INPUT VOLUMES

## Vehicles and pedestrians per 60 minutes

Site: 101 [Crossing 2023 Sat (Opt 3 Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Multi-Lane Option 3
Roundabout

## Volume Display Method: Total and \%



|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: Rte 1 Ramps | 536 | 525 | 11 |
| E: Rothesay Ave WB | 819 | 803 | 16 |
| N: Rothesay Rd SB | 545 | 534 | 11 |
| W: Crossing Access EB | 585 | 573 | 12 |
| Total | 2485 | 2435 | 50 |

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## LANE SUMMARY

## Site: 101 [Crossing 2023 Sat (Opt 3 Multi-Lane)]

Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Multi-Lane Option 3
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back Veh | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \end{aligned}$ | Lane Config | Lane Length m | Cap. Adj. \% | Prob. Block. \% |
| South: Rte 1 Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 316 | 2.0 | 527 | 0.600 | 100 | 25.2 | LOS C | 5.8 | 41.1 | Short | 60 | 0.0 | NA |
| Lane 2 | 154 | 2.0 | 396 | 0.388 | $65^{5}$ | 17.7 | LOS B | 2.5 | 18.1 | Full | 500 | 0.0 | 0.0 |
| Lane 3 | 95 | 2.0 | 531 | 0.179 | 100 | 13.0 | LOS B | 1.1 | 8.2 | Short | 60 | 0.0 | NA |
| Approach | 564 | 2.0 |  | 0.600 |  | 21.1 | LOS C | 5.8 | 41.1 |  |  |  |  |
| East: Rothesay Ave WB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 574 | 2.0 | 782 | 0.734 | 100 | 12.3 | LOS B | 7.0 | 49.6 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 288 | 2.0 | 1038 | 0.278 | 100 | 4.7 | LOS A | 1.6 | 11.1 | Short | 60 | 0.0 | NA |
| Approach | 862 | 2.0 |  | 0.734 |  | 9.7 | LOS A | 7.0 | 49.6 |  |  |  |  |
| North: Rothesay Rd SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 439 | 2.0 | 530 | 0.828 | 100 | 37.4 | LOS D | 12.2 | 87.1 | Short | 60 | 0.0 | NA |
| Lane 2 | 135 | 2.0 | 320 | 0.421 | $51^{5}$ | 20.7 | LOS C | 2.7 | 19.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 574 | 2.0 |  | 0.828 |  | 33.5 | LOS C | 12.2 | 87.1 |  |  |  |  |
| West: Crossing Access EB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 476 | 2.0 | 606 | 0.786 | 100 | 16.0 | LOS B | 7.7 | 55.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 140 | 2.0 | 855 | 0.164 | 100 | 5.5 | LOS A | 0.7 | 5.1 | Short | 60 | 0.0 | NA |
| Approach | 616 | 2.0 |  | 0.786 |  | 13.6 | LOS B | 7.7 | 55.0 |  |  |  |  |
| Intersection | 2616 | 2.0 |  | 0.828 |  | 18.3 | LOS B | 12.2 | 87.1 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
d Dominant lane on roundabout approach

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\Crossing_2023wDevelopment.sip7

## SITE LAYOUT

$\theta$ Site: 101 [Crossing 2023 PM (Opt 4 Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Multi-Lane Option 4
Roundabout


Rte 1 Ramps

## INPUT VOLUMES

## Vehicles and pedestrians per 60 minutes

Site: 101 [Crossing 2023 PM (Opt 4 Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Multi-Lane Option 4
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: Rte 1 Ramps | 946 | 927 | 19 |
| E: Rothesay Ave WB | 667 | 654 | 13 |
| N: Rothesay Rd SB | 784 | 768 | 16 |
| W: Crossing Access EB | 394 | 386 | 8 |
| Total | 2791 | 2735 | 56 |

## LANE SUMMARY

## Site: 101 [Crossing 2023 PM (Opt 4 Multi-Lane)]

Rothesay Rd / Rothesay Ave
2023 PM peak w/ Development - Multi-Lane Option 4
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. $\%$ | Average Delay sec | Level of Service | 95\% Back <br> Veh | Queue Dist m | Lane Config | Lane Length m | Cap. Adj. \% | Prob. Block. \% |
| South: Rte 1 Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 511 | 2.0 | 556 | 0.920 | 100 | 40.4 | LOS D | 16.2 | 115.6 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 484 | 2.0 | 535 | 0.905 | $98^{6}$ | 34.9 | LOS C | 14.8 | 105.6 | Short | 60 | 0.0 | NA |
| Approach | 996 | 2.0 |  | 0.920 |  | 37.7 | LOS D | 16.2 | 115.6 |  |  |  |  |
| East: Rothesay Ave WB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 196 | 2.0 | 410 | 0.478 | $57^{5}$ | 13.5 | LOS B | 2.5 | 17.7 | Full | 500 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 506 | 2.0 | 606 | 0.836 | 100 | 14.7 | LOS B | 8.0 | 57.2 | Short | 60 | 0.0 | NA |
| Approach | 702 | 2.0 |  | 0.836 |  | 14.4 | LOS B | 8.0 | 57.2 |  |  |  |  |
| North: Rothesay Rd SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 615 | 2.0 | 783 | 0.786 | 100 | 21.4 | LOS C | 9.9 | 70.4 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 210 | 2.0 | 524 | 0.401 | $51^{6}$ | 11.6 | LOS B | 2.3 | 16.1 | Short | 60 | 0.0 | NA |
| Approach | 825 | 2.0 |  | 0.786 |  | 18.9 | LOS B | 9.9 | 70.4 |  |  |  |  |
| West: Crossing Access EB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 258 | 2.0 | 610 | 0.423 | 100 | 8.5 | LOS A | 2.5 | 17.7 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 157 | 2.0 | 508 | 0.309 | $73^{5}$ | 8.4 | LOS A | 1.5 | 10.8 | Short | 60 | 0.0 | NA |
| Approach | 415 | 2.0 |  | 0.423 |  | 8.5 | LOS A | 2.5 | 17.7 |  |  |  |  |
| Intersection | 2938 | 2.0 |  | 0.920 |  | 22.7 | LOS C | 16.2 | 115.6 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
6 Lane under-utilisation due to downstream effects
d Dominant lane on roundabout approach

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ICrossing_2023wDevelopment.sip7

## INPUT VOLUMES

## Vehicles and pedestrians per 60 minutes

Site: 101 [Crossing 2023 Sat (Opt 4 Multi-Lane)]
Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Multi-Lane Option 4
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: Rte 1 Ramps | 536 | 525 | 11 |
| E: Rothesay Ave WB | 819 | 803 | 16 |
| N: Rothesay Rd SB | 545 | 534 | 11 |
| W: Crossing Access EB | 585 | 573 | 12 |
| Total | 2485 | 2435 | 50 |

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ICrossing_2023wDevelopment.sip7

## LANE SUMMARY

## Site: 101 [Crossing 2023 Sat (Opt 4 Multi-Lane)]

Rothesay Rd / Rothesay Ave
2023 Sat peak w/ Development - Multi-Lane Option 4
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Bac <br> Veh | $\begin{array}{r} \text { Queue } \\ \text { Dist } \\ \mathrm{m} \end{array}$ | Lane Config | Lane Length m | Cap. Adj. \% | Prob. Block. \% |
| South: Rte 1 Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 316 | 2.0 | 577 | 0.547 | 100 | 21.2 | LOS C | 4.3 | 30.6 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 248 | 2.0 | 525 | 0.473 | $86^{5}$ | 14.5 | LOS B | 3.2 | 23.1 | Short | 60 | 0.0 | NA |
| Approach | 564 | 2.0 |  | 0.547 |  | 18.3 | LOS B | 4.3 | 30.6 |  |  |  |  |
| East: Rothesay Ave WB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 574 | 2.0 | 848 | 0.677 | 100 | 10.8 | LOS B | 5.8 | 41.4 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 288 | 2.0 | 679 | 0.425 | $63^{5}$ | 7.0 | LOS A | 2.3 | 16.5 | Short | 60 | 0.0 | NA |
| Approach | 862 | 2.0 |  | 0.677 |  | 9.5 | LOS A | 5.8 | 41.4 |  |  |  |  |
| North: Rothesay Rd SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 439 | 2.0 | 553 | 0.794 | 100 | 31.8 | LOS C | 10.0 | 71.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 135 | 2.0 | 338 | 0.398 | $50^{5}$ | 17.7 | LOS B | 2.3 | 16.1 | Short | 60 | 0.0 | NA |
| Approach | 574 | 2.0 |  | 0.794 |  | 28.5 | LOS C | 10.0 | 71.0 |  |  |  |  |
| West: Crossing Access EB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 469 | 2.0 | 659 | 0.711 | 100 | 12.4 | LOS B | 6.3 | 44.6 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 147 | 2.0 | 406 | 0.362 | $51^{6}$ | 10.9 | LOS B | 1.8 | 12.6 | Short | 60 | 0.0 | NA |
| Approach | 616 | 2.0 |  | 0.711 |  | 12.1 | LOS B | 6.3 | 44.6 |  |  |  |  |
| Intersection | 2616 | 2.0 |  | 0.794 |  | 16.2 | LOS B | 10.0 | 71.0 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
6 Lane under-utilisation due to downstream effects
d Dominant lane on roundabout approach

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 44: Rothesay Ave \& Rothesay Rd


|  | 4 |  |  | 7 |  |  | 4 | $\dagger$ |  | , | $\dagger$ | $+$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 5 | 447 | 133 | 244 | 301 | 274 | 300 | 146 | 90 | 417 | 125 | 3 |
| Future Volume (vph) | 5 | 447 | 133 | 244 | 301 | 274 | 300 | 146 | 90 | 417 | 125 | 3 |
| Satd. Flow (prot) | 1789 | 1883 | 1601 | 1789 | 1883 | 1601 | 1789 | 1776 | 0 | 1789 | 1878 | 0 |
| Flt Permitted | 0.306 |  |  | 0.216 |  |  | 0.668 |  |  | 0.287 |  |  |
| Satd. Flow (perm) | 576 | 1883 | 1601 | 407 | 1883 | 1601 | 1258 | 1776 | 0 | 541 | 1878 | 0 |
| Satd. Flow (RTOR) |  |  | 130 |  |  | 298 |  | 31 |  |  | 1 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 5 | 486 | 145 | 265 | 327 | 298 | 326 | 257 | 0 | 453 | 139 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Free | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | Free | 2 |  |  | 6 |  |  |
| Total Split (s) | 9.0 | 32.0 | 32.0 | 12.0 | 35.0 |  | 18.6 | 24.0 |  | 22.0 | 27.4 |  |
| Total Lost Time (s) | 4.0 | 4.5 | 4.5 | 4.0 | 4.5 |  | 4.0 | 4.5 |  | 4.0 | 4.5 |  |
| Act Effct Green (s) | 26.5 | 26.0 | 26.0 | 36.9 | 36.4 | 90.0 | 35.3 | 21.2 |  | 43.0 | 25.3 |  |
| Actuated g/C Ratio | 0.29 | 0.29 | 0.29 | 0.41 | 0.40 | 1.00 | 0.39 | 0.24 |  | 0.48 | 0.28 |  |
| v/c Ratio | 0.02 | 0.89 | 0.26 | 0.91 | 0.43 | 0.19 | 0.57 | 0.58 |  | 0.90 | 0.26 |  |
| Control Delay | 21.8 | 51.0 | 7.0 | 48.4 | 10.8 | 0.2 | 20.5 | 33.6 |  | 41.8 | 27.7 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 21.8 | 51.0 | 7.0 | 48.4 | 10.8 | 0.2 | 20.5 | 33.6 |  | 41.8 | 27.7 |  |
| LOS | C | D | A | D | B | A | C | C |  | D | C |  |
| Approach Delay |  | 40.7 |  |  | 18.5 |  |  | 26.3 |  |  | 38.4 |  |
| Approach LOS |  | D |  |  | B |  |  | C |  |  | D |  |
| Queue Length 50th (m) | 0.6 | 78.1 | 1.8 | 17.1 | 13.1 | 0.0 | 35.3 | 35.5 |  | 50.3 | 19.2 |  |
| Queue Length 95th (m) | 3.0 | \#129.5 | 14.5 | m\#53.0 | m33.5 | m0.0 | 55.5 | 60.4 |  | \#101.3 | 35.4 |  |
| Internal Link Dist (m) |  | 94.6 |  |  | 113.6 |  |  | 98.1 |  |  | 65.9 |  |
| Turn Bay Length (m) | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  |  | 50.0 |  |  |
| Base Capacity (vph) | 237 | 575 | 579 | 291 | 760 | 1601 | 593 | 443 |  | 509 | 528 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.02 | 0.85 | 0.25 | 0.91 | 0.43 | 0.19 | 0.55 | 0.58 |  | 0.89 | 0.26 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 71 (79\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.91 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 29.8 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 87.5\% |  |  |  |  | CU Level of Service E |  |  |  |  |  |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 48: Rothesay Rd \& Rothesay Ave


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | * |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 147 | 1 | 642 | 1 | 0 | 2 | 177 | 287 | 5 | 0 | 159 | 29 |
| Future Vol, veh/h | 147 | 1 | 642 | 1 | 0 | 2 | 177 | 287 | 5 | 0 | 159 | 29 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 800 | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 160 | 1 | 698 | 1 | 0 | 2 | 192 | 312 | 5 | 0 | 173 | 32 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | \& |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 86 | 0 | 133 | 0 | 0 | 0 | 118 | 180 | 0 | 0 | 171 | 45 |
| Future Vol, veh/h | 86 | 0 | 133 | 0 | 0 | 0 | 118 | 180 | 0 | 0 | 171 | 45 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 800 | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 93 | 0 | 145 | 0 | 0 | 0 | 128 | 196 | 0 | 0 | 186 | 49 |




Analysis Period (min) 15
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 45: Rothesay Rd


|  | 4 |  |  |  |  |  |  | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\beta}$ |  |  | $\uparrow$ |  | \% | $\hat{\dagger}$ |  |  | ${ }_{\$}$ |  |
| Traffic Volume (vph) | 93 | 0 | 133 | 0 | 0 | 0 | 253 | 173 | 0 | 0 | 171 | 45 |
| Future Volume (vph) | 93 | 0 | 133 | 0 | 0 | 0 | 253 | 173 | 0 | 0 | 171 | 45 |
| Satd. Flow (prot) | 1789 | 1601 | 0 | 0 | 1883 | 0 | 1789 | 1883 | 0 | 0 | 1831 | 0 |
| Flt Permitted | 0.757 |  |  |  |  |  | 0.612 |  |  |  |  |  |
| Satd. Flow (perm) | 1426 | 1601 | 0 | 0 | 1883 | 0 | 1153 | 1883 | 0 | 0 | 1831 | 0 |
| Satd. Flow (RTOR) |  | 739 |  |  |  |  |  |  |  |  | 30 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 101 | 145 | 0 | 0 | 0 | 0 | 275 | 188 | 0 | 0 | 235 | 0 |
| Turn Type | Perm | NA |  |  |  |  | pm+pt | NA |  |  | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Total Split (s) | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 14.0 | 32.0 |  | 18.0 | 18.0 |  |
| Total Lost Time (s) | 4.5 | 4.5 |  |  | 4.5 |  | 4.5 | 4.5 |  |  | 4.5 |  |
| Act Effct Green (s) | 7.6 | 7.6 |  |  |  |  | 30.4 | 31.3 |  |  | 16.4 |  |
| Actuated g/C Ratio | 0.17 | 0.17 |  |  |  |  | 0.68 | 0.70 |  |  | 0.36 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.42 | 0.16 |  |  |  |  | 0.30 | 0.14 |  |  | 0.34 |  |
| Control Delay | 22.2 | 0.4 |  |  |  |  | 3.0 | 2.1 |  |  | 12.4 |  |
| Queue Delay | 0.0 | 0.0 |  |  |  |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Delay | 22.2 | 0.4 |  |  |  |  | 3.0 | 2.1 |  |  | 12.4 |  |
| LOS | C | A |  |  |  |  | A | A |  |  | B |  |
| Approach Delay |  | 9.3 |  |  |  |  |  | 2.7 |  |  | 12.4 |  |
| Approach LOS |  | A |  |  |  |  |  | A |  |  | B |  |
| Queue Length 50th (m) | 7.0 | 0.0 |  |  |  |  | 4.3 | 2.9 |  |  | 12.4 |  |
| Queue Length 95th (m) | 17.2 | 0.0 |  |  |  |  | 7.5 | 5.3 |  |  | 26.4 |  |
| Internal Link Dist ( m ) |  | 190.2 |  |  | 73.2 |  |  | 210.7 |  |  | 122.0 |  |
| Turn Bay Length ( m ) |  |  |  |  |  |  | 50.0 |  |  |  |  |  |
| Base Capacity (vph) | 269 | 901 |  |  |  |  | 913 | 1310 |  |  | 687 |  |
| Starvation Cap Reductn | 0 | 0 |  |  |  |  | 0 | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  |  |  | 0 | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  |  |  | 0 | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.38 | 0.16 |  |  |  |  | 0.30 | 0.14 |  |  | 0.34 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 45 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 45 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 40 (89\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.42 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 6.8 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 45.2\% |  |  |  | ICU Level of Service A |  |  |  |  |  |  |  |  |

Analysis Period (min) 15
Splits and Phases: 67:


|  | 4 |  |  | 7 |  | 4 | 4 | $\dagger$ | \% |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | 4 |  |  |  |  |  | 4 | 「 |
| Traffic Volume (veh/h) | 0 | 383 | 487 | 0 | 564 | 0 | 0 | 0 | 0 | 0 | 262 | 117 |
| Future Volume (Veh/h) | 0 | 383 | 487 | 0 | 564 | 0 | 0 | 0 | 0 | 0 | 262 | 117 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 416 | 529 | 0 | 613 | 0 | 0 | 0 | 0 | 0 | 285 | 127 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 592 | 285 | 285 | 493 | 285 | 0 | 285 |  |  | 0 |  |  |
| vC 1 , stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC 2 , stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 592 | 285 | 285 | 493 | 285 | 0 | 285 |  |  | 0 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 33 | 30 | 100 | 2 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 36 | 624 | 754 | 67 | 624 | 1085 | 1277 |  |  | 1623 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SB 1 | SB 2 |  |  |  |  |  |  |  |  |
| Volume Total | 945 | 613 | 285 | 127 |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |
| Volume Right | 529 | 0 | 0 | 127 |  |  |  |  |  |  |  |  |
| cSH | 691 | 624 | 1700 | 1700 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 1.37 | 0.98 | 0.17 | 0.07 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 308.0 | 110.0 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 193.3 | 57.4 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 193.3 | 57.4 | 0.0 |  |  |  |  |  |  |  |  |  |
| Approach LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 110.6 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 70.4\% |  | Level | Service |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |



|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\ddagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | 4 |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (vph) | 0 | 383 | 487 | 0 | 564 | 0 | 0 | 0 | 0 | 0 | 262 | 117 |
| Future Volume (vph) | 0 | 383 | 487 | 0 | 564 | 0 | 0 | 0 | 0 | 0 | 262 | 117 |
| Satd. Flow (prot) | 0 | 1883 | 1601 | 0 | 1883 | 0 | 0 | 0 | 0 | 0 | 1883 | 1601 |
| Flt Permitted |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 0 | 1883 | 1601 | 0 | 1883 | 0 | 0 | 0 | 0 | 0 | 1883 | 1601 |
| Satd. Flow (RTOR) |  |  | 369 |  |  |  |  |  |  |  |  | 127 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 416 | 529 | 0 | 613 | 0 | 0 | 0 | 0 | 0 | 285 | 127 |
| Turn Type |  | NA | Free |  | NA |  |  |  |  |  | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases |  |  | Free |  |  |  |  |  |  |  |  | 6 |
| Total Split (s) |  | 28.0 |  |  | 28.0 |  |  |  |  |  | 17.0 | 17.0 |
| Total Lost Time (s) |  | 4.5 |  |  | 4.5 |  |  |  |  |  | 4.5 | 4.5 |
| Act Effct Green (s) |  | 25.1 | 45.0 |  | 25.1 |  |  |  |  |  | 10.9 | 10.9 |
| Actuated g/C Ratio |  | 0.56 | 1.00 |  | 0.56 |  |  |  |  |  | 0.24 | 0.24 |
| v/c Ratio |  | 0.40 | 0.33 |  | 0.58 |  |  |  |  |  | 0.63 | 0.26 |
| Control Delay |  | 8.8 | 0.1 |  | 9.9 |  |  |  |  |  | 21.5 | 4.9 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 |  |  |  |  |  | 0.0 | 0.0 |
| Total Delay |  | 8.8 | 0.1 |  | 9.9 |  |  |  |  |  | 21.5 | 4.9 |
| LOS |  | A | A |  | A |  |  |  |  |  | C | A |
| Approach Delay |  | 4.0 |  |  | 9.9 |  |  |  |  |  | 16.4 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | B |  |
| Queue Length 50th (m) |  | 7.2 | 0.0 |  | 28.4 |  |  |  |  |  | 19.3 | 0.0 |
| Queue Length 95th (m) |  | m7.5 | m0.0 |  | 54.1 |  |  |  |  |  | 36.1 | 8.4 |
| Internal Link Dist (m) |  | 124.0 |  |  | 72.0 |  |  | 152.4 |  |  | 127.2 |  |
| Turn Bay Length ( m ) |  |  | 20.0 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) |  | 1051 | 1601 |  | 1051 |  |  |  |  |  | 523 | 536 |
| Starvation Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Reduced v/c Ratio |  | 0.40 | 0.33 |  | 0.58 |  |  |  |  |  | 0.54 | 0.24 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 45 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 45 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $12.8(28 \%)$, Referenced to phase 4:EBT and 8:WBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.63 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 8.4 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 51.0\% |  |  |  | ICU Level of Service A |  |  |  |  |  |  |  |  |

Analysis Period (min) 15
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: $\quad$ 53: Rothesay Ave \& Rte 1 off-ramp


|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 | 「 |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Trafic Volume (vph) | 0 | 326 | 627 | 0 | 639 | 0 | 0 | 0 | 0 | 0 | 740 | 222 |
| Future Volume (vph) | 0 | 326 | 627 | 0 | 639 | 0 | 0 | 0 | 0 | 0 | 740 | 222 |
| Satd. Flow (prot) | 0 | 1883 | 1601 | 0 | 1883 | 0 | 0 | 0 | 0 | 0 | 1883 | 1601 |
| Flt Permitted |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 0 | 1883 | 1601 | 0 | 1883 | 0 | 0 | 0 | 0 | 0 | 1883 | 1601 |
| Satd. Flow (RTOR) |  |  | 280 |  |  |  |  |  |  |  |  | 128 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 354 | 682 | 0 | 695 | 0 | 0 | 0 | 0 | 0 | 804 | 241 |
| Turn Type |  | NA | Free |  | NA |  |  |  |  |  | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases |  |  | Free |  |  |  |  |  |  |  |  | 6 |
| Total Split (s) |  | 43.0 |  |  | 43.0 |  |  |  |  |  | 47.0 | 47.0 |
| Total Lost Time (s) |  | 4.5 |  |  | 4.5 |  |  |  |  |  | 4.5 | 4.5 |
| Act Effct Green (s) |  | 39.6 | 90.0 |  | 39.6 |  |  |  |  |  | 41.4 | 41.4 |
| Actuated g/C Ratio |  | 0.44 | 1.00 |  | 0.44 |  |  |  |  |  | 0.46 | 0.46 |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.43 | 0.43 |  | 0.84 |  |  |  |  |  | 0.93 | 0.30 |
| Control Delay |  | 14.0 | 0.4 |  | 34.1 |  |  |  |  |  | 41.3 | 7.8 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 |  |  |  |  |  | 0.0 | 0.0 |
| Total Delay |  | 14.0 | 0.4 |  | 34.1 |  |  |  |  |  | 41.3 | 7.8 |
| LOS |  | B | A |  | C |  |  |  |  |  | D | A |
| Approach Delay |  | 5.1 |  |  | 34.1 |  |  |  |  |  | 33.6 |  |
| Approach LOS |  | A |  |  | C |  |  |  |  |  | C |  |
| Queue Length 50th (m) |  | 34.6 | 0.0 |  | 106.0 |  |  |  |  |  | 122.8 | 10.7 |
| Queue Length 95th (m) |  | m44.6 | m0.0 |  | \#170.5 |  |  |  |  |  | \#197.8 | 24.6 |
| Internal Link Dist ( $m$ ) |  | 113.6 |  |  | 147.0 |  |  | 166.4 |  |  | 142.0 |  |
| Turn Bay Length ( m ) |  |  | 20.0 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) |  | 828 | 1601 |  | 828 |  |  |  |  |  | 889 | 823 |
| Starvation Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Reduced v/c Ratio |  | 0.43 | 0.43 |  | 0.84 |  |  |  |  |  | 0.90 | 0.29 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 88 (98\%), Referenced to phase 4:EBT and 8:WBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.93 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 23.1 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 80.1\% |  |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 50 : Rothesay Ave





$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2584 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \quad \mathrm{~km} / \mathrm{h}$
$1012 \quad \mathrm{vph}$
300 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3158 | 4600 | No |
| Fi F |  |  |  |
| v | 3158 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2022 | 4600 | No |
| FO F R |  |  |  |
| v | 1136 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\quad \mathrm{D}_{\mathrm{R}}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L} \quad=13.9 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$

Level of service for ramp-freeway junction areas of influence $C$

Speed Estimation $\qquad$


```
Phone:
Fax:
```

E-mail:

Merge Analysis

|  |  |
| :--- | :--- |
| Analyst: Merge Analysis____ |  |
| Agency/Co.: | Katie Hazzard |
| Date performed: | exp |
| Analysis time period: | $1 / 23 / 2017$ |
| Freeway/Dir of Travel: | AM Peak |
| Junction: | WB |
| Jurisdiction: | Rte 100 On Ramp |
| Analysis Year: | Provincial |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2706 | vph |


| Side of freeway | Ramp |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | Right |  |
| Free-flow speed on ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 60.0 | vph |
| Length of first accel/decel lane | 757 | m |
| Length of second accel/decel lane | 280 | m |

Does adjacent ramp exist?
Volume on adjacent Ramp
Position of adjacent Ramp
Type of adjacent Ramp
Distance to adjacent Ramp

$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 4157 | 4600 | No |
| V | 4157 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\mathrm{D}=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=19.6 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation $\qquad$

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route lo0 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2023 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2706 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$1158 \quad$ vph
240 m

Adjacent Ramp Data (if one exists) $\qquad$
Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
m


| 0.909 | 0.990 |
| :--- | :--- |
| 1.00 | 1.00 |
| 3307 | 1300 |

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3307 | 4600 | No |
| Fi F |  |  |  |
| v | 3307 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2007 | 4600 | No |
| FO F R |  |  |  |
| v | 1300 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $\quad \mathrm{D}_{\mathrm{R}}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L}=15.8 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$

Level of service for ramp-freeway junction areas of influence $C$

Speed Estimation $\qquad$

| Intermediate speed variable, | $\mathrm{D}=0.520$ |  |
| :---: | :---: | :---: |
|  | S |  |
| Space mean speed in ramp influence area, | $\underset{R}{S}=82.8$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=82.8$ | km/h |

```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Evening Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2016 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on freeway | 100.0 | 2584 |


| Side of freeway | Ramp |  |
| :--- | :--- | :--- |
| Number of lanes in ramp | Right |  |
| Free-flow speed on ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on ramp | 60.0 | vph |
| Length of first accel/decel lane | 913 | m |
| Length of second accel/decel lane | 150 | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 4183 | 4600 | No |
| FO | 4183 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=21.3 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.6 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 性 |  | ${ }^{1}$ | $\uparrow$ | \% | 「 |
| Traffic Vol, veh/h | 102 | 0 | 131 | 60 | 0 | 7 |
| Future Vol, veh/h | 102 | 0 | 131 | 60 | 0 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 111 | 0 | 142 | 65 | 0 | 8 |





| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ${ }^{7}$ | 「 | $\uparrow$ |  | ${ }^{1}$ | 4 |
| Traffic Vol, veh/h | 16 | 2 | 805 | 23 | 3 | 203 |
| Future Vol, veh/h | 16 | 2 | 805 | 23 | 3 | 203 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | St | None | - | None | - | None |
| Storage Length | 0 | 0 | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 17 | 2 | 875 | 25 | 3 | 221 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }_{1}$ | 4 | $\uparrow$ |  |
| Traffic Vol, veh/h | 1 | 2 | 3 | 827 | 218 | 1 |
| Future Vol, veh/h | 1 | 2 | 3 | 827 | 218 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | 750 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 2 | 3 | 899 | 237 | 1 |



|  | 4 |  |  | 7 |  |  |  | $\dagger$ | 7 |  | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }_{1}$ | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  | ${ }^{1}$ | F |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 1 | 9 | 1 | 41 | 9 | 133 | 1 | 696 | 40 | 93 | 126 | 1 |
| Future Volume (vph) | 1 | 9 | 1 | 41 | 9 | 133 | 1 | 696 | 40 | 93 | 126 | 1 |
| Satd. Flow (prot) | 1789 | 1857 | 0 | 1789 | 1620 | 0 | 1789 | 1868 | 0 | 1789 | 1882 | 0 |
| Flt Permitted | 0.889 |  |  | 0.889 |  |  | 0.669 |  |  | 0.295 |  |  |
| Satd. Flow (perm) | 1674 | 1857 | 0 | 1674 | 1620 | 0 | 1260 | 1868 | 0 | 556 | 1882 | 0 |
| Satd. Flow (RTOR) |  | 1 |  |  | 145 |  |  | 14 |  |  | 1 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 1 | 11 | 0 | 45 | 155 | 0 | 1 | 800 | 0 | 101 | 138 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Total Split (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 35.0 | 35.0 |  | 35.0 | 35.0 |  |
| Total Lost Time (s) | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  |
| Act Effct Green (s) | 5.5 | 5.5 |  | 5.5 | 5.5 |  | 34.1 | 34.1 |  | 34.1 | 34.1 |  |
| Actuated g/C Ratio | 0.12 | 0.12 |  | 0.12 | 0.12 |  | 0.74 | 0.74 |  | 0.74 | 0.74 |  |
| v/c Ratio | 0.01 | 0.05 |  | 0.23 | 0.48 |  | 0.00 | 0.58 |  | 0.25 | 0.10 |  |
| Control Delay | 17.0 | 17.5 |  | 20.9 | 10.7 |  | 2.0 | 5.8 |  | 4.7 | 2.7 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 17.0 | 17.5 |  | 20.9 | 10.7 |  | 2.0 | 5.8 |  | 4.7 | 2.7 |  |
| LOS | B | B |  | C | B |  | A | A |  | A | A |  |
| Approach Delay |  | 17.5 |  |  | 13.0 |  |  | 5.8 |  |  | 3.6 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | A |  |
| Queue Length 50th (m) | 0.1 | 0.7 |  | 3.3 | 0.7 |  | 0.0 | 24.5 |  | 2.2 | 2.7 |  |
| Queue Length 95th (m) | 1.0 | 3.9 |  | 10.0 | 12.5 |  | 0.3 | 46.8 |  | 6.8 | 5.9 |  |
| Internal Link Dist (m) |  | 212.8 |  |  | 58.7 |  |  | 111.4 |  |  | 178.1 |  |
| Turn Bay Length (m) |  |  |  |  |  |  |  |  |  | 100.0 |  |  |
| Base Capacity (vph) | 200 | 223 |  | 200 | 321 |  | 935 | 1390 |  | 412 | 1396 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.01 | 0.05 |  | 0.23 | 0.48 |  | 0.00 | 0.58 |  | 0.25 | 0.10 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 45 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 46 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.58 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 6.6 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 64.4\% |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 64: Ashburn Rd \& Access 5 (main)


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.4 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  | \% | $\uparrow$ | ${ }^{7}$ | 「 |
| Traffic Vol, veh/h | 100 | 0 | 135 | 77 | 0 | 7 |
| Future Vol, veh/h | 100 | 0 | 135 | 77 | 0 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |  | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 0 | - | 0 | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 109 | 0 | 147 | 84 | 0 | 8 |










Splits and Phases: 64: Ashburn \& Access 5


## Appendix D- <br> LOS Results with Phase 2 \& 3 (2033) of Development

## Appendix D- <br> LOS Results with Phase 2 \& 3 (2033) of Development

| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | 「 | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | $\hat{\beta}$ |  | 7 | $\uparrow$ |  |
| Traffic Volume (vph) |  | 294 | 287 | 127 | 195 | 183 | 273 | 20 | 607 | 236 | 124 | 35 |
| Future Volume (vph) | 5 | 294 | 287 | 127 | 195 | 183 | 273 | 20 | 607 | 236 | 124 | 35 |
| Satd. Flow (prot) | 1789 | 1883 | 1601 | 1789 | 1883 | 1601 | 1789 | 1610 | 0 | 1789 | 1821 | 0 |
| FIt Permitted | 0.625 |  |  | 0.331 |  |  | 0.425 |  |  | 0.392 |  |  |
| Satd. Flow (perm) | 1177 | 1883 | 1601 | 623 | 1883 | 1601 | 800 | 1610 | 0 | 738 | 1821 | 0 |
| Satd. Flow (RTOR) |  |  | 312 |  |  | 227 |  | 462 |  |  | 20 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 5 | 320 | 312 | 138 | 212 | 199 | 297 | 682 | 0 | 257 | 173 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  |  | 8 |  |  |
| Total Split (s) | 9.0 | 21.0 | 21.0 | 9.0 | 21.0 | 21.0 | 15.0 | 25.0 |  | 10.0 | 20.0 |  |
| Total Lost Time (s) | 4.0 | 4.5 | 4.5 | 4.0 | 4.5 | 4.5 | 4.0 | 4.5 |  | 4.0 | 4.5 |  |
| Act Efft Green (s) | 18.3 | 14.1 | 14.1 | 20.5 | 19.1 | 19.1 | 27.2 | 16.0 |  | 16.9 | 12.2 |  |
| Actuated g/C Ratio | 0.32 | 0.25 | 0.25 | 0.36 | 0.34 | 0.34 | 0.48 | 0.28 |  | 0.30 | 0.21 |  |
| v/c Ratio | 0.01 | 0.69 | 0.49 | 0.41 | 0.34 | 0.29 | 0.48 | 0.87 |  | 0.76 | 0.43 |  |
| Control Delay | 12.0 | 29.9 | 6.0 | 17.0 | 17.6 | 3.6 | 13.3 | 20.7 |  | 30.5 | 22.2 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 12.0 | 29.9 | 6.0 | 17.0 | 17.6 | 3.6 | 13.3 | 20.7 |  | 30.5 | 22.2 |  |
| LOS | B | C | A | B | B | A | B | C |  | C | C |  |
| Approach Delay |  | 18.0 |  |  | 12.4 |  |  | 18.5 |  |  | 27.1 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 0.4 | 34.6 | 0.0 | 10.4 | 17.0 | 0.0 | 21.0 | 21.0 |  | 17.8 | 15.3 |  |
| Queue Length 95th (m) | 2.1 | \#59.8 | 16.3 | 20.7 | 38.7 | 10.4 | 36.3 | \#83.6 |  | \#40.2 | 30.6 |  |
| Internal Link Dist (m) |  | 367.7 |  |  | 713.5 |  |  | 186.6 |  |  | 28.7 |  |
| Turn Bay Length (m) | 50.0 |  | 50.0 | 50.0 |  | 50.0 |  |  |  |  |  |  |
| Base Capacity (vph) | 435 | 580 | 709 | 333 | 725 | 756 | 623 | 902 |  | 337 | 541 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.01 | 0.55 | 0.44 | 0.41 | 0.29 | 0.26 | 0.48 | 0.76 |  | 0.76 | 0.32 |  |

## Intersection Summary

Cycle Length: 65
Actuated Cycle Length: 56.9
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.87

Intersection Signal Delay: 18.5
Intersection Capacity Utilization 88.4\%
Analysis Period (min) 15

Intersection LOS: B
ICU Level of Service E
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 4: Foster Thurston Dr \& Ashburn Rd


| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | F | \% | $\uparrow$ | 「 | \% | $\hat{F}$ |  | ${ }^{7}$ | F |  |
| Traffic Volume (vph) | 5 | 430 | 462 | 113 | 352 | 147 | 133 | 14 | 148 | 418 | 175 | 93 |
| Future Volume (vph) | 5 | 430 | 462 | 113 | 352 | 147 | 133 | 14 | 148 | 418 | 175 | 93 |
| Satd. Flow (prot) | 1789 | 1883 | 1601 | 1789 | 1883 | 1601 | 1789 | 1625 | 0 | 1789 | 1786 | 0 |
| Flt Permitted | 0.481 |  |  | 0.261 |  |  |  |  |  | 0.519 |  |  |
| Satd. Flow (perm) | 906 | 1883 | 1601 | 492 | 1883 | 1601 | 1883 | 1625 | 0 | 978 | 1786 | 0 |
| Satd. Flow (RTOR) |  |  | 502 |  |  | 245 |  | 161 |  |  | 40 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## Parking (\#/hr)

| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 5 | 467 | 502 | 123 | 383 | 160 | 145 | 176 | 0 | 454 | 291 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  |  | 8 |  |  |
| Total Split (s) | 9.0 | 25.4 | 25.4 | 9.0 | 25.4 | 25.4 | 9.0 | 9.6 |  | 16.0 | 16.6 |  |
| Total Lost Time (s) | 4.0 | 4.5 | 4.5 | 4.0 | 4.5 | 4.5 | 4.0 | 4.5 |  | 4.0 | 4.5 |  |
| Act Effct Green (s) | 23.0 | 18.8 | 18.8 | 25.2 | 23.7 | 23.7 | 9.4 | 5.4 |  | 19.7 | 12.7 |  |
| Actuated g/C Ratio | 0.43 | 0.35 | 0.35 | 0.47 | 0.44 | 0.44 | 0.17 | 0.10 |  | 0.36 | 0.23 |  |
| v/c Ratio | 0.01 | 0.71 | 0.57 | 0.35 | 0.46 | 0.19 | 0.46 | 0.57 |  | 0.83 | 0.65 |  |
| Control Delay | 7.6 | 24.0 | 4.6 | 10.9 | 14.0 | 1.2 | 20.3 | 15.8 |  | 33.0 | 28.0 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 7.6 | 24.0 | 4.6 | 10.9 | 14.0 | 1.2 | 20.3 | 15.8 |  | 33.0 | 28.0 |  |
| LOS | A | C | A | B | B | A | C | B |  | C | C |  |
| Approach Delay |  | 13.9 |  |  | 10.3 |  |  | 17.8 |  |  | 31.0 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 0.3 | 43.3 | 0.0 | 6.6 | 24.5 | 0.0 | 10.8 | 1.6 |  | 41.7 | 26.0 |  |
| Queue Length 95th (m) | 1.5 | \#74.4 | 16.6 | 13.7 | 57.0 | 3.2 | 21.4 | \#21.4 |  | \#74.2 | \#58.3 |  |
| Internal Link Dist (m) |  | 367.7 |  |  | 713.5 |  |  | 186.6 |  |  | 27.8 |  |
| Turn Bay Length ( m ) | 50.0 |  | 50.0 | 50.0 |  | 50.0 | 50.0 |  |  |  |  |  |
| Base Capacity (vph) | 471 | 772 | 952 | 356 | 933 | 916 | 317 | 307 |  | 547 | 455 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.01 | 0.60 | 0.53 | 0.35 | 0.41 | 0.17 | 0.46 | 0.57 |  | 0.83 | 0.64 |  |

## Intersection Summary

Cycle Length: 60
Actuated Cycle Length: 54.1
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.83

Intersection Signal Delay: 18.2
Intersection Capacity Utilization 76.1\%
Analysis Period (min) 15

Intersection LOS: B
ICU Level of Service D
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: $\quad 4: 18 /$ Foster Thurston Dr \& Ashburn Rd


## Phone:

Fax:
E-mail:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Foster Thurston Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2755 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$1339 \quad \mathrm{vph}$
130 m
$\qquad$

| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent ramp |  | vph |
| Position of adjacent ramp |  |  |
| Type of adjacent ramp | m |  |



| 0.909 | 0.990 |
| :--- | :--- |
| 1.00 | 1.00 |
| 3367 | 1503 |

Estimation of V12 Diverge Areas $\qquad$


Capacity Checks


Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$

| Intermediate speed variable, | $D_{S}=0.53$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=82.2$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=82.2$ | km/h |

```
Phone:
Fax:
```

E-mail:

Merge Analysis

| ____Merge Analysis_ |  |
| :--- | :--- |
| Analyst: |  |
| Agency/Co.: | Katie Hazzard |
| Date performed: | exp |
| Analysis time period: | $1 / 23 / 2017$ |
| Freeway/Dir of Travel: | AM Peak |
| Junction: | Westbond |
| Jurisdiction: | Foster Thurston On Ramp |
| Analysis Year: | Provincial |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 2755 | vph |


|  | Ramp |  |
| :--- | :--- | :--- |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 383 | m |
| Length of first accel/decel lane | 120 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 3797 | 4600 | No |
| FO | 3797 | 4600 | No |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=20.0 \quad \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $D$
Speed Estimation


## Phone:

Fax:
E-mail:

Diverge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $3 / 8 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Eastbound |
| Junction: | Ashburn Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing Study |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 90.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3282 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
$329 \quad v p h$
180 m
m

Adjacent Ramp Data (if one exists) $\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
m

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 4011 | 4500 | No |
| Fi F |  |  |  |
| v | 4011 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 3642 | 4500 | No |
| FO F R |  |  |  |
| v | 369 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$


Speed Estimation $\qquad$


```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM Peak |
| Freeway/Dir of Travel: | Eastbond |
| Junction: | Ashburn On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on freeway | 100.0 | 3694 |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 722 | vph |
| Length of first accel/decel lane | 150 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 5325 | 4600 | Yes |
| V |  |  | Yes |
| R12 | 5325 | 4600 |  |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=26.9 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $F$
Speed Estimation


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\hat{\beta}$ |  |  | ¢ |  |  | $\hat{\dagger}$ |  |  | $\dagger$ |  |  |
| Traffic Vol, veh/h | 0 | 0 | 117 | 5 | 0 | 5 | 0 | 1028 | 4 | 4 | 690 | 1 |
| Future Vol, veh/h | 0 | 0 | 117 | 5 | 0 | 5 | 0 | 1028 | 4 | 4 | 690 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - |  | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 127 | 5 | 0 | 5 | 0 | 1117 | 4 | 4 | 750 | 1 |


| Major/Minor | Minor2 |  | Minor1 |  |  |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 1881 | 751 |  | 1943 | 1880 | 1120 | - | 0 | 0 | 1122 | 0 | 0 |
| Stage 1 | - | 759 | - |  | 1120 | 1120 | - | - | - | - | - | - |  |
| Stage 2 | - | 1122 | - |  | 823 | 760 | - | - | - |  |  | - |  |
| Critical Hdwy | - | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 | - | - |  | 4.12 | - |  |
| Critical Hdwy Stg 1 | - | 5.52 | - |  | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | 5.52 | - |  | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Follow-up Hdwy | - | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 | - | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 0 | 71 | 411 |  | 49 | 71 | 251 | 0 | - | - | 623 | - |  |
| Stage 1 | 0 | 415 | - |  | 251 | 282 | - | 0 | - | - | - | - |  |
| Stage 2 | 0 | 281 | - |  | 368 | 414 | - | 0 | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | - | 70 | 411 |  | 34 | 70 | 251 | - | - | - | 623 | - |  |
| Mov Cap-2 Maneuver | - | 70 | - |  | 34 | 70 | - | - | - | - | - | - |  |
| Stage 1 | - | 410 | - |  | 251 | 282 | - | - | - | - | - | - |  |
| Stage 2 | - | 281 | - |  | 251 | 409 | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 17.6 |  |  |  | 77.8 |  |  | 0 |  |  | 0.1 |  |  |
| HCM LOS | C |  |  |  | F |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBT | NBR | EBLn1V | VBLn1 | SBL | SBT | SBR |  |  |  |  |  |  |
| Capacity (veh/h) | - | - | 411 | 60 | 623 | - | - |  |  |  |  |  |  |
| HCM Lane V/C Ratio | - | - | 0.309 | 0.181 | 0.007 | - | - |  |  |  |  |  |  |
| HCM Control Delay (s) | - | - | 17.6 | 77.8 | 10.8 | 0 | - |  |  |  |  |  |  |
| HCM Lane LOS | - | - | C | F | B | A | - |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | - | - | 1.3 | 0.6 | 0 | - | - |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\hat{\beta}$ |  |  | ¢ |  |  | $\hat{\beta}$ |  |  | $\uparrow$ |  |  |
| Traffic Vol, veh/h | 0 | 0 | 26 | 5 | 0 | 5 | 0 | 401 | 1 | 2 | 421 | 1 |
| Future Vol, veh/h | 0 | 0 | 26 | 5 | 0 | 5 | 0 | 401 | 1 | 2 | 421 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - |  | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 28 | 5 | 0 | 5 | 0 | 436 | 1 | 2 | 458 | 1 |


| Major/Minor | Minor2 |  | Minor1 |  |  |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 899 | 458 |  | 913 | 899 | 436 | - | 0 | 0 | 437 | 0 | 0 |
| Stage 1 | - | 462 | - |  | 436 | 436 | - | - | - | - | - | - |  |
| Stage 2 | - | 437 |  |  | 477 | 463 | - | - | - |  |  | - |  |
| Critical Hdwy | - | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 | - | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | - | 5.52 | - |  | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | 5.52 | - |  | 6.12 | 5.52 | - | - | - | - | - | - |  |
| Follow-up Hdwy | - | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 | - | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 0 | 279 | 603 |  | 254 | 279 | 620 | 0 | - | - | 1123 | - |  |
| Stage 1 | 0 | 565 | - |  | 599 | 580 |  | 0 | - | - | - | - |  |
| Stage 2 | 0 | 579 | - |  | 569 | 564 | - | 0 | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | - | 278 | 603 |  | 242 | 278 | 620 | - | - | - | 1123 | - |  |
| Mov Cap-2 Maneuver | - | 278 | - |  | 242 | 278 | - | - | - | - | - | - |  |
| Stage 1 | - | 564 | - |  | 599 | 580 | - | - | - | - | - | - |  |
| Stage 2 | - | 579 |  |  | 541 | 563 | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 11.3 |  |  |  | 15.7 |  |  | 0 |  |  | 0 |  |  |
| HCM LOS | B |  |  |  | C |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBT | NBR | EBLn1 | VBLn1 | SBL | SBT | SBR |  |  |  |  |  |  |
| Capacity (veh/h) | - | - | 603 | 348 | 1123 | - |  |  |  |  |  |  |  |
| HCM Lane V/C Ratio | - | - | 0.047 | 0.031 | 0.002 | - |  |  |  |  |  |  |  |
| HCM Control Delay (s) | - | - | 11.3 | 15.7 | 8.2 | 0 |  |  |  |  |  |  |  |
| HCM Lane LOS | - | - | B | C | A | A |  |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | - | - | 0.1 | 0.1 | 0 | - | - |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ |  | \% | F |  | ${ }^{7}$ | F |  | ${ }^{7}$ | F |  |
| Traffic Vol, veh/h | 2 | 0 | 1 | 11 | 0 | 5 | 5 | 625 | 17 | 31 | 610 | 1 |
| Future Vol, veh/h | 2 | 0 | 1 | 11 | 0 | 5 | 5 | 625 | 17 | 31 | 610 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | 0 | - | - | 500 | - | - | 500 | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - |  | 0 | - | - | 0 |  |
| Grade, \% | - | 0 |  | - | 0 | - |  | 0 |  |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 2 | 0 | 1 | 12 | 0 | 5 | 5 | 679 | 18 | 34 | 663 | 1 |


| Major/Minor | Minor2 |  | Minor1 |  |  |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1433 | 1440 | 664 |  | 1431 | 1431 | 689 |  | 664 | 0 | 0 | 698 | 0 | 0 |
| Stage 1 | 731 | 731 | - |  | 699 | 699 |  |  | - | - | - | - | - |  |
| Stage 2 | 702 | 709 |  |  | 732 | 732 |  |  | - | - | - |  | - |  |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.12 | 5.52 |  |  | 6.12 | 5.52 | - |  | - | - | - |  | - |  |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 112 | 133 | 461 |  | 112 | 134 | 446 |  | 925 | - | - | 898 | - |  |
| Stage 1 | 413 | 427 | - |  | 430 | 442 | - |  | - | - | - | - | - |  |
| Stage 2 | 429 | 437 | - |  | 413 | 427 | - |  | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 107 | 127 | 461 |  | 108 | 128 | 446 |  | 925 | - | - | 898 | - |  |
| Mov Cap-2 Maneuver | 107 | 127 | - |  | 108 | 128 | - |  | - | - | - | - | - |  |
| Stage 1 | 411 | 411 | - |  | 428 | 440 | - |  | - | - | - | - | - |  |
| Stage 2 | 421 | 435 | - |  | 396 | 411 | - |  | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 30.5 |  |  |  | 33.3 |  |  |  | 0.1 |  |  | 0.4 |  |  |
| HCM LOS | D |  |  |  | D |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | BLn1 | EBLn2 | VBLn1V | VBLn2 | SBL | SBT | SBR |  |  |  |  |
| Capacity (veh/h) | 925 | - | - | 107 | 461 | 108 | 446 | 898 | - | - |  |  |  |  |
| HCM Lane V/C Ratio | 0.006 | - | - | 0.02 | 0.002 | 0.111 | 0.012 | 0.038 | - | - |  |  |  |  |
| HCM Control Delay (s) | 8.9 | - | - | 39.3 | 12.8 | 42.4 | 13.2 | 9.2 | - | - |  |  |  |  |
| HCM Lane LOS | A | - | - | E | B | E | B | A | - | - |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | - |  | 0.1 | 0 | 0.4 | 0 | 0.1 | - | - |  |  |  |  |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 4 | $\uparrow$ |  | * ${ }^{\text {P }}$ |  |
| Traffic Vol, veh/h | 2 | 312 | 270 | 20 | 28 | 0 |
| Future Vol, veh/h | 2 | 312 | 270 | 20 | 28 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 339 | 293 | 22 | 30 | 0 |





|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 44: Rothesay Ave \& Rothesay Rd


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 48: Rothesay Rd \& Rothesay Ave


|  | 4 |  |  | 7 |  | $4$ | $4$ | $\dagger$ | $p$ |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | $\uparrow$ |  |  | $\leqslant$ |  | ${ }^{7}$ | 4 |  |  | \& |  |
| Traffic Volume (vph) | 134 | 1 | 244 | 1 | 0 | 2 | 222 | 832 | 5 | 0 | 165 | 72 |
| Future Volume (vph) | 134 | 1 | 244 | 1 | 0 | 2 | 222 | 832 | 5 | 0 | 165 | 72 |
| Satd. Flow (prot) | 1789 | 1603 | 0 | 0 | 1687 | 0 | 1789 | 1882 | 0 | 0 | 1806 | 0 |
| Flt Permitted | 0.756 |  |  |  | 0.911 |  | 0.537 |  |  |  |  |  |
| Satd. Flow (perm) | 1424 | 1603 | 0 | 0 | 1561 | 0 | 1011 | 1882 | 0 | 0 | 1806 | 0 |
| Satd. Flow (RTOR) |  | 265 |  |  | 75 |  |  | 1 |  |  | 40 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 146 | 266 | 0 | 0 | 3 | 0 | 241 | 909 | 0 | 0 | 257 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA |  |  | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Total Split (s) | 21.6 | 21.6 |  | 21.6 | 21.6 |  | 13.0 | 58.4 |  | 45.4 | 45.4 |  |
| Total Lost Time (s) | 4.5 | 4.5 |  |  | 4.5 |  | 4.0 | 4.5 |  |  | 4.5 |  |
| Act Effct Green (s) | 13.2 | 13.2 |  |  | 13.2 |  | 58.3 | 57.8 |  |  | 45.5 |  |
| Actuated g/C Ratio | 0.16 | 0.16 |  |  | 0.16 |  | 0.73 | 0.72 |  |  | 0.57 |  |
| v/c Ratio | 0.62 | 0.55 |  |  | 0.01 |  | 0.29 | 0.67 |  |  | 0.25 |  |
| Control Delay | 42.3 | 8.5 |  |  | 0.0 |  | 1.7 | 4.8 |  |  | 8.9 |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Delay | 42.3 | 8.5 |  |  | 0.0 |  | 1.7 | 4.8 |  |  | 8.9 |  |
| LOS | D | A |  |  | A |  | A | A |  |  | A |  |
| Approach Delay |  | 20.5 |  |  |  |  |  | 4.2 |  |  | 8.9 |  |
| Approach LOS |  | C |  |  |  |  |  | A |  |  | A |  |
| Queue Length 50th (m) | 20.8 | 0.1 |  |  | 0.0 |  | 1.7 | 7.2 |  |  | 15.3 |  |
| Queue Length 95th (m) | 36.6 | 17.9 |  |  | 0.0 |  | m3.3 | m16.7 |  |  | 30.7 |  |
| Internal Link Dist (m) |  | 83.5 |  |  | 78.8 |  |  | 204.7 |  |  | 117.4 |  |
| Turn Bay Length (m) |  |  |  |  |  |  | 100.0 |  |  |  |  |  |
| Base Capacity (vph) | 304 | 550 |  |  | 392 |  | 825 | 1360 |  |  | 1044 |  |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.48 | 0.48 |  |  | 0.01 |  | 0.29 | 0.67 |  |  | 0.25 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 30 (38\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.67 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 8.5 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 83.6\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |  |

Analysis Period (min) 15
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 45: Rothesay Rd



Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 67:


|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\ddagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (vph) | 0 | 282 | 214 | 0 | 625 | 0 | 0 | 0 | 0 | 0 | 199 | 155 |
| Future Volume (vph) | 0 | 282 | 214 | 0 | 625 | 0 | 0 | 0 | 0 | 0 | 199 | 155 |
| Satd. Flow (prot) | 0 | 1883 | 1601 | 0 | 1883 | 0 | 0 | 0 | 0 | 0 | 1883 | 1601 |
| Flt Permitted |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 0 | 1883 | 1601 | 0 | 1883 | 0 | 0 | 0 | 0 | 0 | 1883 | 1601 |
| Satd. Flow (RTOR) |  |  | 233 |  |  |  |  |  |  |  |  | 168 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Trafic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 307 | 233 | 0 | 679 | 0 | 0 | 0 | 0 | 0 | 216 | 168 |
| Turn Type |  | NA | Free |  | NA |  |  |  |  |  | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases |  |  | Free |  |  |  |  |  |  |  |  | 6 |
| Total Split (s) |  | 27.0 |  |  | 27.0 |  |  |  |  |  | 13.0 | 13.0 |
| Total Lost Time (s) |  | 4.5 |  |  | 4.5 |  |  |  |  |  | 4.5 | 4.5 |
| Act Effct Green (s) |  | 26.0 | 40.0 |  | 26.0 |  |  |  |  |  | 8.0 | 8.0 |
| Actuated g/C Ratio |  | 0.65 | 1.00 |  | 0.65 |  |  |  |  |  | 0.20 | 0.20 |
| v/c Ratio |  | 0.25 | 0.15 |  | 0.55 |  |  |  |  |  | 0.57 | 0.37 |
| Control Delay |  | 5.9 | 0.1 |  | 7.8 |  |  |  |  |  | 21.0 | 5.9 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 |  |  |  |  |  | 0.0 | 0.0 |
| Total Delay |  | 5.9 | 0.1 |  | 7.8 |  |  |  |  |  | 21.0 | 5.9 |
| LOS |  | A | A |  | A |  |  |  |  |  | C | A |
| Approach Delay |  | 3.4 |  |  | 7.8 |  |  |  |  |  | 14.4 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | B |  |
| Queue Length 50th (m) |  | 20.2 | 0.0 |  | 25.9 |  |  |  |  |  | 13.1 | 0.0 |
| Queue Length 95th (m) |  | m23.6 | m0.0 |  | 49.4 |  |  |  |  |  | \#27.5 | 9.9 |
| Internal Link Dist (m) |  | 127.1 |  |  | 72.0 |  |  | 152.4 |  |  | 127.2 |  |
| Turn Bay Length ( m ) |  |  | 25.0 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) |  | 1226 | 1601 |  | 1226 |  |  |  |  |  | 400 | 472 |
| Starvation Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Reduced v/c Ratio |  | 0.25 | 0.15 |  | 0.55 |  |  |  |  |  | 0.54 | 0.36 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 40 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 40 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 16 (40\%), Referenced to phase 4:EBT and 8:WBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.57 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 7.9 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 50.9\% |  |  |  | ICU Level of Service A |  |  |  |  |  |  |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: $\quad$ 53: Rothesay Ave \& Rte 1 off-ramp


|  | $y$ |  |  |  |  |  |  | $\uparrow$ |  |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 | 「 |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Trafic Volume (vph) | 0 | 437 | 468 | 0 | 661 | 0 | 0 | 0 | 0 | 0 | 549 | 413 |
| Future Volume (vph) | 0 | 437 | 468 | 0 | 661 | 0 | 0 | 0 | 0 | 0 | 549 | 413 |
| Satd. Flow (prot) | 0 | 1883 | 1601 | 0 | 1883 | 0 | 0 | 0 | 0 | 0 | 1883 | 1601 |
| Flt Permitted |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 0 | 1883 | 1601 | 0 | 1883 | 0 | 0 | 0 | 0 | 0 | 1883 | 1601 |
| Satd. Flow (RTOR) |  |  | 156 |  |  |  |  |  |  |  |  | 162 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 475 | 509 | 0 | 718 | 0 | 0 | 0 | 0 | 0 | 597 | 449 |
| Turn Type |  | NA | Free |  | NA |  |  |  |  |  | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  |  |  |  | , |  |
| Permitted Phases |  |  | Free |  |  |  |  |  |  |  |  | 6 |
| Total Split (s) |  | 49.0 |  |  | 49.0 |  |  |  |  |  | 41.0 | 41.0 |
| Total Lost Time (s) |  | 4.5 |  |  | 4.5 |  |  |  |  |  | 4.5 | 4.5 |
| Act Effct Green (s) |  | 47.1 | 90.0 |  | 47.1 |  |  |  |  |  | 33.9 | 33.9 |
| Actuated g/C Ratio |  | 0.52 | 1.00 |  | 0.52 |  |  |  |  |  | 0.38 | 0.38 |
| v/c Ratio |  | 0.48 | 0.32 |  | 0.73 |  |  |  |  |  | 0.84 | 0.64 |
| Control Delay |  | 7.5 | 0.3 |  | 22.8 |  |  |  |  |  | 37.6 | 18.4 |
| Queue Delay |  | 0.5 | 0.0 |  | 1.8 |  |  |  |  |  | 0.0 | 0.1 |
| Total Delay |  | 8.0 | 0.3 |  | 24.6 |  |  |  |  |  | 37.6 | 18.4 |
| LOS |  | A | A |  | C |  |  |  |  |  | D | B |
| Approach Delay |  | 4.0 |  |  | 24.6 |  |  |  |  |  | 29.3 |  |
| Approach LOS |  | A |  |  | C |  |  |  |  |  | C |  |
| Queue Length 50th (m) |  | 27.4 | 0.0 |  | 96.8 |  |  |  |  |  | 87.7 | 37.2 |
| Queue Length 95th (m) |  | m32.1 | m0.0 |  | 142.9 |  |  |  |  |  | \#130.3 | 67.4 |
| Internal Link Dist ( $m$ ) |  | 113.6 |  |  | 461.9 |  |  | 166.4 |  |  | 142.0 |  |
| Turn Bay Length ( m ) |  |  | 20.0 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) |  | 986 | 1601 |  | 986 |  |  |  |  |  | 763 | 745 |
| Starvation Cap Reductn |  | 201 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 133 |  |  |  |  |  | 0 | 11 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 |  |  |  |  |  | 0 | 0 |
| Reduced v/c Ratio |  | 0.61 | 0.32 |  | 0.84 |  |  |  |  |  | 0.78 | 0.61 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $24(27 \%)$, Referenced to phase 4:EBT and 8:WBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.84 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 19.0 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 71.2\% |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 50 : Rothesay Ave





| Major/Minor |  | Major1 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All |  | 0 | - | 718 | - |
| Stage 1 |  | - |  | 0 | - |
| Stage 2 |  | - |  | 718 | - |
| Critical Hdwy |  | - | - | 6.42 | - |
| Critical Hdwy Stg 1 |  | - | - | - | - |
| Critical Hdwy Stg 2 |  | - | - | 5.42 | - |
| Follow-up Hdwy |  | - | - | 3.518 | - |
| Pot Cap-1 Maneuver |  | - | 0 | ~396 | 0 |
| Stage 1 |  | - | 0 | - | 0 |
| Stage 2 |  | - | 0 | 483 | 0 |
| Platoon blocked, \% |  | - |  |  |  |
| Mov Cap-1 Maneuver |  | - | - | ~ 396 | 0 |
| Mov Cap-2 Maneuver |  | - | - | $\sim 396$ | 0 |
| Stage 1 |  | - | - | - | 0 |
| Stage 2 |  | - | - | 483 | 0 |
|  |  |  |  |  |  |
| Approach |  | NB |  | SB |  |
| HCM Control Delay, s |  | 0 |  | 142.2 |  |
| HCM LOS |  |  |  | F |  |
|  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBT SBLn1 |  |  |  |  |
| Capacity (veh/h) | - 396 |  |  |  |  |
| HCM Lane V/C Ratio | - 1.199 |  |  |  |  |
| HCM Control Delay (s) | - 142.2 |  |  |  |  |
| HCM Lane LOS | - F |  |  |  |  |
| HCM 95th \%tile Q(veh) | - 19.2 |  |  |  |  |
| Notes |  |  |  |  |  |
| $\sim$ : Volume exceeds capacity | \$: Delay exceeds 300s | +: Computation Not Defined |  | *: All | or volume in platoon |



$\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | PM |
| Freeway/Dir of Travel: | EB |
| Junction: | Rothesay Rd Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3137 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
Volume on ramp
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \quad \mathrm{~km} / \mathrm{h}$
$1106 \quad$ vph
300 m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No
Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
vph

$\qquad$


Capacity Checks

|  | Actual | Maximum | LOS F? |
| :---: | :---: | :---: | :---: |
| $\mathrm{v}=\mathrm{v}$ | 3834 | 4600 | No |
| Fi F |  |  |  |
| v | 3834 | 4400 | No |
| 12 |  |  |  |
| $\mathrm{v}=\mathrm{v}-\mathrm{v}$ | 2593 | 4600 | No |
| FO F R |  |  |  |
| v | 1241 | 2000 | No |
| R |  |  |  |

Level of Service Determination (if not $F$ ) $\qquad$

| Density, | $\mathrm{D}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L}=17.5 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ |
| :---: | :---: |
| Level of service for ramp-freeway junction areas of influence | $D$ |

Speed Estimation $\qquad$


```
Phone:
Fax:
```

E-mail:

Merge Analysis $\qquad$

| Analyst: | Katie Hazzard |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | $1 / 23 / 2017$ |
| Analysis time period: | AM Peak |
| Freeway/Dir of Travel: | WB |
| Junction: | Ashburn On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3240 | vph |


|  | Rata__On Ramp |  |
| :--- | :---: | :---: |
| Side of freeway | Right |  |
| Number of lanes in ramp | 1 | $\mathrm{~km} / \mathrm{h}$ |
| Free-flow speed on ramp | 60.0 | vph |
| Volume on ramp | 854 | m |
| Length of first accel/decel lane | 280 | m |
| Length of second accel/decel lane |  |  |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V | 4918 | 4600 | Yes |
| FO | 4918 | 4600 | Yes |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=23.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $F$
Speed Estimation

Phone: Fax:

E-mail:

Diverge Analysis $\qquad$

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Morning Peak |
| Freeway/Dir of Travel: | Westbound |
| Junction: | Route 100 Off Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |

Description:

Freeway Data $\qquad$

| Type of analysis | Diverge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3240 | vph |

Off Ramp Data $\qquad$

Side of freeway
Number of lanes in ramp
Free-Flow speed on ramp
$\begin{array}{lll}\text { Volume on ramp } & 1068 & \mathrm{vph} \\ \text { Length of first accel/decel lane } & 240 & \mathrm{~m}\end{array}$
Length of first accel/decel lane
Length of second accel/decel lane

Right
1
$60.0 \mathrm{~km} / \mathrm{h}$
m
$\qquad$

Does adjacent ramp exist?
Volume on adjacent ramp
No

Position of adjacent ramp
Type of adjacent ramp
Distance to adjacent ramp
m

$\qquad$


Capacity Checks


Level of Service Determination (if not $F$ ) $\qquad$

| Density, | $\mathrm{D}=2.642+0.0053 \mathrm{v}-0.0183 \mathrm{~L}$ |
| ---: | :--- |
| R | $=12.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$ |
| Level of service for ramp-freeway junction areas of influence | D |

Speed Estimation $\qquad$

| Intermediate speed variable, | $D_{S}=0.511$ |  |
| :---: | :---: | :---: |
| Space mean speed in ramp influence area, | $\underset{R}{S}=83.1$ | km/h |
| Space mean speed in outer lanes, | $S_{0}=N / A$ | km/h |
| Space mean speed for all vehicles, | $S=83.1$ | km/h |

```
Phone:
Fax:
```

E-mail:

Merge Analysis

| Analyst: | KEH |
| :--- | :--- |
| Agency/Co.: | exp |
| Date performed: | 2017 |
| Analysis time period: | Evening Peak |
| Freeway/Dir of Travel: | EB |
| Junction: | Route 100 On Ramp |
| Jurisdiction: | Provincial |
| Analysis Year: | 2033 |
| Description: The Crossing |  |

Freeway Data $\qquad$

| Type of analysis | Merge |  |
| :--- | :--- | :--- |
| Number of lanes in freeway | 2 |  |
| Free-flow speed on freeway | 100.0 | $\mathrm{~km} / \mathrm{h}$ |
| Volume on freeway | 3110 | vph |


| Side of freeway | Right |  |
| :---: | :---: | :---: |
| Number of lanes in ramp | 1 |  |
| Free-flow speed on ramp | 60.0 | km/h |
| Volume on ramp | 829 | vph |
| Length of first accel/decel lane | 250 | m |
| Length of second accel/decel lane |  | m |


| Does adjacent ramp exist? | No |  |
| :--- | :--- | :--- |
| Volume on adjacent Ramp |  | vph |
| Position of adjacent Ramp |  |  |
| Type of adjacent Ramp | m |  |


$\qquad$


Capacity Checks $\qquad$

|  | Actual | Maximum | LOS F? |
| :--- | :--- | :--- | :--- |
| V FO | 4628 | 4600 | Yes |
| V | 4628 | 4600 | Yes |

Level of Service Determination (if not $F$ ) $\qquad$
Density, $D=3.402+0.00456 \mathrm{v}+0.0048 \mathrm{v}-0.01278 \mathrm{~L}=22.2 \mathrm{pc} / \mathrm{km} / \mathrm{ln}$
R R 12 A
Level of service for ramp-freeway junction areas of influence $F$
Speed Estimation


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 0.1 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | t |  | \% | $\uparrow$ | \% | 「 |
| Traffic Vol, veh/h | 312 | 0 | 6 | 270 | O | 1 |
| Future Vol, veh/h | 312 | 0 | 6 | 270 | 0 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 0 | - | 0 | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 339 | 0 | 7 | 293 | 0 | 1 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 0.8 |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }^{7}$ | 4 | F |  |
| Traffic Vol, veh/h | 6 | 32 | 22 | 450 | 266 | 4 |
| Future Vol, veh/h | 6 | 32 | 22 | 450 | 266 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | 0 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 7 | 35 | 24 | 489 | 289 | 4 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 0.6 |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * | 「 | F |  | * | $\uparrow$ |
| Traffic Vol, veh/h | 24 | 4 | 468 | 22 | 4 | 294 |
| Future Vol, veh/h | 24 | 4 | 468 | 22 | 4 | 294 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 26 | 4 | 509 | 24 | 4 | 320 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }^{7}$ | 4 | ¢ |  |
| Traffic Vol, veh/h | 1 | 3 | 4 | 489 | 317 | 1 |
| Future Vol, veh/h | 1 | 3 | 4 | 489 | 317 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | 500 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 1 | 3 | 4 | 532 | 345 | 1 |



|  | 4 | $\rightarrow$ |  | 7 |  |  | $4$ | $\dagger$ |  |  | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 2 | 32 | 5 | 179 | 6 | 59 | 4 | 432 | 204 | 34 | 284 | 2 |
| Future Volume (vph) | 2 | 32 | 5 | 179 | 6 | 59 | 4 | 432 | 204 | 34 | 284 | 2 |
| Satd. Flow (prot) | 1789 | 1848 | 0 | 1789 | 1629 | 0 | 1789 | 1793 | 0 | 1789 | 1882 | 0 |
| Flt Permitted | 0.711 |  |  | 0.731 |  |  | 0.570 |  |  | 0.299 |  |  |
| Satd. Flow (perm) | 1339 | 1848 | 0 | 1377 | 1629 | 0 | 1074 | 1793 | 0 | 563 | 1882 | 0 |
| Satd. Flow (RTOR) |  | 5 |  |  | 64 |  |  | 62 |  |  | 1 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 2 | 40 | 0 | 195 | 71 | 0 | 4 | 692 | 0 | 37 | 311 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Total Split (s) | 22.8 | 22.8 |  | 22.8 | 22.8 |  | 37.2 | 37.2 |  | 37.2 | 37.2 |  |
| Total Lost Time (s) | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  |
| Act Effct Green (s) | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 35.7 | 35.7 |  | 35.7 | 35.7 |  |
| Actuated g/C Ratio | 0.23 | 0.23 |  | 0.23 | 0.23 |  | 0.62 | 0.62 |  | 0.62 | 0.62 |  |
| v/c Ratio | 0.01 | 0.10 |  | 0.63 | 0.17 |  | 0.01 | 0.61 |  | 0.11 | 0.27 |  |
| Control Delay | 15.0 | 14.7 |  | 28.8 | 6.8 |  | 5.8 | 10.0 |  | 6.9 | 6.6 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 15.0 | 14.7 |  | 28.8 | 6.8 |  | 5.8 | 10.0 |  | 6.9 | 6.6 |  |
| LOS | B | B |  | C | A |  | A | A |  | A | A |  |
| Approach Delay |  | 14.7 |  |  | 22.9 |  |  | 10.0 |  |  | 6.6 |  |
| Approach LOS |  | B |  |  | C |  |  | A |  |  | A |  |
| Queue Length 50th (m) | 0.2 | 2.7 |  | 17.1 | 0.5 |  | 0.2 | 32.9 |  | 1.3 | 12.3 |  |
| Queue Length 95th (m) | 1.4 | 8.3 |  | 33.5 | 7.7 |  | 1.2 | 78.5 |  | 5.7 | 29.1 |  |
| Internal Link Dist (m) |  | 116.7 |  |  | 101.0 |  |  | 79.1 |  |  | 152.8 |  |
| Turn Bay Length (m) |  |  |  |  |  |  | 25.0 |  |  | 50.0 |  |  |
| Base Capacity (vph) | 426 | 592 |  | 439 | 563 |  | 664 | 1133 |  | 348 | 1164 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.00 | 0.07 |  | 0.44 | 0.13 |  | 0.01 | 0.61 |  | 0.11 | 0.27 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 57.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.63 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 11.8 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 59.2\% |  |  |  | ICU Level of Service B |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

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| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ${ }^{1}$ | 7 | 个 |  | ${ }^{7}$ | 4 |
| Traffic Vol, veh/h | 58 | 25 | 586 | 113 | 33 | 435 |
| Future Vol, veh/h | 58 | 25 | 586 | 113 | 33 | 435 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized |  | None | - | None | - | None |
| Storage Length | 0 | 0 | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 63 | 27 | 637 | 123 | 36 | 473 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | F |  | 7 | F |  | ${ }^{7}$ | F |  | ${ }^{7}$ | F |  |
| Traffic Vol, veh/h | 31 | 20 | 42 | 10 | 5 | 17 | 7 | 647 | 62 | 19 | 506 | 7 |
| Future Vol, veh/h | 31 | 20 | 42 | 10 | 5 | 17 | 7 | 647 | 62 | 19 | 506 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | 0 | - | - | 250 | - |  | 500 | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - |  | 0 |  | - | 0 |  |
| Grade, \% | - | 0 |  | - | 0 | - |  | 0 |  |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 34 | 22 | 46 | 11 | 5 | 18 | 8 | 703 | 67 | 21 | 550 | 8 |



|  | 4 | $\rightarrow$ |  |  |  |  |  | 4 |  |  | $\frac{1}{\dagger}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | 1 | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 18 | 12 | 16 | 87 | 13 | 16 | 18 | 654 | 62 | 18 | 531 | 20 |
| Future Volume (vph) | 18 | 12 | 16 | 87 | 13 | 16 | 18 | 654 | 62 | 18 | 531 | 20 |
| Satd. Flow (prot) | 1789 | 1723 | 0 | 1789 | 1729 | 0 | 1789 | 1859 | 0 | 1789 | 1872 | 0 |
| Flt Permitted | 0.737 |  |  | 0.738 |  |  | 0.387 |  |  | 0.275 |  |  |
| Satd. Flow (perm) | 1388 | 1723 | 0 | 1390 | 1729 | 0 | 729 | 1859 | 0 | 518 | 1872 | 0 |
| Satd. Flow (RTOR) |  | 17 |  |  | 17 |  |  | 13 |  |  | 5 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 20 | 30 | 0 | 95 | 31 | 0 | 20 | 778 | 0 | 20 | 599 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Total Split (s) | 22.6 | 22.6 |  | 22.6 | 22.6 |  | 37.4 | 37.4 |  | 37.4 | 37.4 |  |
| Total Lost Time (s) | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  |
| Act Effct Green (s) | 8.8 | 8.8 |  | 8.8 | 8.8 |  | 31.5 | 31.5 |  | 31.5 | 31.5 |  |
| Actuated g/C Ratio | 0.19 | 0.19 |  | 0.19 | 0.19 |  | 0.70 | 0.70 |  | 0.70 | 0.70 |  |
| v/c Ratio | 0.07 | 0.09 |  | 0.35 | 0.09 |  | 0.04 | 0.60 |  | 0.06 | 0.46 |  |
| Control Delay | 16.7 | 11.5 |  | 21.1 | 11.6 |  | 4.4 | 8.4 |  | 4.8 | 6.5 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 16.7 | 11.5 |  | 21.1 | 11.6 |  | 4.4 | 8.4 |  | 4.8 | 6.5 |  |
| LOS | B | B |  | C | B |  | A | A |  | A | A |  |
| Approach Delay |  | 13.5 |  |  | 18.7 |  |  | 8.3 |  |  | 6.5 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | A |  |
| Queue Length 50th (m) | 1.3 | 0.8 |  | 6.4 | 0.9 |  | 0.5 | 32.5 |  | 0.5 | 21.5 |  |
| Queue Length 95th (m) | 5.8 | 6.0 |  | 18.0 | 6.2 |  | 2.6 | 76.1 |  | 2.8 | 49.1 |  |
| Internal Link Dist (m) |  | 97.7 |  |  | 79.8 |  |  | 100.5 |  |  | 62.0 |  |
| Turn Bay Length (m) |  |  |  |  |  |  | 50.0 |  |  | 25.0 |  |  |
| Base Capacity (vph) | 581 | 732 |  | 582 | 734 |  | 537 | 1374 |  | 382 | 1382 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.03 | 0.04 |  | 0.16 | 0.04 |  | 0.04 | 0.57 |  | 0.05 | 0.43 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 45.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 8.6 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 57.2\% |  |  |  | ICU Level of Service B |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

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| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations | ${ }^{7}$ | 4 | $\uparrow$ |  | ${ }^{1 /}$ | $\stackrel{7}{ }$ |
| Traffic Vol, veh/h | 25 | 734 | 566 | 46 | 48 | 26 |
| Future Vol, veh/h | 25 | 734 | 566 | 46 | 48 | 26 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 500 | - | - | - | 0 | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 27 | 798 | 615 | 50 | 52 | 28 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 0.1 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL |  | NBL | NBR |
| Lane Configurations | $\hat{\beta}$ |  | \% | $\uparrow$ | \% | 「 |
| Traffic Vol, veh/h | 288 | 0 | 6 | 300 | 0 | 1 |
| Future Vol, veh/h | 288 | 0 | 6 | 300 | 0 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 0 | - | 0 | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 313 | 0 | 7 | 326 | 0 | 1 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.3 |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 「 | ${ }^{7}$ | 4 | F |  |
| Traffic Vol, veh/h | 5 | 44 | 44 | 302 | 293 | 5 |
| Future Vol, veh/h | 5 | 44 | 44 | 302 | 293 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | 0 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 48 | 48 | 328 | 318 | 5 |





| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 7 | ${ }^{7}$ | 4 | $\uparrow$ |  |
| Traffic Vol, veh/h | 1 | 5 | 6 | 373 | 360 | 1 |
| Future Vol, veh/h | 1 | 5 | 6 | 373 | 360 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | 500 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 1 | 5 | 7 | 405 | 391 | 1 |



|  | 4 | $\rightarrow$ |  | 7 |  |  | $4$ | $\dagger$ |  |  | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  | ${ }^{7}$ | 个 |  |
| Traffic Volume (vph) | 3 | 16 | 10 | 110 | 15 | 75 | 9 | 301 | 154 | 85 | 275 | 3 |
| Future Volume (vph) | 3 | 16 | 10 | 110 | 15 | 75 | 9 | 301 | 154 | 85 | 275 | 3 |
| Satd. Flow (prot) | 1789 | 1772 | 0 | 1789 | 1646 | 0 | 1789 | 1787 | 0 | 1789 | 1882 | 0 |
| Flt Permitted | 0.694 |  |  | 0.739 |  |  | 0.576 |  |  | 0.446 |  |  |
| Satd. Flow (perm) | 1307 | 1772 | 0 | 1392 | 1646 | 0 | 1085 | 1787 | 0 | 840 | 1882 | 0 |
| Satd. Flow (RTOR) |  | 11 |  |  | 82 |  |  | 68 |  |  | 1 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 3 | 28 | 0 | 120 | 98 | 0 | 10 | 494 | 0 | 92 | 302 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Total Split (s) | 22.5 | 22.5 |  | 22.5 | 22.5 |  | 22.5 | 22.5 |  | 22.5 | 22.5 |  |
| Total Lost Time (s) | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  |
| Act Effct Green (s) | 8.5 | 8.5 |  | 8.5 | 8.5 |  | 23.3 | 23.3 |  | 23.3 | 23.3 |  |
| Actuated g/C Ratio | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 0.61 | 0.61 |  | 0.61 | 0.61 |  |
| v/c Ratio | 0.01 | 0.07 |  | 0.38 | 0.23 |  | 0.02 | 0.44 |  | 0.18 | 0.26 |  |
| Control Delay | 9.7 | 8.3 |  | 15.3 | 5.6 |  | 5.3 | 6.8 |  | 6.8 | 6.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 9.7 | 8.3 |  | 15.3 | 5.6 |  | 5.3 | 6.8 |  | 6.8 | 6.2 |  |
| LOS | A | A |  | B | A |  | A | A |  | A | A |  |
| Approach Delay |  | 8.5 |  |  | 10.9 |  |  | 6.8 |  |  | 6.3 |  |
| Approach LOS |  | A |  |  | B |  |  | A |  |  | A |  |
| Queue Length 50th (m) | 0.2 | 0.8 |  | 5.8 | 0.7 |  | 0.3 | 13.3 |  | 2.5 | 8.5 |  |
| Queue Length 95th (m) | 1.2 | 4.2 |  | 14.3 | 7.1 |  | 1.7 | 35.9 |  | 9.2 | 22.2 |  |
| Internal Link Dist (m) |  | 116.7 |  |  | 101.0 |  |  | 79.1 |  |  | 152.8 |  |
| Turn Bay Length (m) |  |  |  |  |  |  | 25.0 |  |  | 50.0 |  |  |
| Base Capacity (vph) | 622 | 849 |  | 662 | 826 |  | 666 | 1124 |  | 516 | 1157 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.00 | 0.03 |  | 0.18 | 0.12 |  | 0.02 | 0.44 |  | 0.18 | 0.26 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 45 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 37.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.44 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 7.5 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 53.9\% |  |  |  | ICU Level of Service A |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

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| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ${ }^{1}$ | 「 | 个 |  | ${ }^{1}$ | 4 |
| Traffic Vol, veh/h | 58 | 25 | 439 | 100 | 38 | 360 |
| Future Vol, veh/h | 58 | 25 | 439 | 100 | 38 | 360 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | - | - | 500 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 63 | 27 | 477 | 109 | 41 | 391 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.6 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | \% | F |  | ${ }^{7}$ | F |  |
| Traffic Vol, veh/h | 6 | 4 | 5 | 40 | 5 | 37 | 6 | 496 | 152 | 57 | 354 | 7 |
| Future Vol, veh/h | 6 | 4 | 5 | 40 | 5 | 37 | 6 | 496 | 152 | 57 | 354 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | 0 | - | - | 250 | - | - | 500 | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 7 | 4 | 5 | 43 | 5 | 40 | 7 | 539 | 165 | 62 | 385 | 8 |


| Major/Minor | Minor2 |  | Minor1 |  |  |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1171 | 1230 | 389 |  | 1152 | 1151 | 622 |  | 392 | 0 | 0 | 704 | 0 | 0 |
| Stage 1 | 513 | 513 | - |  | 635 | 635 | - |  | - | - | - | - | - |  |
| Stage 2 | 658 | 717 | - |  | 517 | 516 | - |  | - | - | - | - | - |  |
| Critical Hdwy | 7.12 | 6.52 | 6.22 |  | 7.12 | 6.52 | 6.22 |  | 4.12 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - |  | 6.12 | 5.52 | - |  | - | - | - |  | - |  |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 |  | 3.518 | 4.018 | 3.318 |  | 2.218 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 170 | 178 | 659 |  | 175 | 198 | 487 |  | 1167 | - | - | 894 | - |  |
| Stage 1 | 544 | 536 | - |  | 467 | 472 | - |  | - | - | - | - | - |  |
| Stage 2 | 453 | 434 | - |  | 541 | 534 | - |  | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 144 | 165 | 659 |  | 160 | 183 | 487 |  | 1167 | - | - | 894 | - |  |
| Mov Cap-2 Maneuver | 144 | 165 | - |  | 160 | 183 | - |  | - | - | - | - | - |  |
| Stage 1 | 541 | 499 |  |  | 464 | 469 | - |  | - | - |  |  | - |  |
| Stage 2 | 408 | 431 | - |  | 495 | 497 | - |  | - | - | - | - | - |  |
| Approach | EB |  |  |  | WB |  |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 23.4 |  |  |  | 25.1 |  |  |  | 0.1 |  |  | 1.3 |  |  |
| HCM LOS | C |  |  |  | D |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | EBLn2 | VBLn1 | WBLn2 | SBL | SBT | SBR |  |  |  |  |
| Capacity (veh/h) | 1167 | - | - | 144 | 283 | 160 | 407 | 894 | - | - |  |  |  |  |
| HCM Lane V/C Ratio | 0.006 | - | - | 0.045 | 0.035 | 0.272 | 0.112 | 0.069 | - | - |  |  |  |  |
| HCM Control Delay (s) | 8.1 | - | - | 31.2 | 18.2 | 35.7 | 15 | 9.3 | - | - |  |  |  |  |
| HCM Lane LOS | A |  |  | D | C | E | C | A | - | - |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | - |  | 0.1 | 0.1 | 1 | 0.4 | 0.2 | - | - |  |  |  |  |


|  | 4 |  |  | 4 |  | 4 | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 个 |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 12 | 8 | 11 | 135 | 7 | 37 | 9 | 543 | 152 | 57 | 331 | 11 |
| Future Volume (vph) | 12 | 8 | 11 | 135 | 7 | 37 | 9 | 543 | 152 | 57 | 331 | 11 |
| Satd. Flow (prot) | 1789 | 1721 | 0 | 1789 | 1648 | 0 | 1789 | 1821 | 0 | 1789 | 1874 | 0 |
| Flt Permitted |  |  |  | 0.755 |  |  | 0.532 |  |  | 0.268 |  |  |
| Satd. Flow (perm) | 1883 | 1721 | 0 | 1422 | 1648 | 0 | 1002 | 1821 | 0 | 505 | 1874 | 0 |
| Satd. Flow (RTOR) |  | 12 |  |  | 40 |  |  | 28 |  |  | 3 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 13 | 21 | 0 | 147 | 48 | 0 | 10 | 755 | 0 | 62 | 372 | 0 |
| Turn Type | pm+pt | NA |  | pm+pt | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Total Split (s) | 9.0 | 22.6 |  | 9.0 | 22.6 |  | 33.4 | 33.4 |  | 33.4 | 33.4 |  |
| Total Lost Time (s) | 4.0 | 4.5 |  | 4.0 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  |
| Act Effct Green (s) | 6.5 | 6.1 |  | 7.3 | 6.2 |  | 32.9 | 32.9 |  | 32.9 | 32.9 |  |
| Actuated g/C Ratio | 0.14 | 0.13 |  | 0.16 | 0.13 |  | 0.70 | 0.70 |  | 0.70 | 0.70 |  |
| v/c Ratio | 0.05 | 0.09 |  | 0.55 | 0.19 |  | 0.01 | 0.59 |  | 0.18 | 0.28 |  |
| Control Delay | 15.6 | 14.7 |  | 24.9 | 11.2 |  | 4.8 | 8.8 |  | 6.5 | 5.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 15.6 | 14.7 |  | 24.9 | 11.2 |  | 4.8 | 8.8 |  | 6.5 | 5.2 |  |
| LOS | B | B |  | C | B |  | A | A |  | A | A |  |
| Approach Delay |  | 15.0 |  |  | 21.6 |  |  | 8.8 |  |  | 5.3 |  |
| Approach LOS |  | B |  |  | C |  |  | A |  |  | A |  |
| Queue Length 50th (m) | 0.9 | 0.6 |  | 10.6 | 0.5 |  | 0.2 | 22.3 |  | 1.3 | 8.5 |  |
| Queue Length 95th (m) | 3.8 | 5.6 |  | 21.8 | 7.9 |  | 2.1 | \#100.7 |  | 9.0 | 33.7 |  |
| Internal Link Dist (m) |  | 97.7 |  |  | 79.8 |  |  | 100.5 |  |  | 62.0 |  |
| Turn Bay Length (m) |  |  |  |  |  |  | 50.0 |  |  | 25.0 |  |  |
| Base Capacity (vph) | 249 | 677 |  | 268 | 666 |  | 703 | 1287 |  | 354 | 1316 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.05 | 0.03 |  | 0.55 | 0.07 |  | 0.01 | 0.59 |  | 0.18 | 0.28 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 65 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 46.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.59 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 9.6 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 67.4\% |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

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| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | NBL | NBT | SBT | SBR | SEL | SER |
| Lane Configurations | ${ }^{1}$ | 4 | $\uparrow$ |  | ${ }^{1}$ | F' |
| Traffic Vol, veh/h | 25 | 673 | 463 | 46 | 48 | 26 |
| Future Vol, veh/h | 25 | 673 | 463 | 46 | 48 | 26 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 500 | - | - | - | 0 | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 27 | 732 | 503 | 50 | 52 | 28 |



|  | $\checkmark$ |  |  | $\pm$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SWL | SWR |
| Lane Configurations | ${ }^{7}$ | 4 | 4 | 「 | ${ }^{7}$ | 「' |
| Traffic Volume (vph) | 145 | 329 | 443 | 388 | 489 | 309 |
| Future Volume (vph) | 145 | 329 | 443 | 388 | 489 | 309 |
| Satd. Flow (prot) | 1789 | 1883 | 1883 | 1601 | 1789 | 1601 |
| Flt Permitted | 0.342 |  |  |  | 0.950 |  |
| Satd. Flow (perm) | 644 | 1883 | 1883 | 1601 | 1789 | 1601 |
| Satd. Flow (RTOR) |  |  |  | 422 |  | 226 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% | 0\% |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 158 | 358 | 482 | 422 | 532 | 336 |
| Turn Type | Perm | NA | NA | Perm | Prot | Perm |
| Protected Phases |  | 4 | 8 |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 6 |
| Total Split (s) | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Act Effct Green (s) | 18.0 | 18.0 | 18.0 | 18.0 | 18.0 | 18.0 |
| Actuated g/C Ratio | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 |
| v/c Ratio | 0.61 | 0.48 | 0.64 | 0.47 | 0.74 | 0.43 |
| Control Delay | 25.2 | 12.6 | 15.7 | 3.3 | 20.3 | 5.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.2 | 12.6 | 15.7 | 3.3 | 20.3 | 5.6 |
| LOS | C | B | B | A | C | A |
| Approach Delay |  | 16.5 | 9.9 |  | 14.6 |  |
| Approach LOS |  | B | A |  | B |  |
| Queue Length 50th (m) | 9.3 | 19.6 | 28.7 | 0.0 | 33.6 | 5.2 |
| Queue Length 95th (m) | \#31.2 | 36.4 | 52.4 | 11.9 | \#73.9 | 17.7 |
| Internal Link Dist (m) |  | 146.4 | 432.6 |  | 133.7 |  |
| Turn Bay Length (m) | 50.0 |  |  | 50.0 |  |  |
| Base Capacity (vph) | 257 | 753 | 753 | 893 | 715 | 776 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.61 | 0.48 | 0.64 | 0.47 | 0.74 | 0.43 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 45 |  |  |  |  |  |  |
| Actuated Cycle Length: 45 |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2: and 6:SWL, Start of Green |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.74 |  |  |  |  |  |  |
| Intersection Signal Delay: 13.2 |  |  |  | Intersection LOS: B |  |  |
| Intersection Capacity Utilization 69.7\% |  |  |  |  |  |  |

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 62:


| Lane Group | SEL | SET | NWT | NWR | SWL | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 4 | 4 | 「 | * | 「 |
| Traffic Volume (vph) | 134 | 456 | 245 | 709 | 673 | 189 |
| Future Volume (vph) | 134 | 456 | 245 | 709 | 673 | 189 |
| Satd. Flow (prot) | 1789 | 1883 | 1883 | 1601 | 1789 | 1601 |
| Flt Permitted | 0.390 |  |  |  | 0.950 |  |
| Satd. Flow (perm) | 735 | 1883 | 1883 | 1601 | 1789 | 1601 |
| Satd. Flow (RTOR) |  |  |  | 771 |  | 205 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% | 0\% |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 146 | 496 | 266 | 771 | 732 | 205 |
| Turn Type | pm+pt | NA | NA | Perm | Prot | Perm |
| Protected Phases | 1 | 6 | 2 |  | 8 |  |
| Permitted Phases | 6 |  |  | 2 |  | 8 |
| Total Split (s) | 9.0 | 36.0 | 27.0 | 27.0 | 39.0 | 39.0 |
| Total Lost Time (s) | 4.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Act Effct Green (s) | 25.5 | 25.0 | 18.4 | 18.4 | 30.8 | 30.8 |
| Actuated g/C Ratio | 0.39 | 0.38 | 0.28 | 0.28 | 0.47 | 0.47 |
| v/c Ratio | 0.39 | 0.69 | 0.50 | 0.77 | 0.87 | 0.24 |
| Control Delay | 17.0 | 22.8 | 25.0 | 7.9 | 30.2 | 2.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 17.0 | 22.8 | 25.0 | 7.9 | 30.2 | 2.8 |
| LOS | B | C | C | A | C | A |
| Approach Delay |  | 21.5 | 12.3 |  | 24.2 |  |
| Approach LOS |  | C | B |  | C |  |
| Queue Length 50th (m) | 12.4 | 53.4 | 30.4 | 0.0 | 82.5 | 0.0 |
| Queue Length 95th (m) | 23.3 | 83.4 | 51.0 | 27.2 | \#157.4 | 10.0 |
| Internal Link Dist (m) |  | 152.1 | 429.7 |  | 108.5 |  |
| Turn Bay Length (m) | 50.0 |  |  | 50.0 |  |  |
| Base Capacity (vph) | 372 | 954 | 681 | 1071 | 992 | 980 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.39 | 0.52 | 0.39 | 0.72 | 0.74 | 0.21 |

## Intersection Summary

Cycle Length: 75
Actuated Cycle Length: 65.3
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.87

Intersection Signal Delay: 18.8
Intersection Capacity Utilization 68.8\%
Analysis Period (min) 15

Intersection LOS: B
ICU Level of Service C
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 27:


